

LAND USE APPLICATION FORM

(Please print or type the information below)

Planning Department 39250 Pioneer Blvd. Sandy OR 97055 503-668-4886

Name of Project Sandy Health Clinic					
Location or Address 39831 Hwy 26, Sandy, OR 97055					
Map & Tax Lot Number T 2S , R 4E , Section 13 ; Tax Lot(s) 24E13AD01001					
Plan Designation C-1 Zoning Designation Commercial Acres 0.47					
Request:					
clinic. Project will	Request for a Type II Design Review with (2) Type II Adjustments for a new health clinic. Project will consist of demolition of existing one-story building, construction of a new health clinic building, and associated site work.				
	I am the (check one) ☑ owner ☐ lessee of the property listed above and the statements and information contained herein are in all respects true, complete and correct to the best of my knowledge and belief.				
Applicant Steve Kelly		Owner			
Address 2051 Kaen Ro	oad	Address			
City/State/Zip Orego	n City, OR 97045	City/State/Zip			
Phone 503-655-8591		Phone			
Email Email stevekel@clackamas.us					
Signature Signature					
If signed by Agent, owner's written authorization must be attached.					
File No.	Date	Rec. No.	Fee \$		
Type of Review (circle one): Type I Type II Type III Type IV					



SUPPLEMENTAL APPLICATION DESIGN REVIEW / CONDITIONAL USE PERMIT

(Please print or type the information below)

Planning Department 39250 Pioneer Blvd. Sandy OR 97055 503-668-4886

USES WITHIN BUILDING (SQUARE FOOTAGE)

Offices:	Shop:	Storage:	
Kitchen:	Laundry:	Rest Rooms:	
Other:			
		& CONSTRUCTION TYPE apancies by square footage)	
UBC Occupancy R	Cating:		
UBC Type of Cons	struction:		
Will fire sprinklers	be installed in the bu	nilding? [] Yes [] No	

SITE ANALYSIS DATA				
Туре	Lot Coverage (Square Feet)	Lot Coverage (Percent of Site)		
Buildings				
Parking Lots and Driveways				
Private Walks & Pedestrian Ways				
Landscaping – Improved Area				
Landscaping – Natural areas				
Storm Water Detention, Retention & Bioswale Areas				
Other (describe)				
Other (describe)				

CONSTRUCTION MATERIAL DETAILS
Color & Type of Siding Materials:
Color & Type of Trim Materials:
Color & Type of Roof Materials:
Color & Type of Exterior Doors:
Color & Type of Exterior Stairs, Balconies & Railings:
Trash & Recycling Enclosure (describe type, colors, height):
Type of Lighting Fixtures (describe):
Pole:
Wall-Mounted:
Fencing (height and type):
Mailboxes (location and type):
Private Pedestrian Walkways (type of surfacing):
Recreational Amenities (describe type and location):
Other Site Elements (describe):

TYPE OF IRRIGATION SYSTEM
Describe type and brand of irrigation system to be installed. Formal irrigation plans must be submitted with construction plans.
PROPOSED SOIL AMENDMENTS
Describe soil conditions and proposed plans for soil treatment & amendments:
ADDITIONAL LANDSCAPING INFORMATION

LANDSCAPE MATERIALS				
Quantity	Type – Include botanical and common names. Plants must be keyed to landscape plan.	Size	Height	Spacing



Sandy Health Clinic 39831 Highway 26 Sandy, OR 97055

Type II Design Review Project Narrative February 12, 2020

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Application formsAttached separately

Attached separately Land Use Application Form, Supplemental Application Form, and fee

Design Review Drawings

Attached separately

Contacts

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Division City of Sandy

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Land Use / Design Reviews

Application Requested Type II Design Review

(2) Type II Adjustments, please see Sections B.3 and E.2 in the Building Design Standards, below. Sections are highlighted in red for clarity.

Pre-Application Conference Conference held December 18th, 2019

Design Review Application Submittal: Feb 12, 2020

Site Description

Site Address: Sandy Health Clinic

39831 HWY 26 Sandy, OR 97055

Jurisdiction: Sandy, OR / Clackamas County

Map & Tax Lot Numbers: T2S, R4E, Section 13; Tax Lot 24E13AD01001

Parcel Number: 01830433

Total Site Area: 0.47 acres (20,473sf)

Zoning: C-1 (Central Business District)

Current title Owner: Clackamas County Health Centers

2051 Kaen Road, 3rd Floor Oregon City, OR 97045

Street classification

Hwy 26 / Mt. Hood Highway Major Arterial roadway

SE Ten Eyck Road Minor Arterial roadway

Pleasant Street Local Street

Project Description

Overview

The project site is located between Hwy 26 / Mt. Hood Highway and Pleasant Street, at the corner of SE Ten Eyck Road. The site is generally flat, with an approximate $2 \frac{1}{2}$ -foot slope rising from the north to south at the sidewalk along Hwy 26, and an approximate $2 \frac{3}{4}$ -foot slope rising from the north to the south at the sidewalk along Pleasant Street. The parcel currently has a vacant building that was previously a distribution center, and an auto dealership. Zoning is C-1. The building height limit is 45 feet.

The proposed construction is for a one story Type VB, sprinklered health clinic, with primary care, behavioral health, and dental services. The reception / waiting area will be accessed from the parking lot, between the Sandy police station and the new building, at the northeast corner of the building. There will be other access points facing Hwy 26 and Pleasant Street. The Sandy clinic will operate Monday through Friday with hours of 8am-6pm. For the proposed development, 6 of the required spaces of the off-street parking will be shared on site with the Sandy Police Station. A parking agreement with Immanuel Lutheran Church, northeast of the property, will accommodate all staff parking and overflow visitor parking.

Total gross floor area: 9,381 gsf

Parking stalls: 22 stalls including 1 accessible van space and 6 compact spaces.

Bike storage: 5% or 2 whichever is greater

2 total (2 ½ feet x 6 feet x 7 feet vertical) for commercial use

Project Code Summary

Occupancy: B - Business

Construction type summary: One-story

Type VB

NFPA 13 Sprinkler System throughout.

Max code height: 60 ft maximum

Building is approximately 28 ft high

Zoning Requirements Narrative

Zoning: C-1 (Central Business District)

Land Use Review process: Preapplication Conference (December 18th, 2019)

Type II Design Review procedure

17.42.00: This district is intended to provide the community with a mix of retail,

personal services, offices, and residential needs of the community and its trade area in the city's traditional commercial core. This district is not intended for intensive automobile or industrial uses. This district is intended to provide the principal focus for civil and social functions within

the community.

city.

This commercial district is intended for civic uses and to provide all basic services and amenities required to keep the downtown the vital center of our community. While the district does not permit new low density building types, it is not intended to preclude dwelling units in buildings containing commercial activities. All development and uses shall be consistent with the intent of the district, as well as compatible with the space, access and exposure constraints and opportunities of the central

Zoning Requirements Narrative

Please see attached drawings for additional clarification regarding compliance.

Topic	Requirement	Chapter	Compliance
Permitted Uses	Commercial in buildings with up to 30,000 sf of gross floor area and without drive-through facilities	17.42.10.B.2. g	Medical facilities permitted outright.
Development Standards	Lot Area: No minimum Lot Dimensions: No minimum Setbacks: No minimum; maximum 10 ft Lot Coverage: No maximum Landscaping: 10% minimum Structure Height: 45 ft maximum	17.42.30.A	Lot Area: Comply Lot Dimensions: Comply Setbacks: Comply Lot Coverage: Comply Landscaping: 14% provided Structure Height: 28 ft
Special Setbacks	Property abutting a more restrictive zoning district shall have the same yard setback as required by the abutting district. Pleasant Street: Across street from more restrictive R-2., requiring 10 ft minimum setback and additional 10 ft added for each 10 ft increment in building height over 35 ft.	17.42.30.B	10 ft minimum setback provided from north property line.
Landscaping Preservation	Significant plant and tree specimens should be preserved to the greatest extent practicable.	17.92.10.C	Significant trees are currently at the sidewalks along Hwy 26 and Pleasant Street and will be preserved in the design. Trees will be preserved during construction by construction fences.
Planter Sizing	Planter and boundary areas used for required plantings shall have a minimum diameter of 5 feet.	17.92.10.D	Planted areas are 5 feet wide, minimum.
Planting Vision Clearance	Plantings or other screening is not permitted within vision clearance areas.	17.92.10.E	Tall plantings and screens are kept back from the street intersections.
Pedestrian Amenities	Up to 35% of the total required landscaped area may be developed into pedestrian amenities.	17.92.10.F	Area developed for pedestrian amenities are the civic space near the main entry and the internal courtyard / break area. Spaces are less than 35% total landscaped area.
Landscaping Extent	All areas not occupied by paved roadways, walkways, patios, or buildings shall be landscaped.	17.92.10.K	Complies.

Topic	Requirement	Chapter	Compliance
Торго	•	•	•
Minimum Landscaping and Screening Improvements	10% required for C-1 zone (2,047 SF)	17.92.20	15% (2,999 SF) provided.
Required Tree Plantings	1 medium canopy street tree at 30 feet on center. 1 medium parking lot tree per 8 cars (8 / 21 total cars = 2.6 trees)	17.92.30	Compliant street trees and parking lot trees provided. See Landscape Plan L1.01.
Irrigation	Landscaping to be irrigated to sustain viable plant life	17.92.40	Electric solenoid controlled underground irrigation system, with low point self drain will be used.
Types and Sizes of Plant Materials	A. 75% landscape area to be combination of trees, shrubs, or evergreen ground cover. B. Use native plant materials acclimatized to the Pacific Northwest. C. Trees with a mature spread of crown greater than 15 feet should have trunks with maintained clear condition of over 5 feet of clear wood. D. Deciduous trees to be balled and burlapped, minimum of 7 feet in overall height or 1 ½" in caliper 6" above the ground. E. Coniferous trees to be minimum of 5 feet above the ground at time of planting. F. Shrubs to be a minimum of 1 gal in size or 2 feet in height. G. Hedges to form a continuous, solid visual screen within 2 years after planting. H. Vines for screening to be minimum of 1 gal. or 30" in height. I. Groundcover to be fully rooted and well branched or leafed and provide complete coverage in one year. J. Turf areas to be species normally grown as permanent lawns in western Oregon. K. Landscaped areas may include architectural features or artificial ground cover not to exceed 25% of the required landscaped area.	17.92.50	A. Complies B. Complies C. Complies D. Complies E. Complies F. Complies G. No hedges in design. H. Vines not used for site screening. I. Complies J. No turf in design. K. Design includes benches, boulders, aluminum planters, wood fences, dark brown mulch, stone pavers, and a monument sign that do not exceed 25% of the landscaped area.
Landscaping Between Public Right-of-Way and Property Lines	Except for portions allowed for parking, loading, or traffic maneuvering, a required setback area abutting a public street and open area between property and roadway in the public street to be landscaped.	17.92.70	Area between property line and public streets are landscaped except where there is a sidewalk or driveway.

Topic	Requirement	Chapter	Compliance
Screening	A. Height and Opacity B. Chain Link Fencing C. Height Measurement D. Berms	17.92.90	A. Wood fencing is 8'-0" tall and at least 80% opaque. B. Not in project. C. Screen height is measured from the finished grade of screened improvements.
Screening of Service Facilities	Equipment and trash and recycling areas to be screened.	17.92.100	D. Not in project. The site transformer and condensing unit are screened, and the trash enclosure is CMU to match the building base material.
Off Street Parking Requirements	For medical office / clinic use: Number of car parking spaces: 1 per 300 sf, plus 1 per 2 employees Number of bike parking spaces: 5% or 2 whichever is greater	17.98.20	Car parking spaces: 8,345 GSF / 300 = 27.81 stalls 25% reduction for C-1 zone = 20.86 (21) required stalls. 6 of these required stalls are shared with the police station. 12 staff, 6 staff parking stalls at Immanuel Lutheran Church parking lot via agreement with church. Bike parking spaces: 27 stalls x 5% = 1.4 2 required bike spaces area provided near the main entry.
Accessible (ADA) Parking Stalls	1 accessible parking space required for parking facility with 1 to 25 stalls.	2010 ADA Standards Table 208.2	1 van accessible parking stall provided

Topic	Requirement	Chapter	Compliance
Parking Lot Design and Size	No more than 35% of parking stalls shall be compact spaces.	17.98.60	6 compact spaces / 22 total spaces = 27%, therefore ok
	90 degree parking aisle width: 20 feet single sided one-way, 25 feet double sided two-way		All parking it 90 degree. 25 foot aisle provided off of Pleasant Street. 17'-3" aisle provided at south end of site, near compact parking stalls. This is larger than the approximately 14 foot aisle that currently exists at the south end of the 6 shared stalls. If a stall needs to be removed to provide a 20 foot space, there will be one parking stall fewer than required. Because these stalls are compact, 17'-3" will be adequate for cars to back up into the aisle.
On-Site Circulation	Groups of more than 3 parking spaces shall be provided with adequate aisles or turnaround areas so that all vehicles enter the right-of-way in a forward manner.	17.98.70	Complies
Driveway	Driveway to an off-street parking area shall be a minimum of 20 feet for a two-way drive for the first 20 feet of the driveway. Shall not traverse a slope in excess of 15% at any point along the driveway length.	17.98.100	Complies
Landscaping and Screening	Between, and at the end of each parking bay, there shall be planters that have a minimum width of 5 feet and a minimum length of 17 feet for a single depth bay and 34 feet for a double bay. Each planter shall contain one major structural tree and ground cover.	17.98.120.D	Complies. Please see Site Plan and Landscape Plan
Paving	Parking areas, driveways, aisles, and turnarounds shall be paved with concrete, asphalt, or comparable surfacing, constructed to city standards for off-street vehicle areas.	17.98.130.A	Permeable asphalt will be used for the parking lot surface.

Topic	Requirement	Chapter	Compliance
Drainage	Provide adequate provisions for collection of drainage waters to eliminate sheet flow of water onto sidewalks, public rights-of-way, and abutting private property.	17.98.140	Permeable asphalt will be used for the parking lot surface.
Lighting	Artificial lighting to be provided at parking.	17.98.150	See sheet E1.02 – Electrical Site Lighting Plan.
Bicycle Parking Facilities	A. Location 17.98.160 B. Bicycle Parking Space Dimensions		A. Bike parking is located next to the primary building entrance, visible from the reception/waiting room, separated from the vehicular parking area, with direct access to the public right-ofway. B. Each of the (2) bike
	C. Security		parking spaces are 2 ½ feet by 6 feet, covered with a vertical clearance of 12 feet. C. Bikes can be locked to a provided bike rack with both cable and U-shaped locks, permitting the frame and one wheel to be secured. Bike rack is anchored to the
	D. Signing		ground and sheltered under a roof overhang. D. Bike parking is visible from the entry and public right-of-way, so no signage is needed.
Off-Street Loading Facilities	A. minimum area of loading zone to be 250 sf. B. Loading berth to be 10 feet by 35 feet minimum with a height clearance of 14 feet. C. Loading areas to be screened from public view with the same screening as parking lots. F. Off-street loading facilities not required when buildings abut a public alley in a way that loading can be conducted from the alley in accordance with applicable traffic and parking ordinances.	17.98.190	F. Loading will be conducted from clinic side of parking lot. Loading will be conducted off clinic hours. Deliveries anticipated at this clinic will be smaller in quantity due to requirements of the building program.

Building Design Standards Narrative

SANDY DESIGN STANDARDS (17.90.110)		PROPOSAL RESPONSE		
A	Site Layout and Vehicle Access			
A.1. A.3.	Lot shall abut or have cross access to a dedicated public street Off street parking located to the rear or side of buildings, with no portion of the lot within required setbacks or within 10-feet of the public right-of-way. Driveways for ingress or egress	 The lot has access to Hwy 26/Mt Hood Hwy and Pleasant Street Parking lot is an extension of the police station parking lot and sited between the two buildings. All portions of the lot are within required setbacks. 		
A.4.	shall be limited to one per 150 ft. Adjacent parking lots shall be connected to one another when the City determines it is practicable to do so.	Parking lot is an extension of the police station parking lot and sited between the two buildings.		
A.5.	Urban design details shall be used to calm traffic and protect pedestrians in parking areas.	Sidewalk crossing the driveway will be a different paving material than the parking lot.		
A.8. A.12.	Raised walkways or painted crossings from public street sidewalk to building entrance(s). Free-standing buildings shall be connected to one another with a seamless pedestrian network that provides access to building entrances and civic spaces.	 There is a different paving material used from the sidewalk to the main building entrance. The sidewalks along Pleasant Street and Hwy 26 connect to the health clinic and police station entrances. 		
B and	Building Facades, Materials,			
B.1.	Articulation	 1) All elevations facing public streets are broken into 30 feet or shorter. Each plane projects or recedes 24 inches from the adjacent plane. 2) Wall planes incorporate visually contrasting and complimentary trim. 		
B.2.	Pedestrian Shelters	 a) Shelter over building's main entry is provided by roof projecting over entry. Metal canopies are provided over the other entries. b) Canopies, roof overhangs, and alcoves are provided. c) Overhang over entry projects 5 feet to protect pedestrians. d) Shelter over main entry is extension of roof with same roof slope. 		
B.3.	Building Materials	a) Building is architecturally unified by palette of earth tone material colors, continuous gabled roof form, and repeated dormer/pop-out language.		

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B.4. Colors	 b) Building has a 36-inch base of Ebony colored, split-faced concrete block veneer with running bond pattern. Type II adjustment, based on notes from pre-application meeting: Percentage of gaps in base material is 18%. Please see Base Material Diagram on Sheet G1.30. c) Foundation is sheathed with the split-faced concrete block veneer. d) Siding above veneer base consists of horizontal wood textured fiberboard sizing (redwood color), vertical ribbed fiberboard panels (1 5/8" ribs and weathered copper color) e) Building elevations facing a public right-of-way or civic space incorporate the following features: Wood door and window trim and fascia Metal canopies Metal brackets – these are cosmetic metal applied to the ends of the extruded framed walls, labeled "break metal trim" on the exterior elevations f) Materials required on elevations visible from abutting public streets turn the corner and are consistent around the full perimeter of the building. a) Color palette is warm earth tones and wood look. Material colors are noted in B.3. section above. Exterior paint for trim and fascia is Miller Historic color H119 Sturgis Gray b) Black color is only used for metal canopies
C Roof Pitch, Materials, and	c) No day-glow or reflective colors are used.
Parapets	
C.1. Gabled Roof Pitch C.2. Secondary Roof Forms	 Primary roof forms are 6:12, except at the east roof. East roof is 4 feet wider than the rest of the roofs, so the pitch is 5 5/8:12 to allow the ridges to be at the same level. 6:12 pitch is only required for new buildings with a span of 50 feet or less. Portion of roofing at 5 5/8:12 is 62'-8" wide due to building program needs. Secondary roof forms are 4 1/2:12. Secondary roof forms comprise of 13% of roof area. (1,514 secondary roof area, 11,624 total roof area)
C.3. Gable	Gable ends of the roof face Hwy 26, the intersection
C.S. Gable	of Hwy 26 and SE Ten Eyck Road, and the parking lot. The gable facing the parking lot, and part of the main entrance, is visible from Pleasant Street.
C.4. Secondary Roof Form Quantities	• (2) secondary roof forms on the 76'-7" length of roof facing Ten Eyck. (2) secondary roof forms on the 114'-11" length of roof facing Pleasant Street.
C.5. Roof Materials	Roofing is a standing seam metal roof, color is gray.
C.6. Roof and Wall Mounted Equipment	 There is no rooftop equipment other than an approximately 12" tubular skylight centered on the roof. Mechanical and electrical equipment is internal in dedicated rooms and in the attic space.

D Ent	Building Orientation and		
D.1.	Orientation	•	More than 50% of the building's street frontage is within 10 feet or a sidewalk or civic space. The edges of the building are as close to the property line as allowed. No off-street parking is placed between the building and adjacent streets.
D.2.	Parking Placement	•	Not applicable
D.3.	Ground Floor Connection	•	Ground floor spaces are connected to the sidewalks along Pleasant Street and Hwy 26.
D.4.	Corner Entrance	•	There is a door into the building within 40 feet of the corner at the intersection of Ten Eyck and Hwy 26, and an door into the building within 40 feet of the corner at the intersection of Ten Eyck and Pleasant Street. A direct corner entrance is not practical due to the nature of the building's use as a health clinic and its relation to the parking lot. The corners have detailing consistent with the Sandy Style.
D.6.	Activated Pedestrian Environment on two Elevations	•	There is an entrance with a pedestrian shelter facing Hwy 26 and facing Pleasant Street, however, due to the nature of the clinic, these are staff entrances, not customer entrances. The patient entrance faces the parking lot. Patients may leave the other (2) doors, but these are primarily intended for clinic staff.
D.7.	Primary Entry Spacing	•	Due to the nature of the medical clinic, entrances are spaced further than 30' apart. There is no public retail as a part of this building.
D.8.	Primary Entrance Architecture	•	The roof overhangs the main entrance by 5' and there is a bench and landscaped elements to emphasize it. There is a metal canopy over the other entrances, with landscaping near these entries.
Е	Windows		
E.1.	Unified Design	•	There are only 4 different sizes of windows in this design, and their headers, sills, and mullions are in consistent planes in relation to each other.
E.2.	Ground Floor Windows	•	Type II adjustment: Percentage of window area on Hwy 26 elevation is 27%. Percentage of window area on SE Ten Eyck Road elevation is 28%. Percentage of window area facing Pleasant street is 23%. Due to the use of the building as a clinic, it is not practical to have 40% windows on (2) of these frontages. The building GSF is just shy of 10,000 SF, which only requires 25% window area, which we are meeting on (2) frontages. a) Typical windows have a sill 3 feet above grade. b) Windows are square and vertically oriented. c) Windows are divided into panes that are smaller than 6 feet. d) Windows have 4 inch wood trim around them.
E.4.	Prohibited Windows	•	a) None of the windows are darkly tinted or mirrored.

		b) Storefront windows are located at the entrance. The rest of the windows are vinyl.
F Des	Landscaping and Streetscape sign	
F.1.	Landscape and Screening General Standards (Chapter 17.92)	Please see Chapter 17.92 sections in the Zoning Requirements Narrative above.
F.2.	Streetscape Design Conflicts	There are no conflicts with the Streetscape design and Landscaping and Screening General Standards.
G	Civic Space	
G.1.	Percent of Ground Floor Area	• The civic space near the main entry to the clinic is 3% of the ground floor area. (320 SF / 9,381 SF).
G.2.	Dimensions and Area	The civic space is 19'-8" across and 320 SF.
G.3.	Туре	The civic space is an extension of the sidewalk in front of the clinic entrance, with benches for seating, and doubles as a zone for patients to await pick-up.
G.4.	Location	The civic space is located roughly mid-block, near the entrance, which will be a zone with higher pedestrian activity.
G.5.	Adjacency to Right-of-Way	The civic space is directly adjacent to the sidewalk on Pleasant Street, with rectangular stone pavers to identify it. This space is not gated or otherwise closed to public access.
Н	Lighting	
H.1.	Chapter 15.30, Dark Sky Ordinance	Streetscape lighting conforms to the Downtown Sandy Streetscape Design and Dark Sky Ordinance. See sheet E1.02 – Electrical Site Lighting Plan. The area 10 feet beyond the property line receives no more than 0.25 of a foot-candle of light and the new lighting does not exceed 4,125 Kelvins.
H.2.	Integration	Site lighting is situated to highlight the architectural design of the clinic and to compliment the site lighting at the nearby police station.
H.3.	Safety	Exterior can lights are integrated into the metal canopies over the entries. Walkways, parking lot, and entries are illuminated at 1.5-2.0 foot candles: see sheet E1.02 – Electrical Site Lighting Plan.
Ι	Safety and Security	
I.1.	Windows	Windows are located around the full perimeter of the building, facing pedestrian, parking, and loading areas.
I.2.	Interior Surveillance	Windows are located so interior activity by be seen from all public right-of-ways, however, due to the nature of the building as a medical clinic, internal shades will be used to provide patients and staff with privacy as needed. The police station is also right

			next to the clinic, which will aid in surveillance of the site.
I.3.	Street Address	•	8" tall street address numbers are near south entry, near the intersection of Hwy 26 and Pleasant Street, shown on sheet A3.11, elevation 6.
I.4.	On-Site Lighting Orientation	•	Site lighting is placed to provide adequate surveillance of on-site activities. See sheet E1.02 – Electrical Site Lighting Plan.
J	External Storage and Screening		
J.1.	Exterior Storage	•	There will be no exterior storage of merchandise or materials.
J.3.	Equipment Screening	•	Mechanical condensing unit and transformer are screened from view with wood landscape fencing. Garbage storage is screened within trash enclosure.
J.4.	Trash Screening	•	Trash and recycling storage is in a split face CMU enclosure in the southeast corner of the site. Enclosure CMU matches the color of the concrete block veneer base of the building. And the metal roof of the trash enclosure matches the metal roofing color.

-1:60 Vicinity Map

-Existing Site Survey

-Site Hardscape Plan

-Site Plan

E. Architectural Drawings:

-Floor Plan

-Roof Plan

-Trash Enclosure / Site Details

-Window Area and Base Calculations

-Photometric Site Plan

-Traffic Impact Analysis Letter

-Stormwater Utility Narrative

Cover Sheet A. Site Analysis: -500 Foot Radius B. Site Plan: -Site Demolition Plan

C. Grading Plan

D. Utility Plan

-Building Elevations
-Building Sections

-(3) Renderings

F. Exterior Lighting Plan:
-Electrical Symbol Legend
-Lighting Fixture Schedule

-Electrical Site Plan

G. Landscape Plan (Landscape Plan + (3) Supplemental Information Sheets)
H. Other Submissions:

-Light Fixture Cut Sheets: S1 through S7-Exterior Building Materials

AMA TEAM

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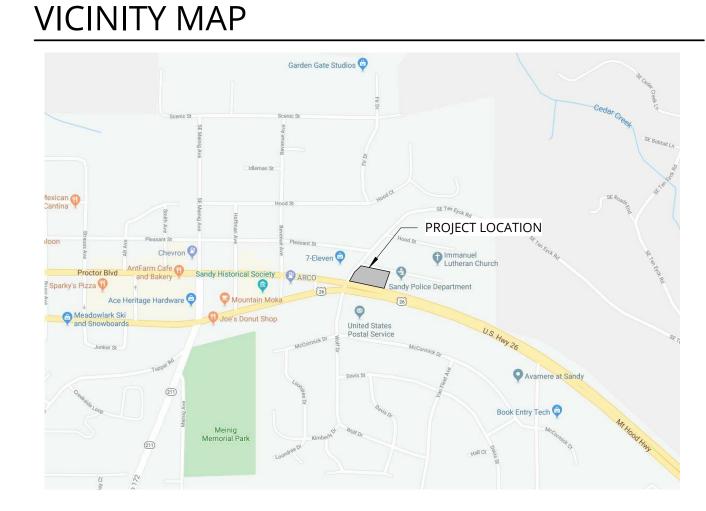
sshanks@kclengineering

mkelly@kclengineering.com

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sshanks@kclengineering

<u>OWNER</u>	
CLACKAMAS COUNTY	
2051 KAEN ROAD	503.655.859
OREGON CITY, OR 97045	www.clackamas.us/communitydevelopmer
PROJECT COORDINATOR	503.650.566
STEVE KELLY	stevekel@clackamas.u
FQHC DIRECTOR	503.655.859 ⁻
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OWNER/OPERATIONS	
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ODECON CITY OD 0704F	www.clackamas.u
OREGON CITY, OR 97045	
TECHNOLOGY SERVICES MGR	503.655.882
,	503.655.882 ronaldsan@clackamas.u
TECHNOLOGY SERVICES MGR	





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CENTER SANDY HEALTH 39831 HIGHWAY 26 SANDY, OR 97055

REASON FOR ISSUE

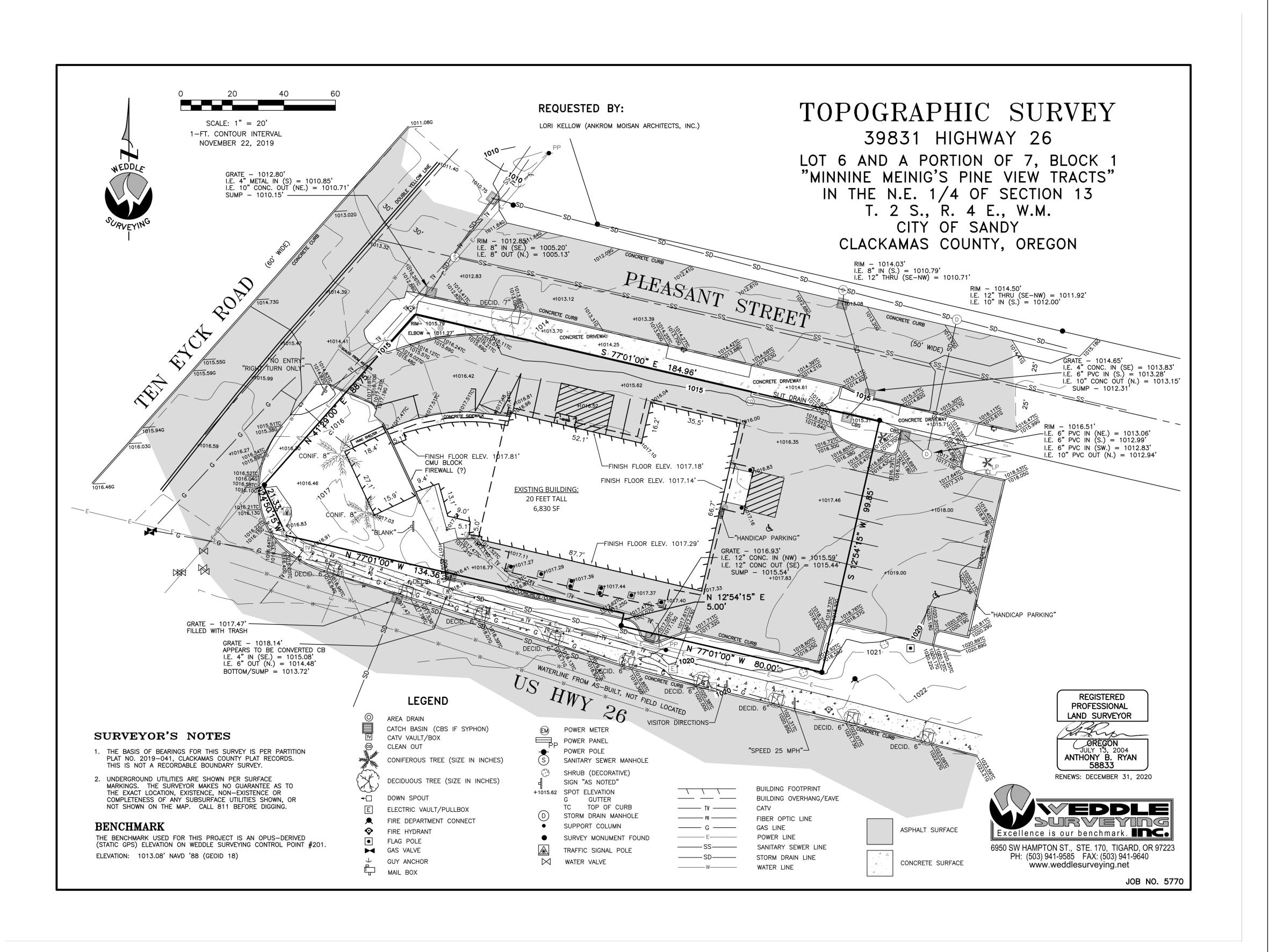
COVER SHEET

DESIGN REVIEW

PROJECT NUMBER 192530 DATE 4.3.2020

SHEET NUMBER

CS



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HEALTH CLINIC

SANDY

DATE REASON FOR ISSUE

N DATE REASON FOR ISSO

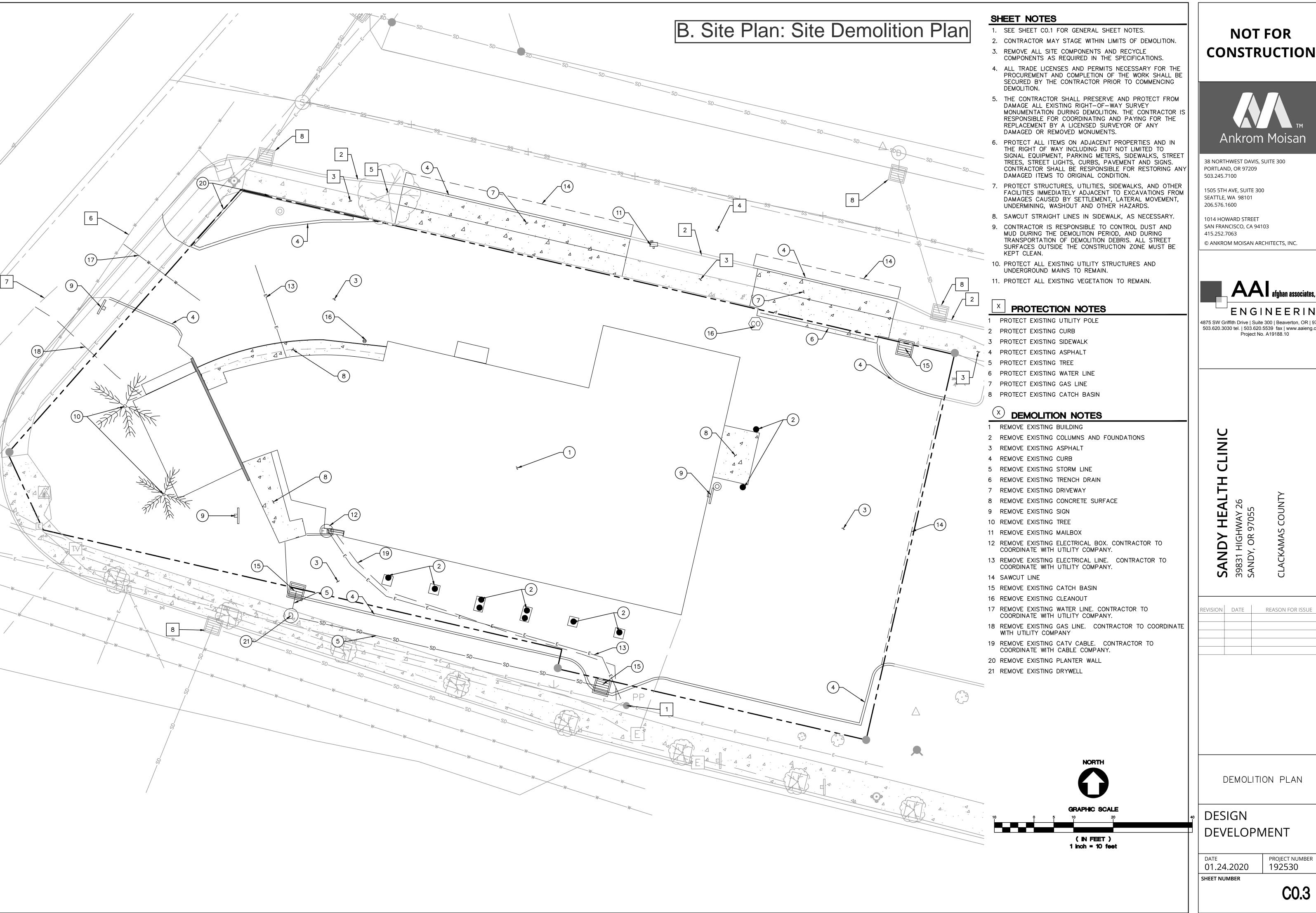
SURVEY

DESIGN
DEVELOPMENT

DATE PROJECT NUMBER 1.24.2020 192530

SHEET NUMBER

G0.11



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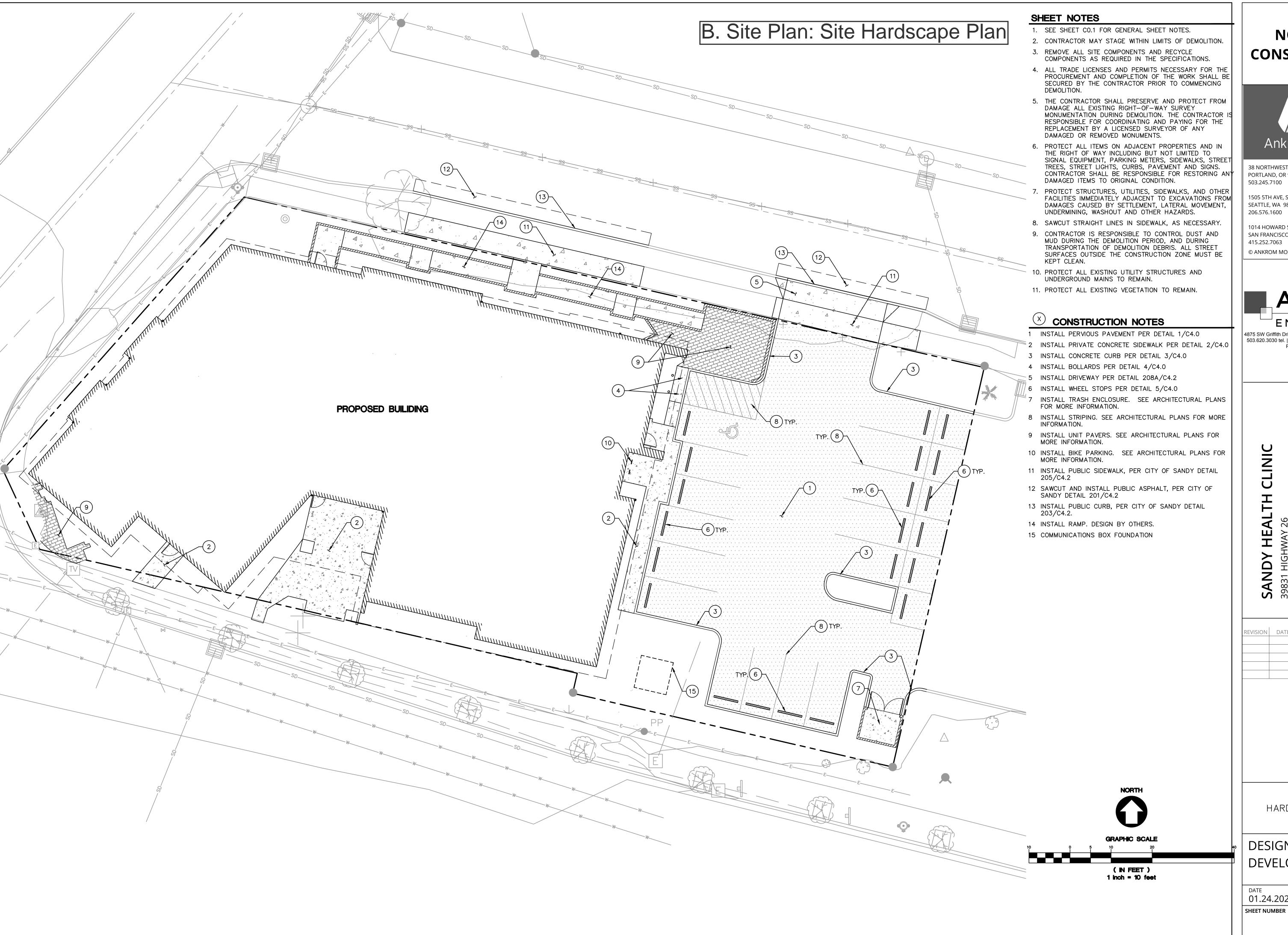


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REASON FOR ISSUE

DEMOLITION PLAN

DEVELOPMENT



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Project No. A19188.10

REVISION DATE **REASON FOR ISSUE**

HARDSCAPE PLAN

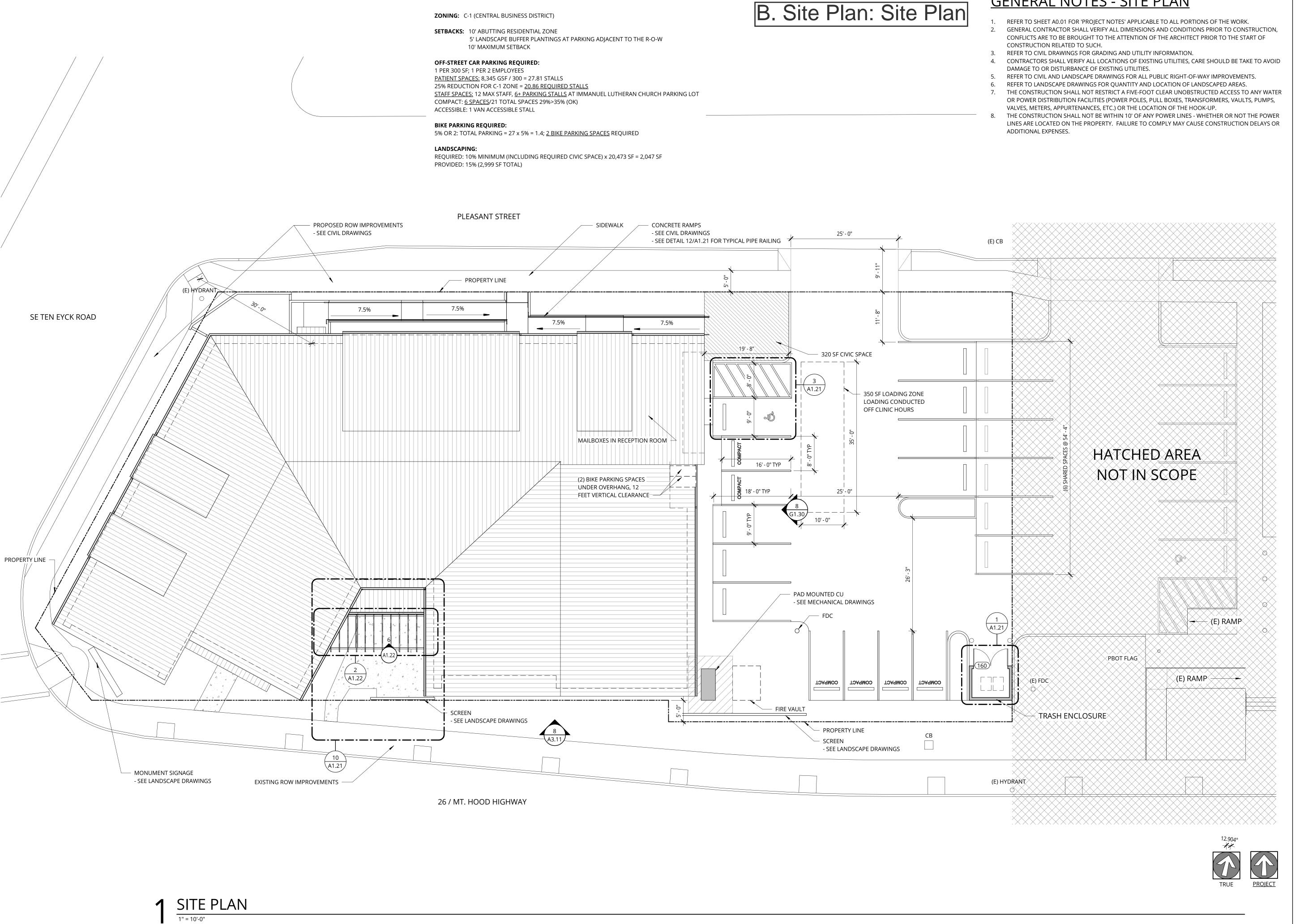
DESIGN DEVELOPMENT

01.24.2020

192530

PROJECT NUMBER

C1.0



GENERAL NOTES - SITE PLAN NOT FOR

Ankrom Moisan

CONSTRUCTION

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REASON FOR ISSUE

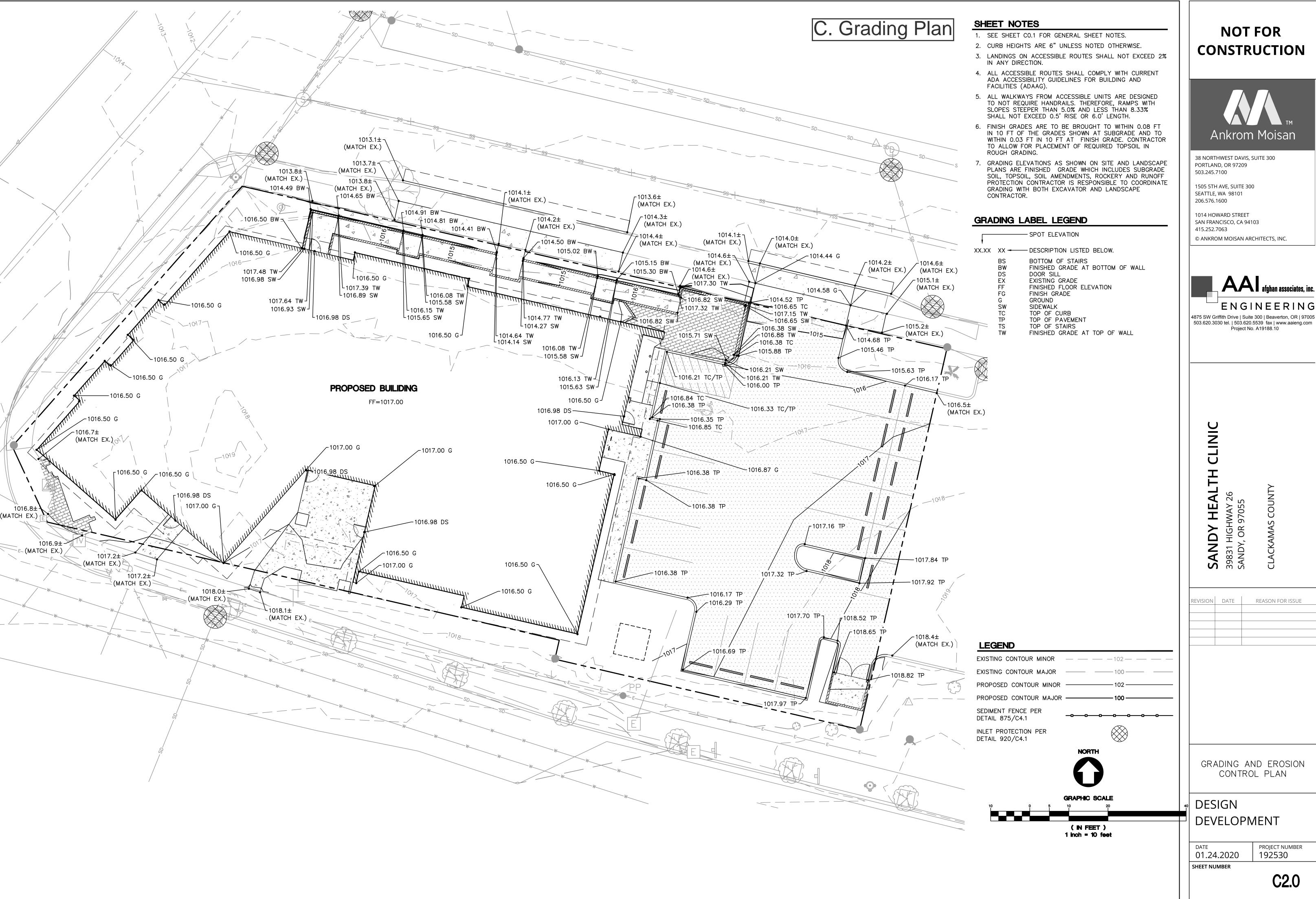
SITE PLAN

DESIGN REVIEW

DATE 4.3.2020

PROJECT NUMBER 192530

A1.01



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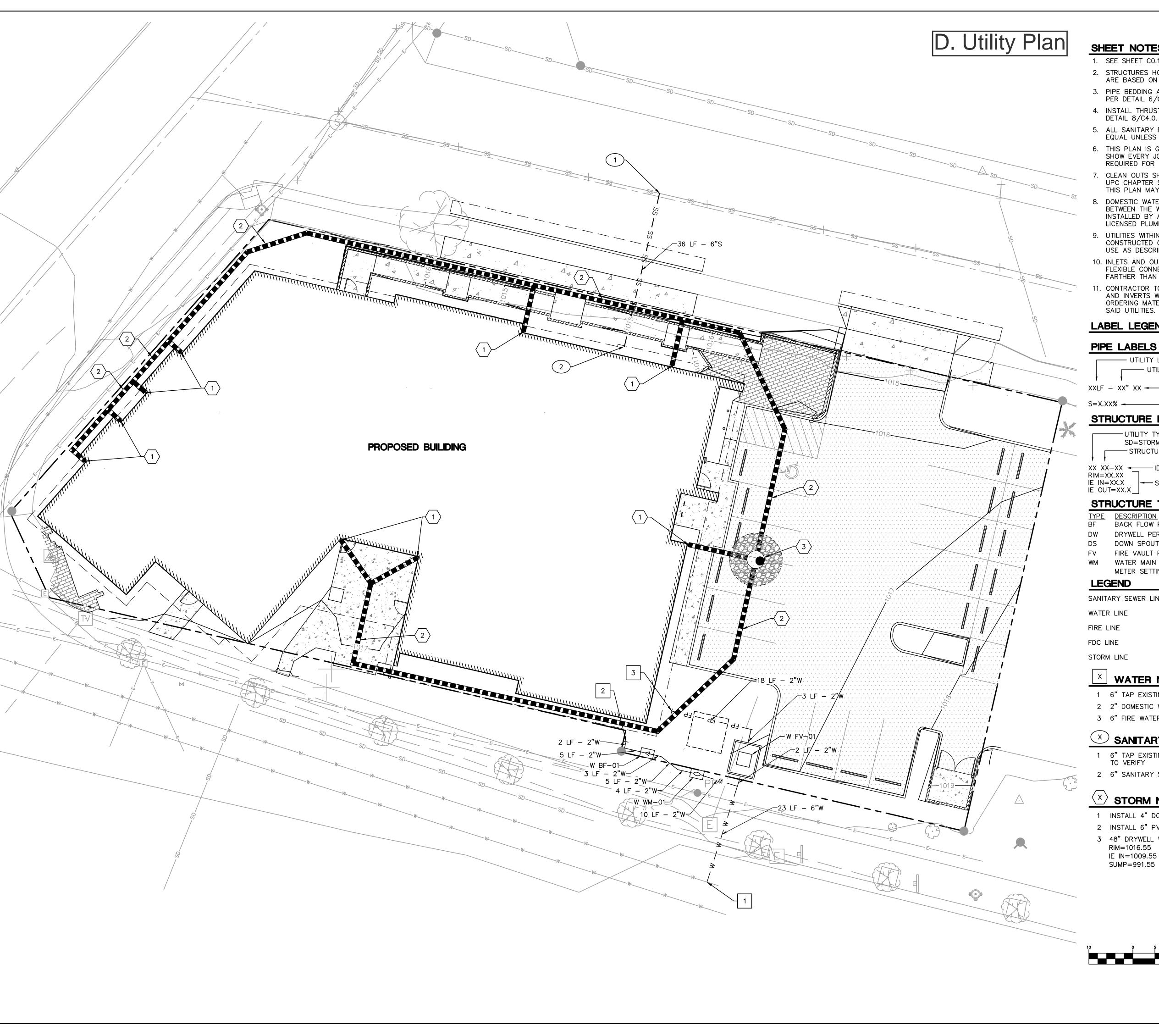
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REASON FOR ISSUE

GRADING AND EROSION

DEVELOPMENT

192530



SHEET NOTES

- 1. SEE SHEET CO.1 FOR GENERAL SHEET NOTES.
- 2. STRUCTURES HORIZONTAL LOCATIONS AND PIPE INVERTS ARE BASED ON THE CENTER OF THE STRUCTURE.
- 3. PIPE BEDDING AND BACKFILL UTILITIES SHALL BE DONE PER DETAIL 6/C4.0.
- 4. INSTALL THRUST BLOCKS ON FIRE AND WATER LINES PER DETAIL 8/C4.0.
- 5. ALL SANITARY PIPING SHALL BE PVC 3034 OR APPROVED EQUAL UNLESS NOTED OTHERWISE.
- 6. THIS PLAN IS GENERALLY DIAGRAMMATIC. IT DOES NOT SHOW EVERY JOINT, BEND, FITTING, OR ACCESSORY REQUIRED FOR CONSTRUCTION.
- 7. CLEAN OUTS SHALL BE INSTALLED IN CONFORMANCE WITH UPC CHAPTER SEVEN, SECTION 707 AND SECTION 719. THIS PLAN MAY NOT SHOW ALL REQUIRED CLEAN OUTS.
- DOMESTIC WATER AND FIRE LINES AND ACCESSORIES BETWEEN THE WATER METER AND THE BUILDING SHALL BE INSTALLED BY A LICENSED PLUMBER EMPLOYED BY A LICENSED PLUMBING CONTRACTOR.
- 9. UTILITIES WITHIN FIVE FEET OF A BUILDING SHALL BE CONSTRUCTED OF MATERIALS APPROVED FOR INTERIOR USE AS DESCRIBED IN THE CURRENT EDITION OF THE UPC.
- 10. INLETS AND OUTLETS TO ON-SITE MANHOLES SHALL HAVE FLEXIBLE CONNECTION NO CLOSER THAN 12" AND NO FARTHER THAN 36" FROM THE MANHOLE.
- 11. CONTRACTOR TO VERIFY SANITARY AND WATER SIZING AND INVERTS WITH APPROVED PLUMBING PLANS PRIOR TO ORDERING MATERIALS OR BEGINNING CONSTRUCTION OF

LABEL LEGEND

— UTILITY LENGTH

— UTILITY SIZE

XXLF - XX" XX - UTILITY TYPE

S=X.XX% - SLOPE (WHERE APPLICABLE)

STRUCTURE LABELS

-UTILITY TYPE (FP=FIRE PROTECTION, S=SANITARY, SD=STORM DRAINAGE, W=WATER) - STRUCTURE TYPE (SEE BELOW)

XX XX-XX - ID NUMBER (WHERE APPLICABLE) STRUCTURE INFO (WHERE APPLICABLE)

STRUCTURE TYPES

DESCRIPTION BF BACK FLOW PER DETAIL 7/C4.0

DW DRYWELL PER DETAIL 9/C4.0

FIRE VAULT PER DETAIL 414/C4.2

WATER MAIN PER CITY OF SANDY DETAIL WATER METER SETTING DETAIL ON SHEET C4.2

SANITARY SEWER LINE — FDC — FDC — FDC —

WATER NOTES

- 1 6" TAP EXISTING WATER MAIN
- 2 2" DOMESTIC WATER STUB
- 3 6" FIRE WATER STUB

) SANITARY NOTES

- 1 6" TAP EXISTING MAIN 6" IE = 101075 MIN. CONTRACTOR TO VERIFY
- 2 6" SANITARY STUB IE = 1011.50

STORM NOTES

- 1 INSTALL 4" DOWNSPOUT @ 1%
- 2 INSTALL 6" PVC @ 1%
- 3 48" DRYWELL WITH 12' ANNULUS ROCK RIM=1016.55 IE IN=1009.55 (N, S, W)



GRAPHIC SCALE (IN FEET) 1 inch = 10 feet

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CLINIC

REVISION DATE **REASON FOR ISSUE**

UTILITY PLAN

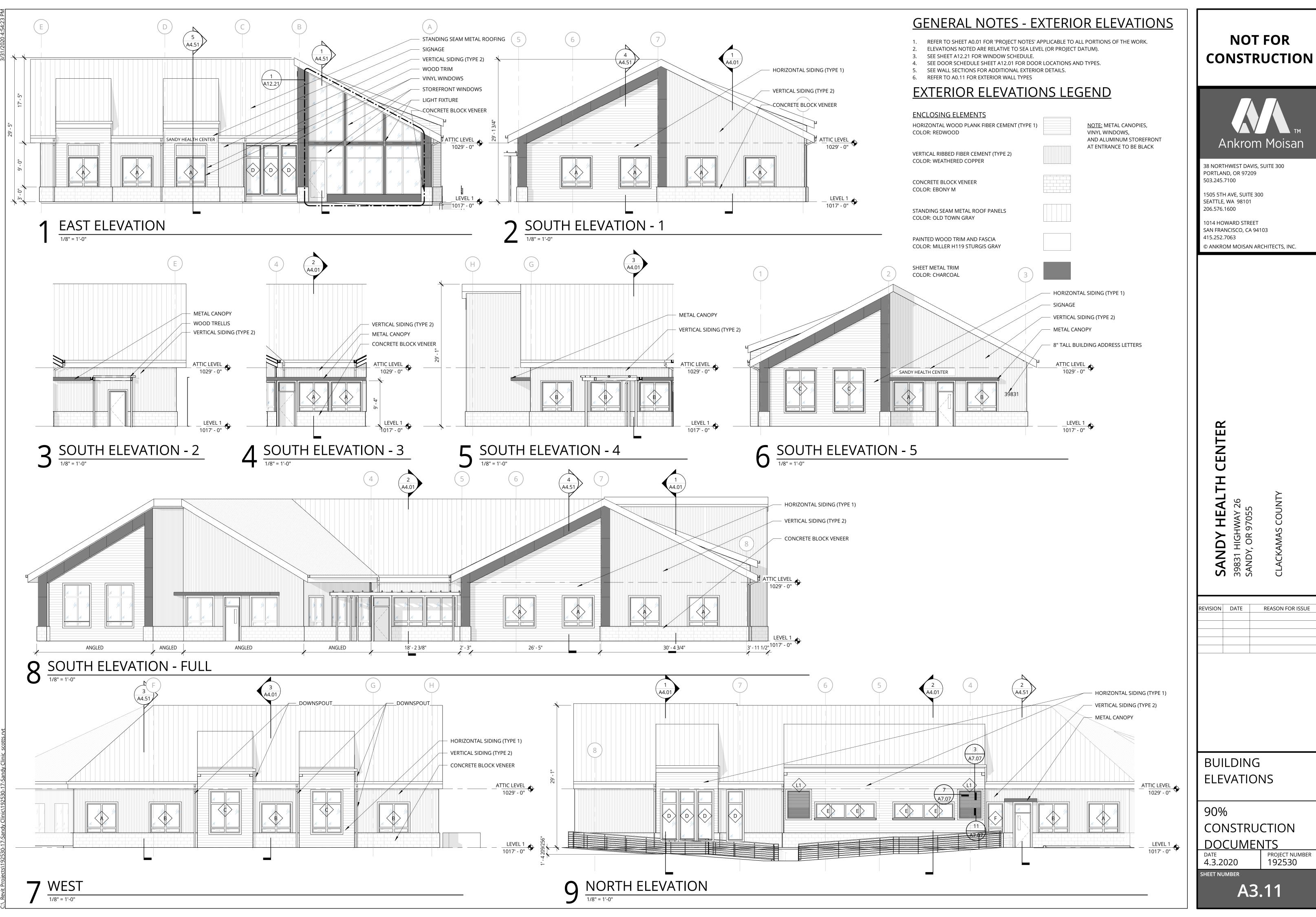
DESIGN DEVELOPMENT

01.24.2020 SHEET NUMBER

C3.0

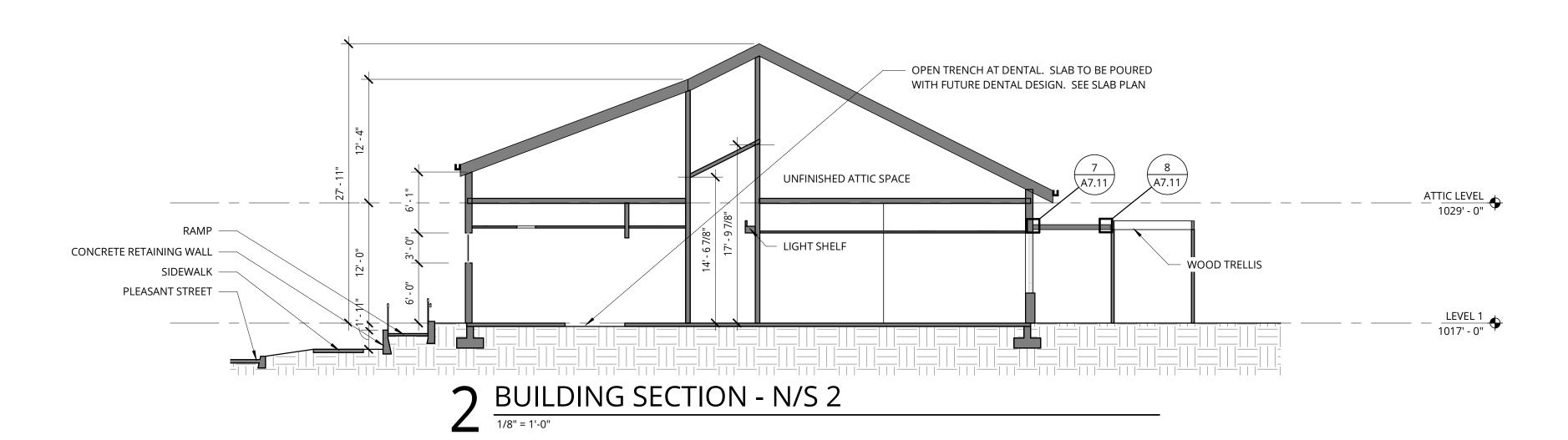
PROJECT NUMBER

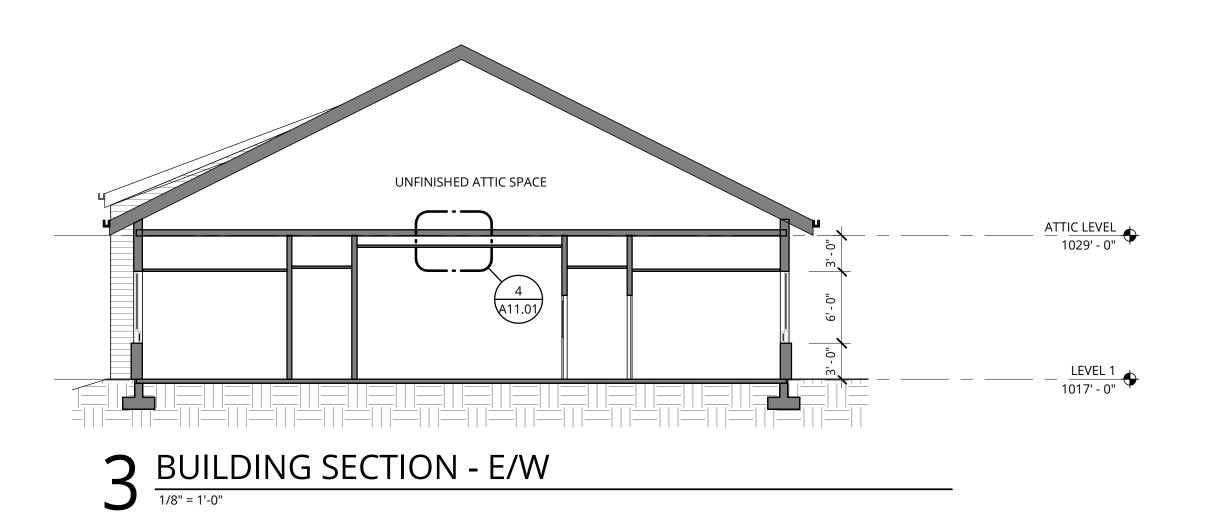
192530



E. Architectural Drawings: Building Sections

EXPOSED WOOD TRUSS CEILING UNFINISHED ATTIC SPACE ATTIC LEVEL 1029' - 0" - 26 / MT. HOOD HIGHWAY CONCRETE RETAINING WALL - SIDEWALK PLEASANT STREET LEVEL 1 1017' - 0" **BUILDING SECTION - N/S 1**





GENERAL NOTES - BUILDING SECTIONS

- REFER TO SHEET A0.01 FOR 'PROJECT NOTES' APPLICABLE TO ALL PORTIONS OF THE WORK. ELEVATIONS NOTED ARE RELATIVE TO SEA LEVEL (OR BUILDING DATUM).
- 3. SEE SHEET A12.21 FOR WINDOW SCHEDULE.
- 4. SEE ENLARGED ELEVATIONS AND WALL SECTIONS FOR ADDITIONAL EXTERIOR DETAILS.

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BUILDING SECTIONS

DESIGN DEVELOPMENT

DATE 1.24.2020

PROJECT NUMBER 192530

A4.01

GENERAL NOTES - FLOOR PLANS

- 1. REFER TO SHEET A0.01 FOR 'PROJECT NOTES' APPLICABLE TO ALL PORTIONS OF THE WORK. 2. PRIOR TO FRAMING VERIFY THAT FINAL APPLIANCE AND PLUMBING FIXTURE SIZES/CLEARANCES MATCH
- THOSE USED AS BASIS OF DESIGN SHOWN ON DRAWING A5.41.
- 3. REFERENCE SLAB PLAN FOR CONCRETE WALL LOCATIONS, UNO. COORDINATE WITH STRUCTURAL DRAWINGS.
- 4. SEE SHEETS A0.11 & A0.21 FOR WALL ASSEMBLIES.
- SEE SHEET A0.41 FOR TYPICAL FRAMING AND ACOUSTICAL DETAILS.
- 6. SEE FIRE/LIFE SAFETY SHEET ON G2.21 FOR LOCATIONS OF FIRE EXTINGUISHER CABINETS. REFER TO ENLARGED AREA PLANS (A5.11 SERIES) FOR DETAILED INFORMATION WITHIN EACH SECTOR
- REFER TO STRUCTURAL DRAWINGS FOR COLUMNS, SHEAR WALL AND BEAM SIZES.
- 9. DIMENSIONS ARE TO FACE OF STUD, UNLESS NOTED OTHERWISE. 10. CORRIDORS TO MAINTAIN 5'-0" FINISH TO FINISH CLEARANCE, MINIMUM.

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REASON FOR ISSUE

FLOOR PLAN

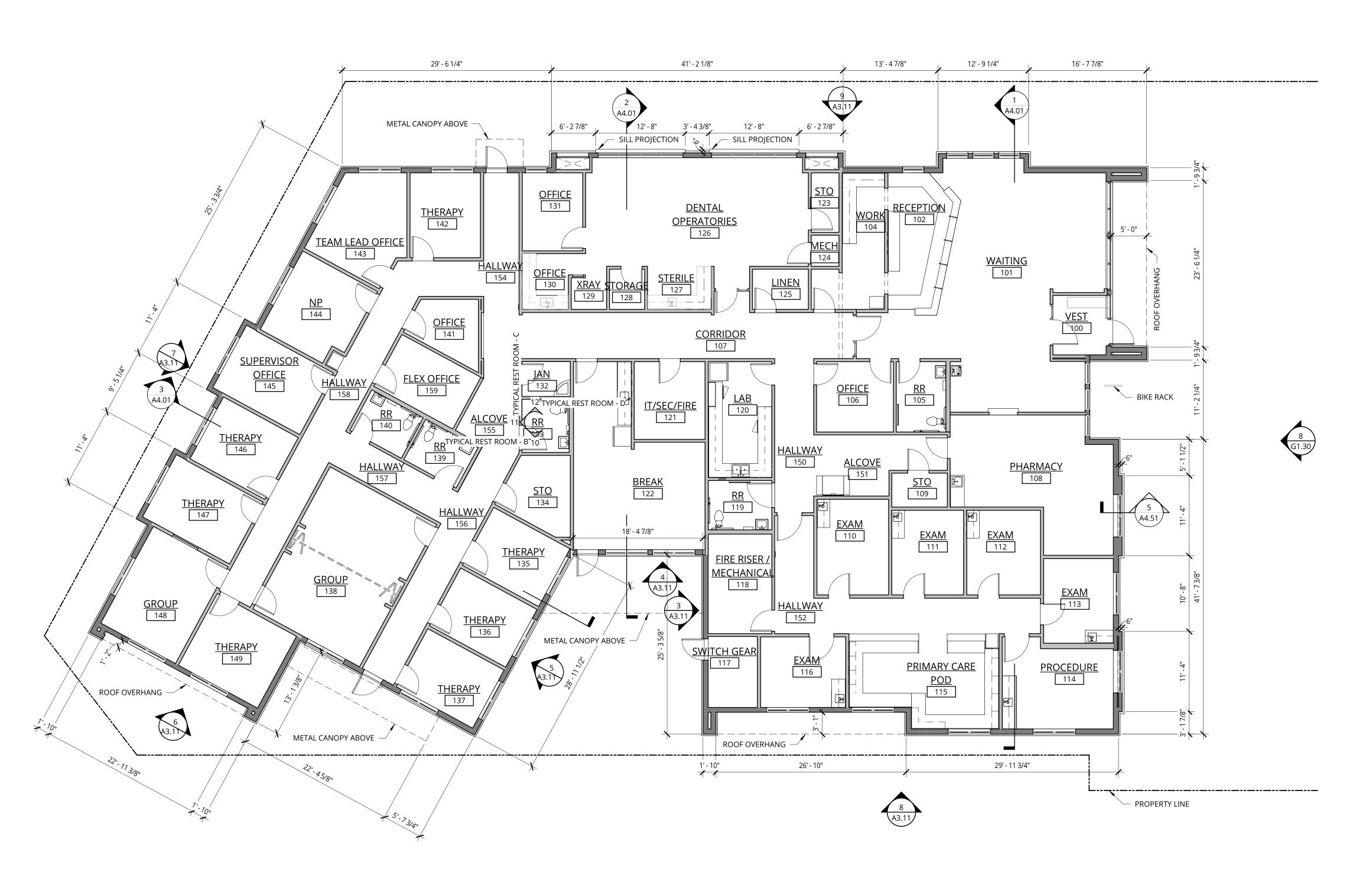
90% CONSTRUCTION

DOCUMENTS

DATE PROJECT

4.3.2020 1925 PROJECT NUMBER 192530

G0.34





GENERAL NOTES - ROOF PLANS

- 1. REFER TO SHEET A0.01 FOR 'PROJECT NOTES' APPLICABLE TO ALL PORTIONS OF THE WORK.
- 2. SEE SHEET A0.31 FOR HORIZONTAL ASSEMBLIES.
- PROVIDE POSITIVE ROOF SLOPE TO DRAIN AT MINIMUM SLOPE OF 1/4" PER FOOT MEASURED ALONG VALLEYS, UNLESS NOTED OTHERWISE.
 ROOF PENETRATIONS SHOWN ARE SCHEMATIC IN NATURE; COORDINATE ACTUAL SIZE, TYPE AND
- 4. ROOF PENETRATIONS SHOWN ARE SCHEMATIC IN NATURE; COORDINATE ACTUAL SIZE, TYPE AND LOCATION OF EQUIPMENT, CURBS, AND ANY OTHER ROOF PENETRATIONS THAT MAY BE REQUIRED TO SUPPORT, SECURE OR FLASH ROOFTOP EQUIPMENT.
- 5. COMPLY WITH THE MOST STRINGENT OF SMACNA, NRCA OR MANUFACTURERS' REQUIREMENTS FOR FLASHINGS, COPINGS AND OTHER SHEET METAL CONSTRUCTION.
- 6. VERIFY ROOFING MANUFACTURERS MINIMUM REQUIREMENTS FOR LAPPING OF ALL MATERIALS. BRING CONFLICTS WITH ARCHITECTURAL DETAILS TO THE ATTENTION OF THE ARCHITECT PRIOR TO
- 7. SEE MEP DRAWINGS FOR ROOFTOP EQUIPMENT AND PENETRATIONS.





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SAND SAND CLACK

ROOF PLAN

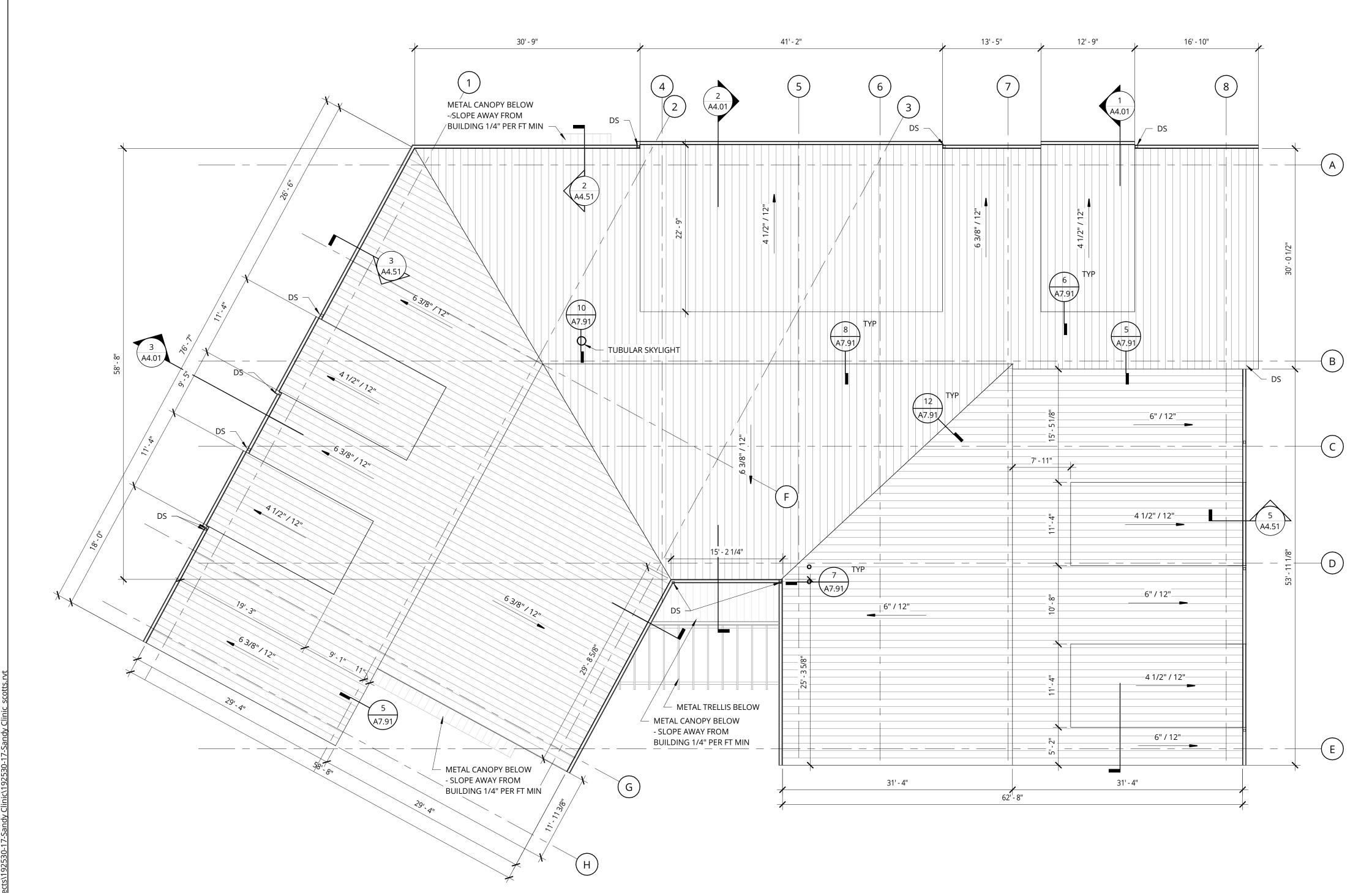
90% CONSTRUCTION

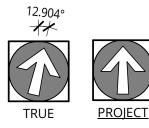
DOCUMENTS

DATE PROJECT NUMBER
4.3.2020 192530

ET NI IMPED

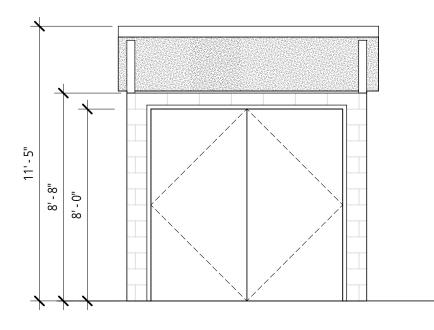
A2.03



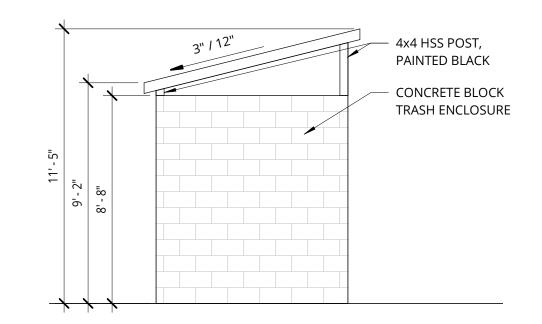


1 ROOF PLAN

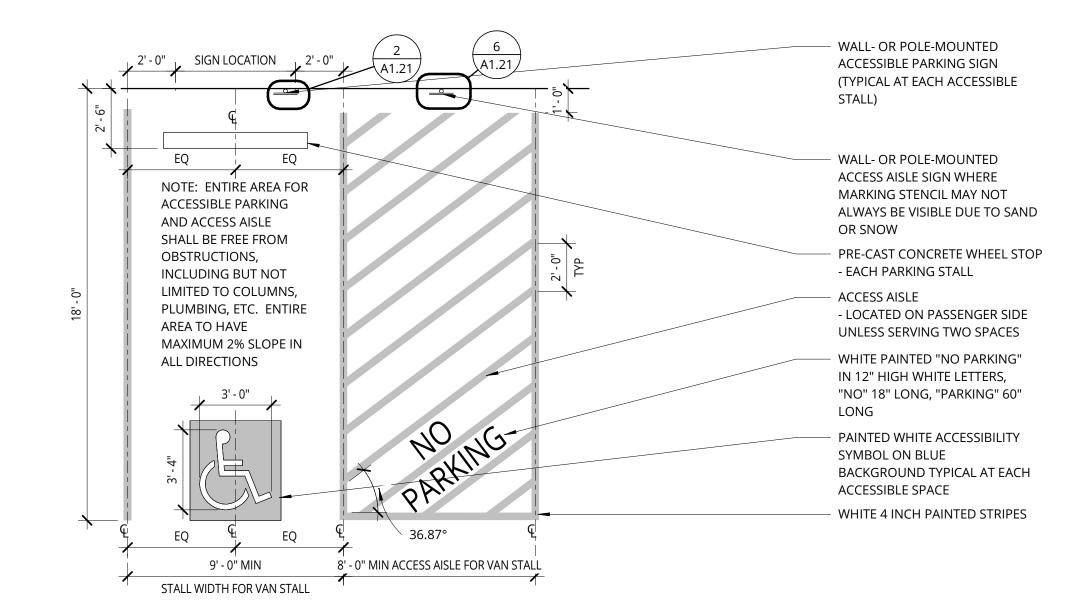
1 TRASH ENCLOSURE



5 TRASH ENCLOSURE FRONT 1/4" = 1'-0"



E. Architectural Drawings: Trash Enclosure / Site Details



ACCESSIBLE PARKING SIGNAGE

SIGN ELEVATION

PARKING

ACCESSIBLE

1' - 6"

2 INCH DIAMETER STEEL POST

- CENTER ON PARKING SPACE

WHITE, RETROREFLECTIVE
SHEETING BACKGROUND WITH
GREEN TEXT AND WHITE ON

LOWER SIGN TO READ

"VAN ACCESSIBLE" (AT VAN

DESIGNATED SPACES ONLY)

WHITE, RETROREFLECTIVE

SHEETING BACKGROUND WITH

WITH CAP

BLUE SYMBOL

GREEN TEXT

- ANCHOR BOLT

- 1/4" DIAMETER (4)

INCH FROM CORNERS

WALKING SURFACE

- 1/4 X 8 X 8 INCH STEEL PLATE

WITH 3/8 INCH HOLES 1 X 1

ALL SIGNS TO COMPLY WITH THE STANDARDS FOR

SIGN

R7-8A

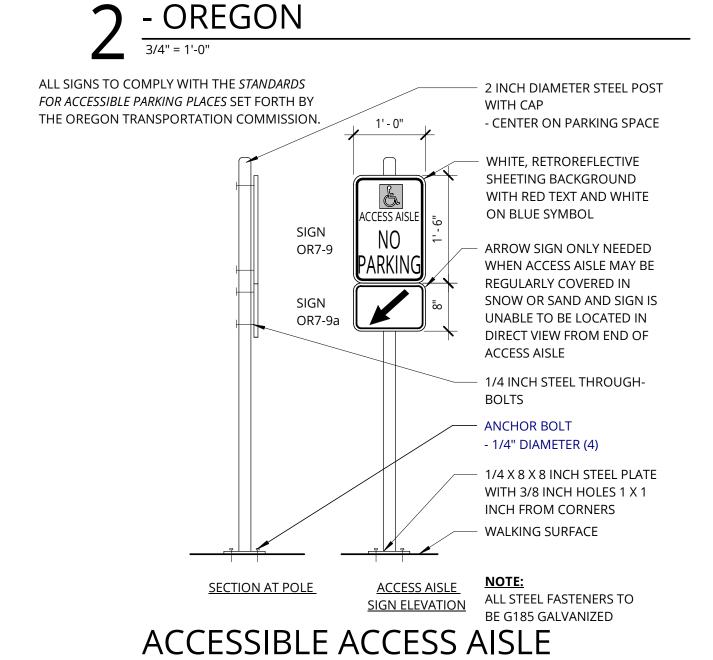
SECTION AT POLE

ACCESSIBLE PARKING PLACES SET FORTH BY THE

OREGON TRANSPORTATION COMMISSION.

1/4 INCH STEEL

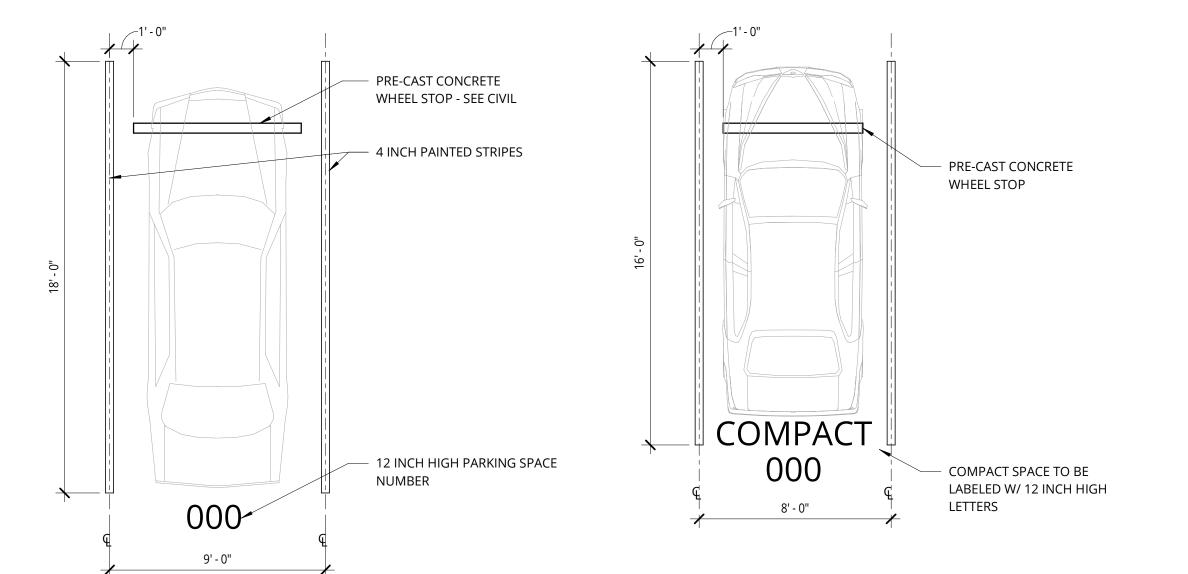
THROUGH-BOLTS



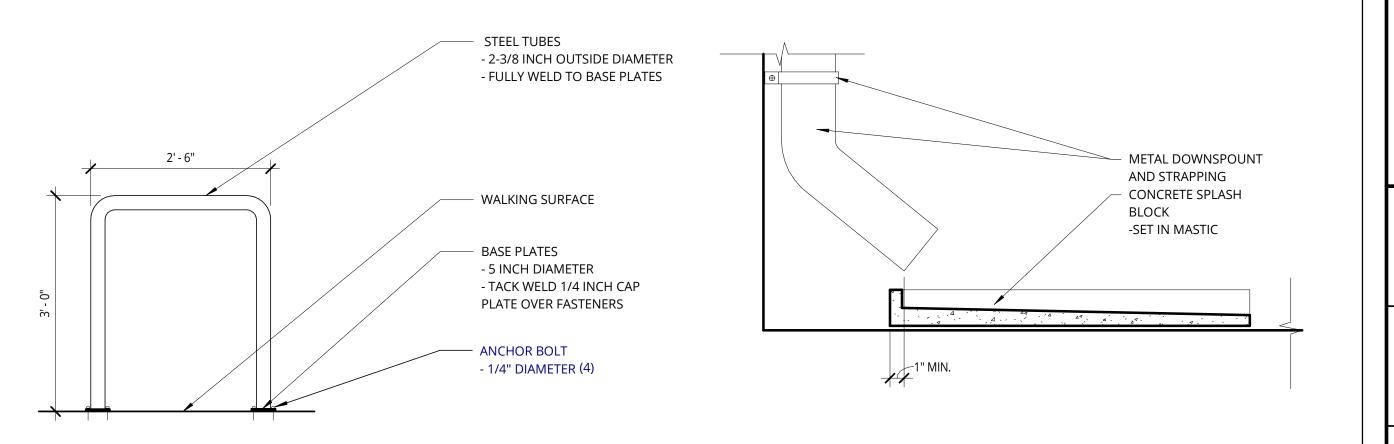
6 SIGNAGE - OREGON

3/4" = 1'-0"

3 ACCESSIBLE PARKING STALL - OREGON



7 STANDARD AND COMPACT PARKING STALL DIMENSIONS - SFO



1 1 BIKE RACK

3/4" = 1'-0"

1 2 SPLASH BLOCK - SECTION

1 1/2" = 1'-0"

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SITE DETAILS

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DATE PROJECT NUMBER 1.24.2020 192530

A1.21

9 TRASH ENCLOSURE SIDE

E. Architectural Drawings: Window Area and Base Calculations

133 SF WINDOW AREA / 505 SF WALL AREA = 26%

3 26 / MT HOOD HWY - WEST A

214 SF WINDOW AREA / 656 SF WALL AREA = 33%

26/MT HOOD HWY TOTAL: 569 SF WINDOW AREA / 2,082 SF WALL AREA = 27%

4 26 / MT HOOD HWY - WEST B

¹17.90.110.E GROUND FLOOR WINDOWS: 40% OF GROUND FLOOR ELEVATION REQUIRED ON (2) STREET FRONTAGES

144 SF WINDOW AREA / 703 SF WALL AREA = 21%

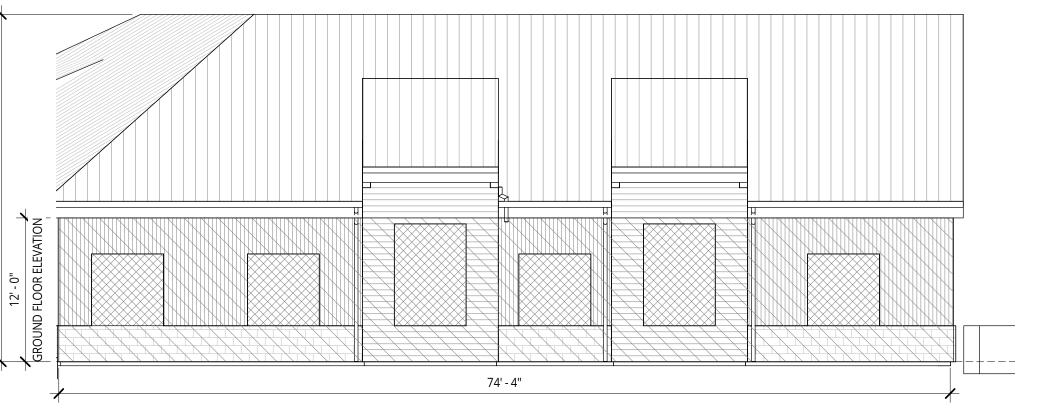
26 / MT HOOD HWY - EAST



78 SF WINDOW AREA / 218 SF WALL AREA = 36%

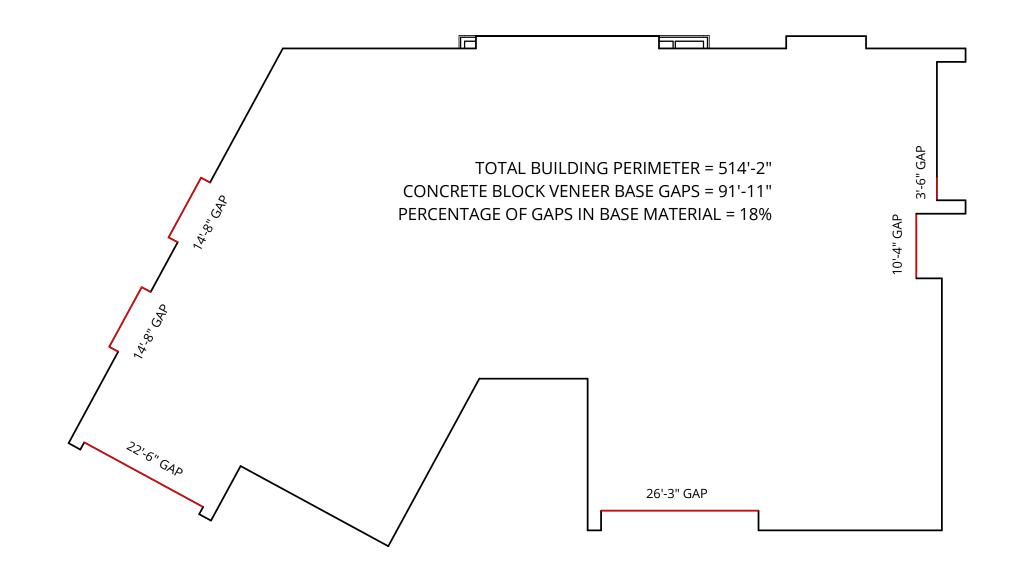
17.90.110.E GROUND FLOOR WINDOWS: 40% OF GROUND FLOOR ELEVATION REQUIRED ON (2) STREET FRONTAGES 424 SF WINDOW AREA / 983 SF WALL AREA = 43%

8 EAST ELEVATION WINDOWS 1/8" = 1'-0"



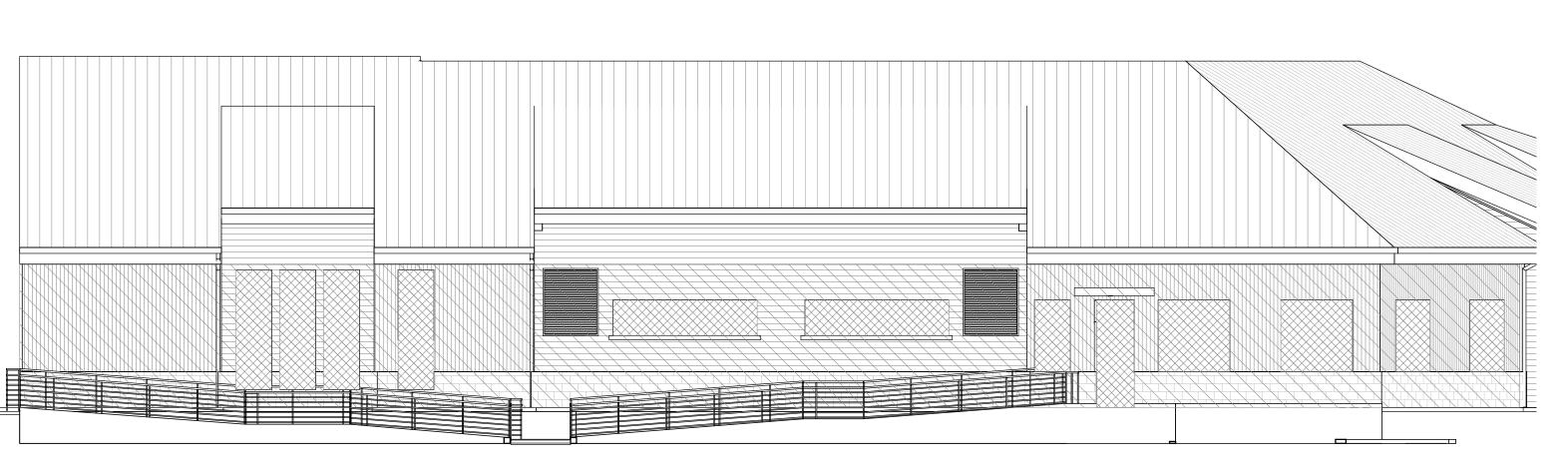
17.90.110.E GROUND FLOOR WINDOWS: 40% OF GROUND FLOOR ELEVATION REQUIRED ON (2) STREET FRONTAGES 246 SF WINDOW AREA / 895 SF WALL AREA = 28%

5 SE TEN EYCK ROAD GROUND FLOOR WINDOWS 1/8" = 1'-0"



7 BASE MATERIAL DIAGRAM

1/16" = 1'-0"



17.90.110.E GROUND FLOOR WINDOWS: 40% OF GROUND FLOOR ELEVATION REQUIRED ON (2) STREET FRONTAGES **345 SF WINDOW AREA / 1515 SF WALL AREA = 23%**

PLEASANT STREET GROUND FLOOR WINDOWS

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ZONING ELEVATIONS

DESIGN REVIEW

DATE 4.3.2020

PROJECT NUMBER 192530

G1.30

- THE CURRENT ADOPTED EDITION OF THE ELECTRICAL CODE SHALL BE THE STANDARD FOR THE ELECTRICAL INSTALLATION. VERIFY WITH LOCAL OFFICIALS WHEN PERMITS ARE OBTAINED. NOTIFY DESIGN TEAM OF ANY DESCREPANCIES BETWEEN THE PROJECT MANUAL OR DRAWINGS AND THE GOVERNING CODE.
- INSTALLATION SHALL FOLLOW ALL REQUIREMENTS OF THE ADAAG AMERICANS WITH DISABILITIES ACT. REFER TO PROJECT MANUAL AND PROJECT CODE REVIEW SHEET FOR LIST OF ALL
- APPLICABLE CODES.

GENERAL NOTES - ELECTRICAL

- COORDINATE LOCATION/INSTALLATION OF MECHANICAL AND ELECTRICAL WORK WITH ALL OTHER TRADES. NO ASPECT OF A SYSTEM INSTALLATION OR ITS ROUGH-IN SHALL COMMENCE UNTIL PROPER AND TIMELY COORDINATION WITH ALL TRADES ASSOCIATED WITH THE INSTALLATION HAS OCCURRED. ITEMS TO BE COORDINATED SHALL INCLUDE BUT NOT BE LIMITED TO: BUILDING STRUCTURE, SHEET METAL, ALL PIPING SYSTEMS, LIGHT FIXTURES, CONDUITS, CABLE TRAYS, ETC. REFER TO ALL GENERAL, MECHANICAL, AND ELECTRICAL DRAWINGS AND SPECIFICATIONS FOR THIS PROJECT. ANY REWORK OF INSTALLED EQUIPMENT OR SYSTEMS WILL BE AT THE CONTRACTORS EXPENSE.
- NOTE THAT THE ELECTRICAL DRAWINGS ARE ONLY A PORTION OF THE COMPLETE SET OF PLANS CONTRACT DOCUMENTS. THE COMPLETE SET CONTRACT OF DOCUMENTS SHALL BE USED TO DEFINE THE ELECTRICAL SCOPE OF WORK. THIS SHALL INCLUDE, BUT NOT BE LIMITED TO, USING THE ARCHITECTURAL PLANS FOR DIMENSIONS AND DETAILS; EQUIPMENT PLANS FOR ROUGH-IN REQUIREMENTS, AND THE MECHANICAL PLANS FOR EQUIPMENT SIZES AND LOCATIONS.

INSTALLATION NOTES - ELECTRICAL

- CONTRACTOR SHALL FAMILIARIZE THEMSELVES WITH EXISTING CONDITIONS PRIOR TO
- ALL 120V-1 PHASE CIRCUITS EXCEEDING 100 FEET TO CENTER OF LOAD SHALL HAVE
- CONDUCTORS INCREASED TO ACCOUNT FOR VOLTAGE DROP. RACEWAYS AND BOXES ARE SHOWN DIAGRAMMATICALLY ONLY AND INDICATE THE GENERAL AND APPROXIMATE LOCATION. THE LAYOUT DOES NOT NECESSARILY SHOW
- THE LOCATIONS OF INDICATED RUNS INTENDED TO SHOW THE ACTUAL ROUTING OF THE ALL LIGHT FIXTURES, SWITCHES, DEVICES, ETC. ARE SHOWN IN PREFERRED LOCATION. E.C. RESPONSIBLE FOR MODIFYING CONDUIT, HANGERS, CIRCUITING, ETC. TO PROVIDE

THE TOTAL NUMBER OF RACEWAYS OR BOXES FOR THE CIRCUITS REQUIRED, NOR ARE

- A COMPLETE AND OPERATIONAL SYSTEM. ALL RECEPTACLE CIRCUITS SHALL HAVE DEDICATED NEUTRALS PER CODE. PROVIDE A DEDICATED GREEN INSULATED GROUND CONDUCTORS TO ALL DEVICES.
- THE CONDUIT SYSTEM SHALL NOT BE USED AS THE ONLY EQUIPMENT GROUNDING METHOD. DO NOT INSTALL DEVICES BACK TO BACK ON OPPOSITE SIDES OF WALL. MAINTAIN
- MINIMUM OF 8" DISTANCE BETWEEN WHEREVER APPLICABLE. BALANCE THE LOAD ON PANELS AS EVENLY AS POSSIBLE DURING INSTALLATION.
- CIRCUIT NUMBERING SHOWN ON PLANS MAY BE ADJUSTED PROVIDE FINAL TYPED PERMANENT PANEL DIRECTORY AT PROJECT COMPLETION.
- CONTRACTOR SHALL BE RESPONSIBLE FOR OPENINGS IN ALL WALLS CREATED BY THEIR WORK. PENETRATIONS SHALL BE SEALED IN ACCORDANCE WITH THE RATINGS OF THE AFFECTED WALL. REFER TO ARCHITECTURAL CODE PLAN FOR RATED WALLS.

MANUAL FIRE ALARM PULL STATION SMOKE DETECTOR SMOKE DETECTOR WITH 520Hz SOUNDER BASE SMOKE DETECTOR - WALL MOUNTED DUCT SMOKE DETECTOR CARBON MONOXIDE DETECTOR HEAT DETECTOR HORN - WALL MOUNTED COMBINATION HORN WITH STROBE - WALL MOUNTED COMBINATION HORN WITH STROBE - CEILING MOUNTED COMBINATION SPEAKER WITH STROBE - WALL MOUNTED COMBINATION SPEAKER WITH STROBE - CEILING MOUNTED STROBE - WALL MOUNTED STROBE - CEILING MOUNTED SPEAKER - WALL MOUNTED SPEAKER - CEILING MOUNTED FIRE FIGHTER TELEPHONE STATION ADDRESSABLE INPUT MODULE SPRINKLER WATER FLOW SWITCH - ADDRESSABLE INPUT MODULE SPRINKLER VALVE TAMPER SWITCH - ADDRESSABLE INPUT MODULE SPRINKLER POST INDICATOR VALVE TAMPER - ADDRESSABLE INPUT MODULE ADDRESSABLE OUTPUT MODULE SD FAN SHUT DOWN RELAY - ADDRESSABLE OUTPUT MODULE MAGNETIC DOOR HOLD - SURFACE MOUNTED MAGNETIC DOOR HOLD - FLOOR MOUNTED SMOKE DAMPER COMBINATION FIRE/SMOKE DAMPER FIRE ALARM ANNUNCIATOR PANEL FIRE ALARM CONTROL PANEL + EMERGENCY COMMUNICATIONS PANEL

FIRE DETECTION AND ALARM SYMBOLS

GENERAL SYMBOLS E ☐ CONDUIT SLEEVE CONDUIT UP, REFER TO TAG ON DRAWING FOR SIZE CONDUIT DOWN, REFER TO TAG ON DRAWING FOR SIZE CIRCUIT HOMERUN, CONCEALED CONDUIT OR CABLE CIRCUIT HOMERUN, UNDER FLOOR CONDUIT OR CABLE KITCHEN EQUIPMENT TAG NUMBER, REFER TO KITCHEN EQUIPMENT CONNECTION SCHEDULE KEYNOTE

EQUIPMENT IDENTIFICATION TAG. REFER TO EQUIPMENT CONNECTION SCHEDULE

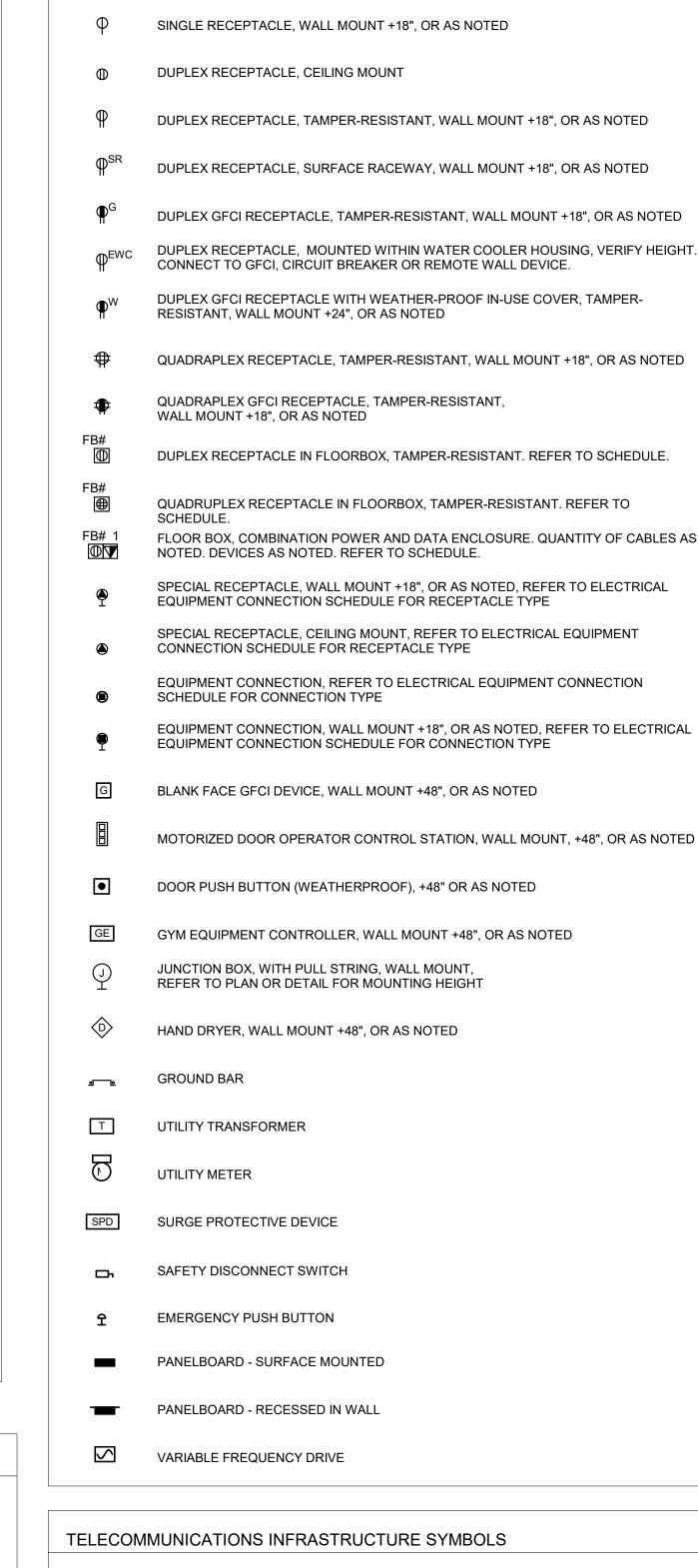
DETAIL DRAWING REFERENCE TAG, SIM-SIMILAR, TYP-TYPICAL, OPP-OPPOSITE

SHEET REFERENCE

SHEET REFERENCE

INTERIOR ELEVATION DRAWING REFERENCE TAG

\ A101 /



VOICE / DATA OUTLET: 4" SQUARE JUNCTION BOX, MUD RING, AND 1"C WITH

SEE RISER DIAGRAM AND SPECIFICATIONS FOR ADDITIONAL REQUIREMENTS

THERMOSTAT JUNCTION BOX ROUGH-IN. WALL MOUNTED +48" OR AS NOTED.

HUMIDISTAT JUNCTION BOX ROUGH-IN. WALL MOUNTED +48" OR AS NOTED.

NOTED. EXTEND 3/4" CONDUIT TO ACCESSIBLE LOCATION ABOVE CEILING.

NOTED. EXTEND 3/4" CONDUIT TO ACCESSIBLE LOCATION ABOVE CEILING.

CARBON DIOXIDE SENSOR JUNCTION BOX ROUGH-IN. WALL MOUNTED +48" OR AS

TERMPERATURE SENSOR JUNCTION BOX ROUGH-IN. WALL MOUNTED +48" OR AS

WIRELESS ACCESS POINT- SEE SCHEDULE FOR EXACT REQUIREMENTS

PULL ROPE TO ACCESSIBLE CEILING SPACE OR MDF ROOM

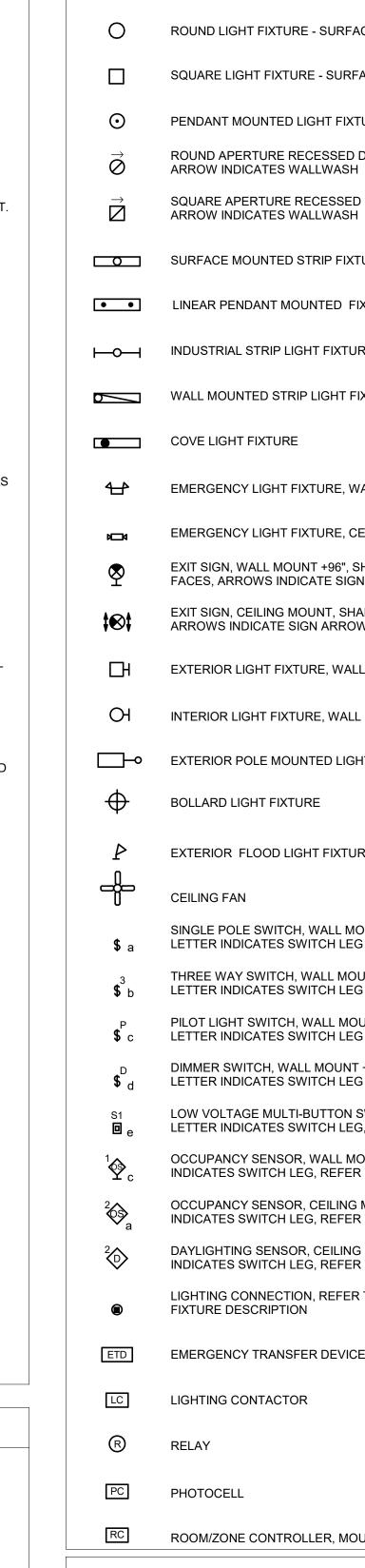
CABLE TELEVISION LOCATION - RADIO GRADE CABLING

TEMPERATURE CONTROLS SYMBOLS - DEVICES PROVIDED BY T.C.C

EXTEND 3/4" CONDUIT TO ACCESSIBLE LOCATION ABOVE CEILING.

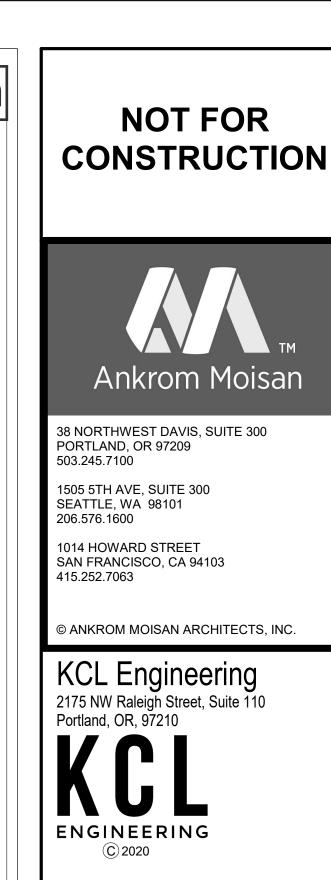
EXTEND 3/4" CONDUIT TO ACCESSIBLE LOCATION ABOVE CEILING.

POWER SYMBOLS





SEE RISER DIAGRAM AND SPECIFICATIONS FOR ADDITIONAL REQUIREMENTS



CLINIC

出

ANDY

REVISION DATE

ELECTRICAL

AND GENERAL

DEVELOPMENT

E0.01

PROJECT NUMBER

192530

SYMBOL LEGEND

REASON FOR ISSUE

GH OR

NOTE: NOT ALL SYMBOLS APPLY TO THIS PROJECT

NIC NOT IN CONTRACT

ON CENTER

OFOI OWNER FURNISHED.

RELOCATED

TELEVISION

VOLT-AMPERES

WIREGUARD COVER

WEATHERPROOF DEVICE

WEATHER RESISTANT DEVICE +24" INDICATES MOUNTING HEIGHT CENTER

TYPICAL

VOLTS

NTS NOT TO SCALE

NM

OC

TCC

WG

WR

NONMETALLIC

OWNER FURNISHED

OWNER INSTALLED

REPLACED WITH NEW

SCCR SHORT CIRCUIT CURRENT RATING

UPS UNINTERRUPTIBLE POWER SUPPLY

TAMPER PROOF DEVICE

CONTRACTOR INSTALLED

EXISTING ITEM TO BE REMOVED

EXISTING ITEM TO BE REMOVED AND

EXISTING ITEM TO BE REMOVED AND

TEMPERATURE CONTROL CONTRACTOR

LINE OF DEVICE TO FINISHED FLOOR

ELECTRICAL ABBREVIATIONS

ABOVE FINISHED FLOOR

ATS AUTOMATIC TRANSFER SWITCH

CURRENT TRANSFORMER

EXISTING ITEM TO REMAIN

ELECTRICAL CONTRACTOR

FAAP FIRE ALARM ANNUNCIATOR PANEL

MECHANICAL CONTRACTOR

FACP FIRE ALARM CONTROL PANEL

FIRE SMOKE DAMPER

KVA KILO-VOLT-AMPERES

MCB MAIN CIRCUIT BREAKER

MDP MAIN DISTRIBUTION PANEL

KILOWATTS

MLO MAIN LUGS ONLY

EMERGENCY LIGHT FIXTURE

NEW LOCATION OF EXISTING ITEM

GROUND FAULT CIRCUIT INTERRUPTER

NEW DEVICE IN EXISTING LOCATION

ROUGH IN FOR FUTURE DEVICE

CIRCUIT BREAKER

CEILING

ER

FSD

MC

GND GROUND

DEVICE MOUNTED +8" ABOVE COUNTER TOP (VERIFY LOCATION)

> SECTION CUT REFERENCE TAG. SIM-SIMILAR. TYP-TYPICAL. OPP-OPPOSITE 1.24.2020 HEET NUMBER

LIGHTING FIXTURE SCHEDULE

1. ALL FIXTURES SHALL BE U.L. OR SIMILARLY LISTED.

- REFER TO ARCHITECTURAL DOCUMENTS FOR EXACT MOUNTING LOCATIONS, DETAILS, AND CONFIGURATIONS OF ALL LUMINAIRES. IF ARCHITECTURAL DRAWINGS DO NOT CLARIFY EXACT MOUNTING LOCATION OR DETAIL, CONTRACTOR SHALL ISSUE AN RFI FOR ARCHITECT TO SPECIFICALLY CLARIFY PRIOR TO FIXTURE ROUGH-IN.
- VERIFY COMPATIBILITY OF LIGHT FIXTURES WITH CEILING MATERIAL, ADJACENT CONSTRUCTION, AND ADJACENT FINISHES PRIOR TO SHOP DRAWINGS SUBMITTAL AND NOTIFY THE ARCHITECT OF ANY CONFLICTS WITH THE PROPOSED...

4FT VERTICAL LINEAR WALL MOUNT, SOLID FRONT WITH SIDE OPTICS, 3500K

2IN LED ACCENT, FLOOD DISTRIBUTION, HINGE MOUNT ADJUSTABLE AIM, ALTERNATE UP/DOWN,

LED WALL SCONCE, GLASS SHADE, 3000K

LED EXIT SIGN, UNIVERSAL MOUNTING

- 4. CONTRACTOR IS RESPONSIBLE FOR ALL MISCELLANEOUS HARDWARE NECESSARY TO INSTALL AND SUPPORT THE LUMINAIRES. ADJUSTABLE INTERIOR AND EXTERIOR LIGHT FIXTURES SHALL BE TARGETED AND ADJUSTED BY THE CONTRACTOR UNDER THE OBSERVATION AND IN COMPLIANCE WITH RECOMMENDATIONS OF THE ARCHITECT. ALL LABOR AND MATERIAL

YPE	MANUFACTURER	MODEL	DESCRIPTION	VOLTAGE	LOAD-VA	LAMP TYPE	APPROVED EQUALS
D1			6IN LED RECESSED DOWNLIGHT, OPEN, 3500K	120 V	25 VA		AS APPROVED BY ENGINEER
D2			3.5IN LED RECESSED DOWNLIGHT, TRIMLESS, OPEN, 3000K	120 V	25 VA		AS APPROVED BY ENGINEER
D3			SIMILAR TO TYPE D2. RECESSED ADJUSTABLE DOWNLIGHT.	120 V	25 VA		AS APPROVED BY ENGINEER
F1			2X2 RECESSED LED TROFFER, 3500K, STANDARD OUTPUT	120 V	35 VA		AS APPROVED BY ENGINEER
F2			2X2 RECESSED LED TROFFER, 3500K, HIGH OUTPUT	120 V	35 VA		AS APPROVED BY ENGINEER
F4			12FT CONTINUOUS LENGTH, 4IN WIDE APERTURE RECESSED LINEAR LED, STANDARD OPTICS, 3500K	120 V	24 VA		AS APPROVED BY ENGINEER
F5			2X2 RECESSED LED EDGE-LIT TROFFER, 3500K, STANDARD OUTPUT	120 V	35 VA		AS APPROVED BY ENGINEER
L1			4FT LED SURFACE MOUNTED LENSED WRAP, 3500K	120 V	40 VA		AS APPROVED BY ENGINEER
L2			LED UTILITY STRIP FIXTURE. 4' LENGTH, CHAIN MOUNTED. 3500K	120 V	40 VA		AS APPROVED BY ENGINEER
L4			4FT LED COVE LIGHT MOUNTED INSIDE OF COVE SHELF, CONTINUOUSLY, 3000K	120 V	40 VA		AS APPROVED BY ENGINEER
L5			LOW PROFILE LINEAR NICHE DOWNLIGHT. 3000K, 90 CRI	120 V	40 VA		AS APPROVED BY ENGINEER
L6			4FT LED UTILITY STRIP, SURFACE MOUNTED. 3500K	120 V	40 VA		AS APPROVED BY ENGINEER
P1			32IN LED PENDANT, 2700K, CLOTH SHADE	120 V	30 VA		AS APPROVED BY ENGINEER
P2			LED GLASS PENDANT, CABLE HUNG, 3000K	120 V	30 VA		AS APPROVED BY ENGINEER
S1			LED SITE AREA LIGHT, 25FT OVERALL HEIGHT, 5" SQUARE STEEL POLE, 3000K, FORWARD THROW, HOUSE SIDE SHIELD	120 V	0 VA		AS APPROVED BY ENGINEER
S2			6IN ROUND LED LIGHTING BOLLARD, 9" HEIGHT, 3000K	120 V	0 VA		AS APPROVED BY ENGINEER
S3			2IN LED CYLINDER, DOWN DISTRIBUTION, WALL MOUNT, WET LOCATION LISTED, 3000K	120 V	0 VA		AS APPROVED BY ENGINEER
S4			6IN CYLINDER LED DOWNLIGHT, PENDANT THREAD MOUNT, WET LOCATION LISTED, 3000K	120 V	0 VA		AS APPROVED BY ENGINEER
S5			ADJUSTABLE LED FLOOD LIGHT PROJECTOR. MOUNTED ALONG UNDERSIDE OF EXTERIOR SOFFIT. ADJUSTABLE AIM KNUCKLE MOUNT, WIDE FLOOD OPTIC, 3000K, REMOTE POWER SUPPLY	120 V	0 VA		AS APPROVED BY ENGINEER
S6			LINEAR LED TAPE LIGHT. OUTDOOR RATED. 3000K, 200 LUMENS/FT. APPROXIMATELY 12'-9" IN TOTAL LENGTH.	120 V	24 VA		AS APPROVED BY ENGINEER
S7			LED SLIM STEP LIGHT, 3000K	120 V	0 VA		AS APPROVED BY ENGINEER
W1			3FT LED WALL MOUNT VANITY LIGHT, ABOVE RESTROOM MIRROR, 3500K	120 V	35 VA		AS APPROVED BY ENGINEER

EQUIPMENT CONNECTION SCHEDULE

120 V

120 V

120 V

120 V

20 VA

20 VA

20 VA

5 VA

RED LED

AS APPROVED BY ENGINEER

AS APPROVED BY ENGINEER

AS APPROVED BY ENGINEER

ABBREVIATIONS:

W2

W3

W4

- NEMA 1 ENCLOSURE
- 3R NEMA 3R ENCLOSURE NEMA 4 ENCLOSURE
- 4X NEMA 4X ENCLOSURE
- BO PROVIDED BY OTHERS CB CIRCUIT BREAKER IN PANEL
- CSD COMBINATION STARTER/DISCONNECT
- CP CORD AND PLUG PROVIDED WITH UNIT
- ECB ENCLOSED CIRCUIT BREAKER

HOA HAND-OFF-AUTO

- FAR FIRE ALARM SHUTDOWN RELAY
- FDS FUSED DISCONNECT SWITCH GF GROUND FAULT CIRCUIT INTERRUPTION

INT INTEGRAL WITH EQUIPMENT FROM FACTORY

- MMS MANUAL MOTOR STARTER WITH FUSES
- NFD NON-FUSED DISCONNECT SWITCH RD RETURN AIR DUCT DETECTOR
- RSR RUN STATUS RELAY, NORMALLY OPEN SD SUPPLY AIR DUCT DETECTOR
- SSP START/STOP PUSHBUTTON WITH PILOT SS START/STOP PUSHBUTTON
- ST SHUNT TRIP
- TOR TIME DELAY OFF RELAY
- TS TOGGLE SWITCH WITH PLUG FUSE
- WITH PLUG FUSE

10	TOUGLE SWITCH WITH LOUT C
TS-L	LOCKABLE TOGGLE SWITCH WI
VFD	VARIABLE FREQUENCY DRIVE

						1				T		
	ELECTRICAL CHARACTERISTICS					<u>DISCONNECT</u>				NTROLS		
TAG	VOLTAGE	PHASE	MOTOR HP	<u>KW</u>	<u>MCA</u>	TYPE	SIZE (AMPS)	<u>NEMA</u> RATING	FUSE SIZE (AMPS)	STARTER	DESCRIPTION	REMARKS
AHU-1	208 V	3			63	INT	-	-	-	-	-	CONNECT TO SINGLE POINT POWER CONNECTION AT MECHANICAL UNIT. COORDINATE WITH APPROVED SHOP DRAWINGS.
B-1	120 V	1	-	-	5.88	TS-L	20	1	20	-	-	PROVIDE WITH LOCKABLE TOGGLE SWITCH COVER PER NEC. PROVIDE EMERGENCY-OFF PUSHBUTTON CONTROLS.
B-2	120 V	1	-	-	5.88	TS-L	20	1	20	-	-	PROVIDE WITH LOCKABLE TOGGLE SWITCH COVER PER NEC. PROVIDE EMERGENCY-OFF PUSHBUTTON CONTROLS.
CAB-1	120 V	1			5	TS-L	20		20			
CP-1	120 V	1		-	2	TS	20	1	20	-	-	-
CU-1	208 V	3	-	-	121.4	FDS	200	3R	150	-	-	UNIT PROVIDED WITH NON-FUSED DISCONNECT.
CU-2	208 V	1			16.5	FDS	30	3R	25	-	-	
EF-1	120 V	1	1/2	-	11.52	TS-L				0	-	
P-1	208 V	3	3	-	12.94	FDS	30	1	-	-	-	CONNECT TO SINGLE POINT POWER CONNECTION AT MECHANICAL UNIT. COORDINATE WITH APPROVED SHOP DRAWINGS.
P-2	208 V	3	3	-	12.94	FDS	30	1	-	-	-	CONNECT TO SINGLE POINT POWER CONNECTION AT MECHANICAL UNIT. COORDINATE WITH APPROVED SHOP DRAWINGS.
WH-1	120 V	1	-	-	5.88	TS-L	20	1	20	-	-	-

NOT FOR CONSTRUCTION



38 NORTHWEST DAVIS, SUITE 300 PORTLAND, OR 97209 503.245.7100

1505 5TH AVE, SUITE 300 SEATTLE, WA 98101 206.576.1600

1014 HOWARD STREET SAN FRANCISCO, CA 94103

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2175 NW Raleigh Street, Suite 110 Portland, OR, 97210 ENGINEERING

CLINIC SANDY HEALTH 39831 HIGHWAY 26 SANDY, OR 97055

REASON FOR ISSUE REVISION DATE

ELECTRICAL SCHEDULES

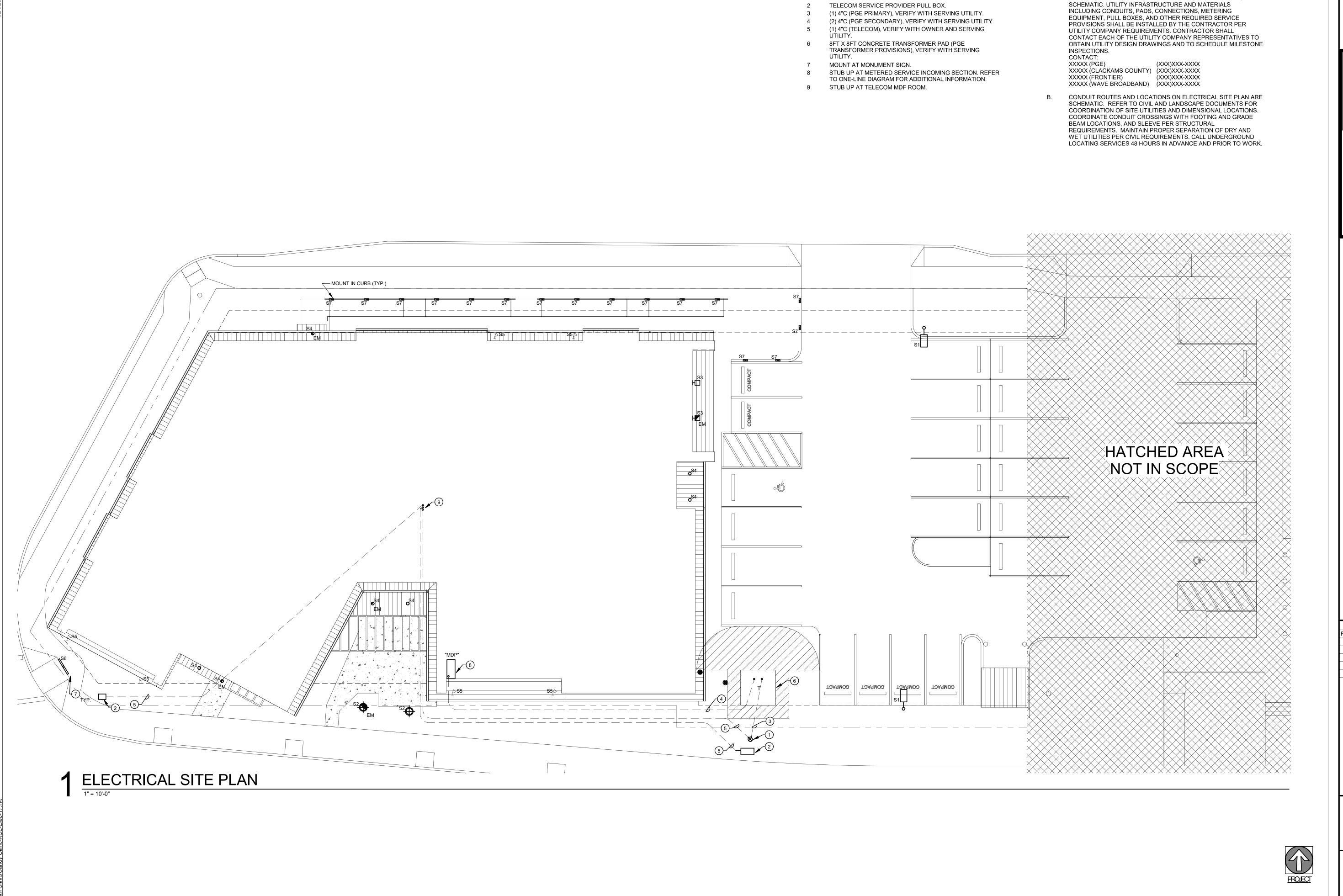
CONSTRUCTION <u>DOCUMENTS</u> DATE 3.26.2020

SHEET NUMBER

E0.02

PROJECT NUMBER

192530



KEYNOTES #

JOINT UTILITY POLE.

NOT FOR CONSTRUCTION

F. Exterior Lighting Plan



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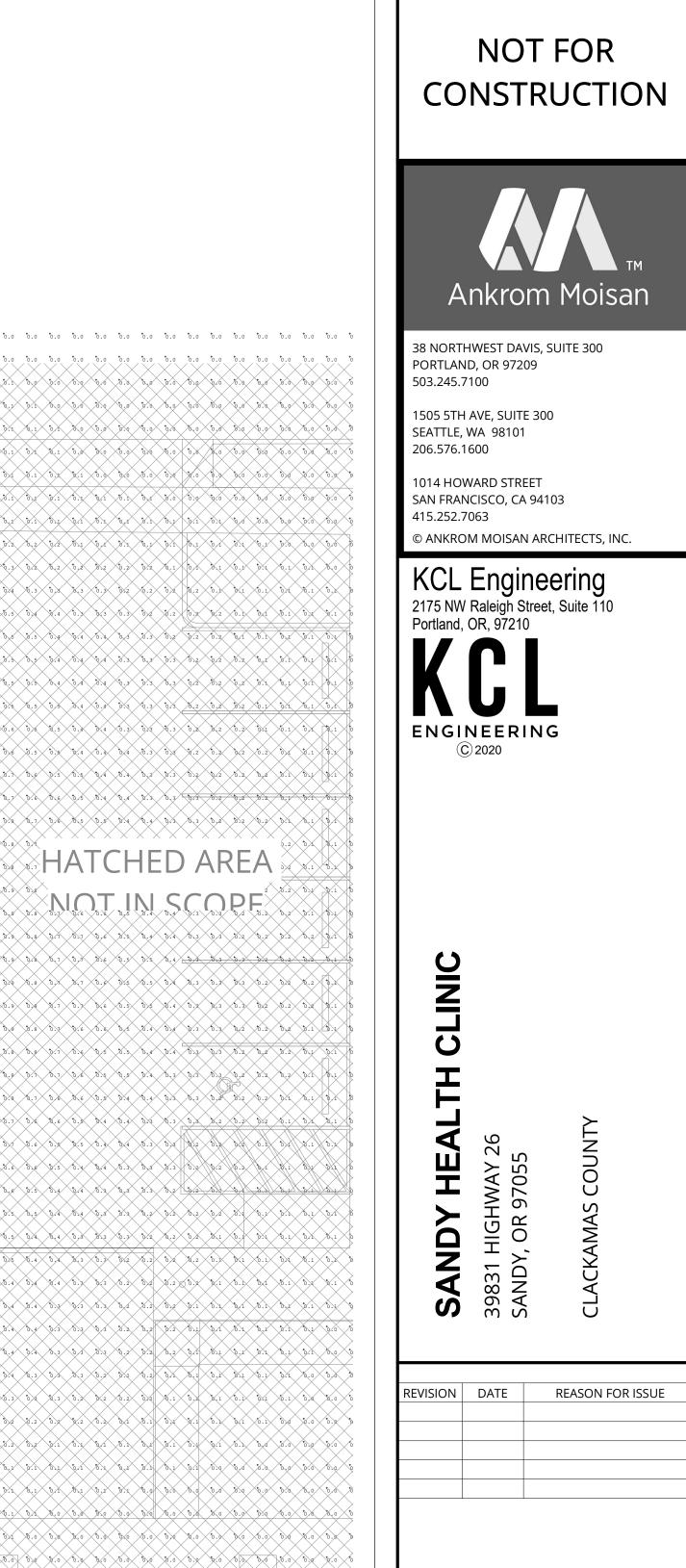
ELECTRICAL SITE PLAN

DESIGN DEVELOPMENT

DATE 1.24.2020

E1.01

PROJECT NUMBER 192530

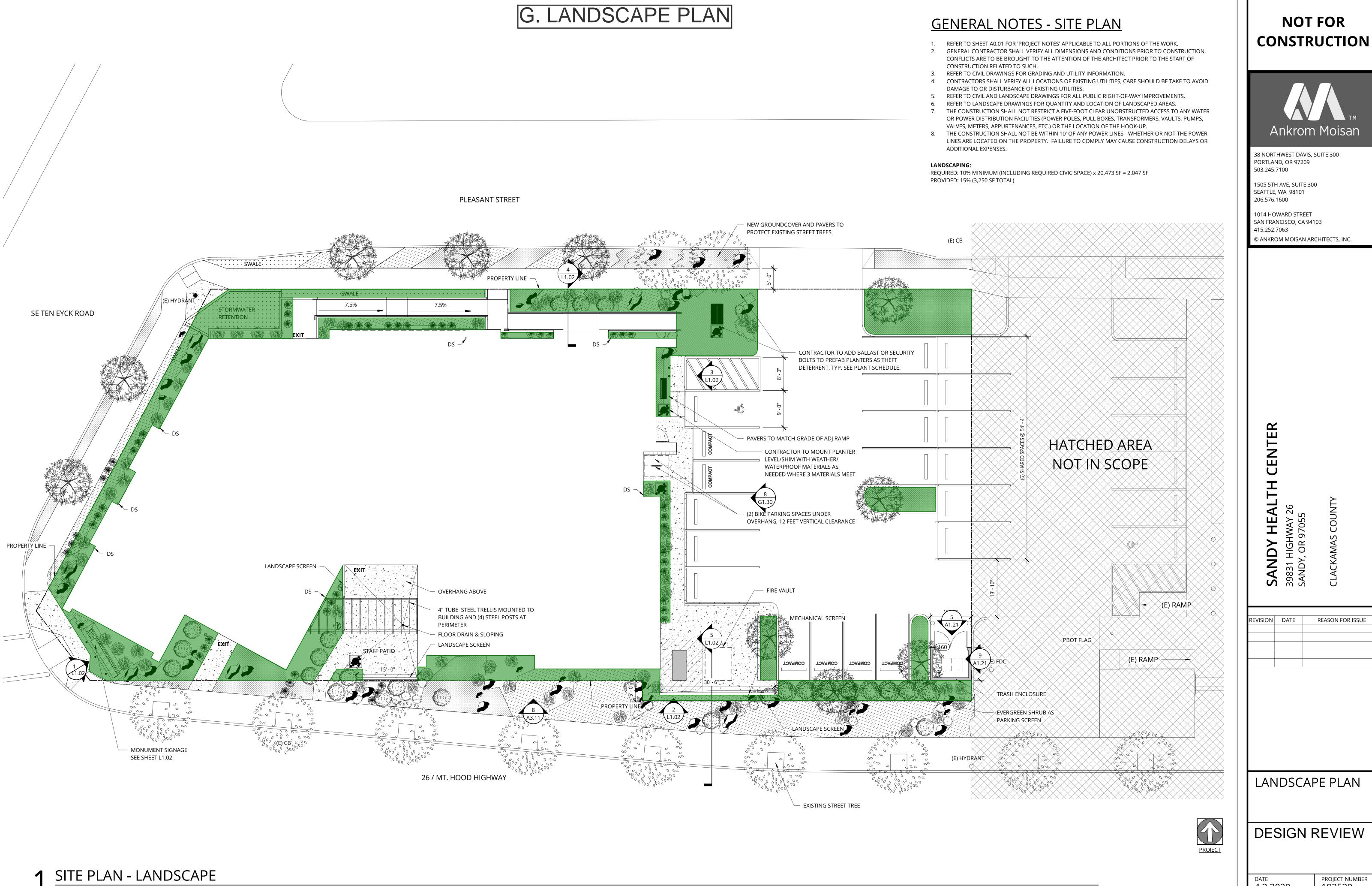


ELECTRICAL SITE LIGHTING PLAN

50% CONSTRUCTION DOCUMENTS PROJECT NUMBER

3.26.2020 192530

PHOTOMETRIC SITE PLAN



206.576.1600 1014 HOWARD STREET

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38 NORTHWEST DAVIS, SUITE 300

NOT FOR

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CENTER

SANDY 39831 HIGH SANDY, OR

REASON FOR ISSUE

DESIGN REVIEW

DATE 4.3.2020

PROJECT NUMBER 192530

L1.01

NOT FOR CONSTRUCTION



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HEALTH CLINIC

SANDY HEALTH
39831 HIGHWAY 26
SANDY, OR 97055

REVISION DATE REASON FOR ISSUE

LANDSCAPE DETAILS

DESIGN DEVELOPMENT

DATE PROJECT NUMBER 1.24.2020 192530

NUMBER L1.02

MONUMENT SIGNAGE

EXISTING

HIGHWAY

PLANTED

SLOPE

WOOD LANDSCAPE SCREEN

OBSCURES SIGHT LINES

EDOM DEDESTRIANS AND

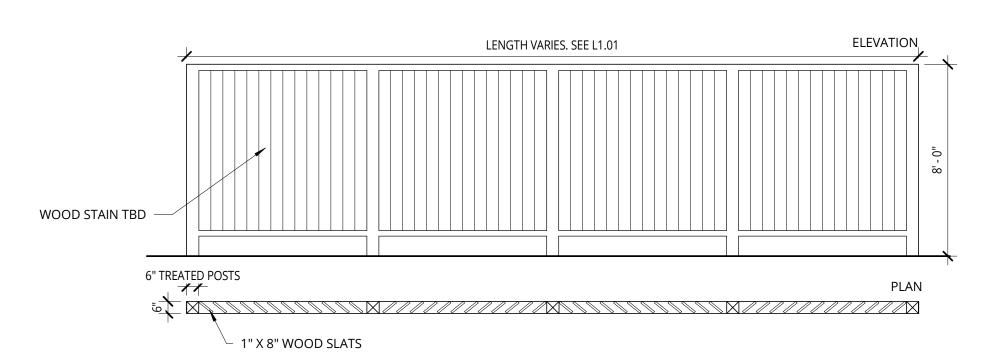
MECHANICAL UNITS

LEVEL 1

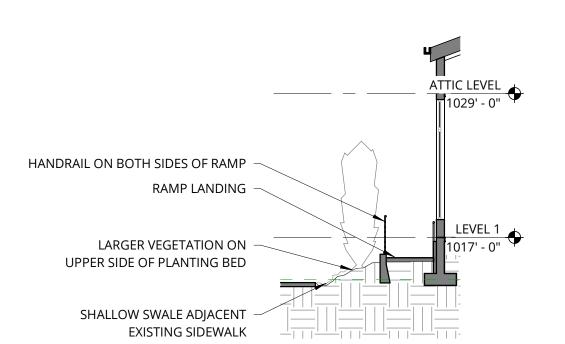
1017' - 0"

5 SIGHTLINES & LANDSCAPE SCREEN

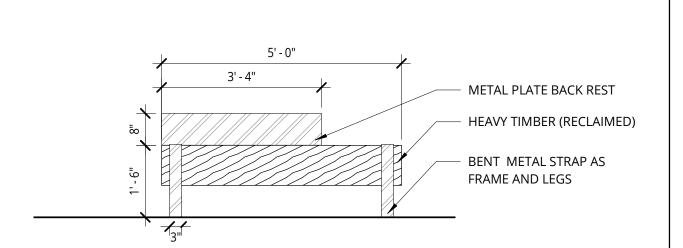
1/8" = 1'-0"



TYPICAL LANDSCAPE SCREEN



 $4 \frac{\text{RAMP SECTION}}{\frac{1}{8"} = 1'-0"}$



3 DESIGN BUILD HEAVY TIMBER BENCHES

1/2" = 1'-0"

SIGNAGE LETTERING LASER CUT FROM BENT STEEL PLATE.
MOUNT FRONT OF STEEL 4" FROM FRONT FACE OF STONE

STONE VENEER TO MATCH ANGLE OF PAVERS,
ALL SIDES
THREE (3) IN-GOUND LIGHTS. WASH FACE OF VENEER,
BACKLIGHTING THE LETTERING. SEE ELLC.
HORIZONTAL STONE
PAVERS TO SIGN BASE. SEE PLAN
FOUNDATION BELOW FROST LINE

LEVEL 1
1017'- 0"

GENERAL PLANTING NOTES:

- A. DO NOT WILLFULLY PROCEED WITH PLANTING OPERATIONS WHEN IT IS OBVIOUS THAT UNKNOWN OBSTRUCTIONS AND GRADE DIFFERENCES EXIST THAT MAY NOT HAVE BEEN KNOWN DURING THE DESIGN PROCESS. BRING SUCH CONDITIONS IMMEDIATELY TO ATTENTION OF OWNER'S AUTHORIZED REPRESENTATIVE FOR RESOLUTION. ASSUME FULL RESPONSIBILITY FOR COSTS INCURRED AND REQUIRED MODIFICATIONS DUE TO LACK OF PROVIDING SUCH NOTIFI CATION.
- B. ENSURE THAT FINISH GRADE ELEVATIONS OF PLANTING AREAS ARE SET AT THE PROPER ELEVATIONS RELATIVE TO PAVING FINISH SURFACE ELEVATIONS, UTILITY COVERS AND CURBS. SHRUB PLANTING AREAS AT 2" BELOW AND LAWN 1" BELOW ADJACENT GRADE. NOTIFY OWNER OF ANY DISCREPANCIES.
- C. ASSURE POSITIVE DRAINAGE IN ALL PLANTING AREAS TO DRAIN AWAY FROM BUILDING, 2% MINIMUM.
- D. PLANT MATERIAL, I.E. TREES, SHRUBS VINES, ESPALIERS AND GROUNDCOVERS, MUST BE APPROVED BY OWNER'S AUTHORIZED REPRESENTATIVE PRIOR TO INSTALLATION. PLANT MATERIAL INSTALLED WITHOUT OWNER'S AUTHORIZED REPRESENTATIVE'S APPROVAL MAY BE SUBJECT TO REMOVAL AND REPLACEMENT WITH RELATED COSTS BORNE BY CONTRACTOR.
- E. FINAL LOCATIONS OF PLANT MATERIALS ARE SUBJECT TO APPROVAL OF THE OWNER'S AUTHORIZED REPRESENTATIVE PRIOR TO INSTALLATION. PERFORM THE FOLLOWING BEFORE BEGINNING PLANTING PIT
- E.A. SHRUBS PLACE ACTUAL PLANT CONTAINERS ON-SITE IN "FINAL" LOCATIONS. E.B. TREES - PAINT OR STAKE CENTER OF TREE.
- F. PLANTING SHALL NOT BE PERFORMED UNTIL PRE-PLANTING SOIL AMENDMENTS ARE COMPLETE AND APPROVED BY THE OWNER'S REPRESENTATIVE.
- G. TOPSOIL SHALL BE UTILIZED IN ALL PLANTING AREAS TO THE MAXIMUM EXTENT FEASIBLE. TOPSOIL REMOVED DURING CONSTRUCTION ACTIVITY SHALL BE CONSERVED FOR LATER USE ON AREAS REQUIRING REVEGETATION AND LANDSCAPING.
- H. SOIL AMENDMENTS SHALL BE PROVIDED IN ACCORDANCE WITH THE RECOMMENDATIONS OF THE FERTILITY ANALYSIS PROVIDED BY AND APPROVED SOIL TESTING LAB. SOILS SHALL BE THOROUGHLY LOOSENED TO A DEPTH OF NOT LESS THAN 8 INCHES AND SOIL AMENDMENT SHALL BE THOROUGHLY INCORPORATED INTO THE SOIL OF ALL LANDSCAPE AREAS TO A DEPTH OF AT LEAST 6 INCHES BY TILLING, DISKING OR OTHER SUITABLE PROCESSES.
- IF CONFLICTS ARISE BETWEEN ACTUAL SIZE OF PLANTING AREAS ON-SITE AND THOSE AREAS INDICATED ON DRAWINGS, CONTACT OWNER'S AUTHORIZED REPRESENTATIVE FOR RESOLUTION. FAILURE TO MAKE SUCH CONFLICTS KNOWN TO OWNER'S AUTHORIZED REPRESENTATIVE IN A TIMELY FASHION MAY RESULT IN CONTRACTOR'S LIABILITY TO RELOCATE PLANT MATERIALS OR AT WORST CASE, BECOME UNABLE TO CHARGE OWNER FOR PLANT MATERIAL ALREADY PLANTED.
- J. SHRUB AND GROUNDCOVER AREAS TO RECEIVE A 3-INCH DEEP LAYER MULCH TO BE SUBMITTED FOR APPROVAL FROM LANDSCAPE ARCHITECT.
- K. IRRIGATION: ALL LANDSCAPE AREAS WITHIN THE SITE INCLUDING TURF, SHRUB BEDS AND TREE AREAS SHALL BE IRRIGATED WITH AN AUTOMATIC IRRIGATION SYSTEM. THE IRRIGATION SYSTEM SHALL BE ADJUSTED TO EMIT THE WATER REQUIREMENTS OF THE INDIVIDUAL PLANT MATERIAL
- L. PROVIDE ROOT CONTROL BARRIERS FOR ALL TREES PLANTED WITHIN 5' OF A HARDSCAPE EDGE SUCH AS PAVING. WALLS, STEPS, ETC. REFER TO PLANTING DETAILS FOR ADDITIONAL INFORMATION.
- M. INSTALL PLANT MATERIAL WITH ITS BEST SIDE FACING PREDOMINATE VIEW OF PUBLIC.
- N. PROVIDE THE PROPER SETBACK BETWEEN UTILITIES AND TREES CONTACT CITY INSPECTOR FOR REQUIRED SETBACKS IN THE CASE THAT THE DRAWINGS ARE NOT CLEAR.
- O. ALL WORK WITHIN THE PUBLIC RIGHT OF WAY UNDER SEPARATE PERMIT. SHOWN FOR REFERENCE ONLY. REFER TO APPROVED RIGHT OF WAY DRAWINGS PRIOR TO CONSTRUCTION.
- P. REFERENCE CIVIL AND ARCHITECTURAL DRAWINGS FOR ADDITIONAL SITEWORK INFORMATION.
- Q. ALL WORK IN AREAS OF TREE PRESERVATION TO BE DONE USING HAND TOOLS WITH CARE TAKEN TO AVOID DAMAGE TO EXISTING TREE ROOTS, OR UNDER DIRECT SUPERVISION OF A PROJECT ARBORIST.
- R. DO NOT MULCH AGAINST TREE TRUNK.
- S. PLANT PER PLAN BUT NO CLOSER THAN 5 FEET TO TRUNK, ADJUST LOCATION OF NEW PLANTS AS NEEDED TO AVOID TREE ROOTS IF ENCOUNTERED DURING HAND DIGGING.
- T. USE TEMPORARY DRIP IRRIGATION TO WATER PLANTS UNTIL ESTABLISHED, SEE IRRIGATION PLAN FOR MORE INFORMATION.
- U. UNUSED.
- V. PER VMC 20.925.115, PRIOR TO OCCUPANCY, A LICENSED LANDSCAPE ARCHITECT SHALL CERTIFY THAT ALL REQUIRED LANDSCAPING HAS BEEN PLANTED PER THE APPROVED PLANS.

PREPARATION, INSTALLATION AND MAINTENANCE OF NEW TREES

- ALL TREES SHALL BE SECURELY STAKED OR GUYED.
- 2. ALL PLANT MATERIAL SHALL BE FREE OF ANY DEFECTS, OF NORMAL HEALTH, HEIGHT, LEAF DENSITY AND SPREAD APPROPRIATE TO THE SPECIES AS DEFINED BY THE AMERICAN ASSOCIATION OF NURSERYMEN (AAN) STANDARDS. ALL TREES SHALL BE BALL AND BURLAP OR EQUIVALENT.
- 3. ALL LANDSCAPING SHALL BE MAINTAINED FREE FROM DISEASE, PESTS, WEEDS

MAINTENANCE NOTES FOR EXISTING TREES

- WASH OFF FOLIAGE WHICH BECOMES SOILED DURING CONSTRUCTION.
- 2. WATER TREES AND OTHER VEGETATION WHICH ARE TO REMAIN AS NECESSARY TO MAINTAIN THEIR HEATH DURING THE COURSE OF THE WORK. RATE AND FREQUENCY OF APPLICATION TO BE DETERMINED BY PROJECT ARBORIST.
- 3. ALL PRUNING SHALL BE PERFORMED BY A CURRENT ARBORIST LICENSED WITHIN THE STATE/COUNTY/CITY WHERE THE WORK IS TO BE COMPLETED.

STORMWATER PLANTING NOTES

- 1. STORMWATER FACILITIES TO BE PLANTED & CONSTRUCTED PER CITY OF
- 2. PLANT QUANTITIES MEET REQUIREMENTS OF CITY OF SANDY.
- CONTRACTOR IS RESPONSIBLE FOR VERIFYING THAT THE REQUIRED CITY/COUNTY STORMWATER FACILITY INSPECTIONS HAVE BEEN PERFORMED AND APPROVED PRIOR TO PLACEMENT OF THE ENGINEERED SOIL
- 4. REFER TO CIVIL ENGINEERS PLANS FOR SOIL (FG) FINISHED GRADE ELEVATION AND DEPTH PRIOR TO INSTALLING THE APPROVED TOPSOIL, IRRIGATION AND PLANTING ABOVE DRAIN ROCK AND PIPING.

LANDSCAPE CALCULATION NOTES

LANDSCAPE CALCULATIONS

SHALL BE MAINTAINED SO THAT FOLIAGE HEIGHT ABOVE PAVEMENT DOES NOT EXCEED 2.5 FT. STREET TREES WITHIN SIGHT DISTANCE TRIANGLE SHALL BE LIMBED UP TO A HEIGHT OF 10 FT. CONSISTENT WITH ALL A300 STANDARDS TO PROVIDE SIGHT

5 FOOT L1 BUFFER REQUIRED: 2" CALIPER TREES, 1 PER 30 LINEAR FEET, TYP

10 FOOT L2 BUFFER REQUIRED: 2" CALIPER TREE, 1 PER 30 LINEAR FEET, 3" CONTINUOUS HEDGE - 3 GALLON CONTAINER WITH 18" MINIMUM SPREAD, TYP

STREET TREES: 2" CALIPER AT 30' ON CENTER, TYP

FIELD ADJUST EXISTING PLANTING TO ACCOMODATE NEW WORK

INFILL PLANTING, FIELD ADJUST TO AVOID EXISTING TREE ROOTS

PARKING LOT PLANTING REQUIREMENTS: A MINIMUM OF 10% OF THE PARKING LOT IS TO BE LANDSCAPED, INCLUDING 1 TREE PER 10 PARKING STALLS AND 1 SHRUB FOR 30 SF OF THE REQUIRED LANDSCAPE AREA, TYP

PLANT SCHEDULE

TREES	BOTANICAL/COMMON NAMES	CONT	CAL	SIZI	Ξ (ΣΤΥ
	NYSSA SYLVATICA 'HAYMAN'S RED'/ RED RAGE TUPELO	B&B	2" CAL			9
	ILEX CRENATA 'STEEDS' UPRIGHT HOLLY			6'H/7	GAL	18
SHRUBS	BOTANICAL/COMMON NAMES	SIZE	HT.			QTY
	OSMANTHUS XFORTUNEI 'SAN JOSE' SWEET TEA OLIVE	3 GAL				10
ORNAMENT GRASSES	FAL BOTANICAL/COMMON NAMES	SIZE				QTY
	OPHIOPOGON PLANISCAPUS 'NIGRESCENS' / MONDO GRASS	3 GA	<u> </u>			66
Experience of the second	DELPHINIUM ELATUM/ MAGIC FOUNTAIN MIX	3 GA	L			28
	CAREX MORROWII 'AUREA-VARIEGATA'/ VARIEGATED JAPANESE SEDGE	3 GA	AL.			55
VINES	BOTANICAL/COMMON NAMES	SIZE				QTY
	CLEMATIS ARMANDII 'APPLE BLOSSOM/ WHITE EVERGREEN CLEMATIS	1 GA	L			2
STORMWA SWALE PL	ATER/ LANTING MIX BOTANICAL/COMMON NAMES					SF
	STORMWATER CAREX OBNUPTA / SLOUGH SEDGE JUNCUS EFFUSUS / SOFT RUSH			1 GAL 1 GAL	50% @ 12" oc 50% @ 12" oc	220 sf

PAVERS AND STONE AREA/QTY RECTANGULAR TUMBLED STONE PAVERS, RUNNING PATTERN ORIENTATION AT ANGLE INDICATED.

MULCH 4" DARK BROWN BARK MULCH BY INSTALLER, LOCAL SUPPLIER, NO DYES - FOR ALL BEDS AT PLANT INSTALLATION



AS NOTED ON L1.01

ARCHITECT TO APPROVE SAMPLE

PURPLEWINTERCREEPER

GROUND COVERS	BOTANICAL/COMMON NAMES	CONT.	SPACING	AREA	
	POTENTILLA N. 'NANA'/CINQUEFOIL	1 gal	18" o.c.	2600 sf	
	FUONYMUS 'COLORATUS' /	1 gal	18" o.c	1500 sf	

FURNITURE



PLANTERS QTY 4 powder-coated aluminum planters,27" x 27" x 28"-color TBD, 1 gal evergreen shrub in center (selected by installer), seasonal annuals by owner. BOD: Ore, Inc Cube https://ore.design/products/cube/

BENCHES QTY 2 single-sided heavy-timber benches with steel back rest and legs, scaled dimensions as shown, Contractor design/build QTY: 1 double -sided heavy-timber benches with steel back rest and legs, scaled dimensions as shown, Contractor design/build

G. Landscape Plan: Supplemental Information

NOT FOR CONSTRUCTION



38 NORTHWEST DAVIS, SUITE 300 PORTLAND, OR 97209 503.245.7100

1505 5TH AVE, SUITE 300 SEATTLE, WA 98101 206.576.1600

1014 HOWARD STREET SAN FRANCISCO, CA 94103 415.252.7063

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HEA

SANDY

REASON FOR ISSUE

LANDSCAPE NOTES + PLANT SCHEDULE

DESIGN DEVELOPMENT

PROJECT NUMBER 1.24.2020 192530

SHEET NUMBER

G. Landscape Plan: Supplemental Information

TREE BACKFILL AMENDED AS FOLLOWS: 3 PARTS OF EXISTING TOPSOIL

 1 PART COMPOST AS SPECIFIED SEE CHART

CALIPER SIZE	PERMAMATRIX POUNDS REQUIRED (DRY)
1.0"	5.00
1.5"	7.50
2.0"	10.00
2.5"	20.00
3.0"	30.00
3.5"	50.00

SHRUB, GRASSES AND GROUNDCOVER

- BACKFILL AMENDED AS FOLLOWS: 3 PARTS OF EXISTING TOPSOIL

•	I PART COMPOST
•	AS SPECIFIED SEE CHART

CONTAINER SIZE	PERMAMATRIX POUNDS REQUIRED (DRY)
PLUG	.05
4-INCH	.20
1 GAL.	.50
2 GAL.	.75
3 GAL.	1.25
6 GAL.	1.50
15 GAL.	5.00

PERMAMATRIX AVAILABLE LOCALLY FROM SUNMARK ENVIRONMENTAL 503.241.7333

PLANTING BACKFILL SOIL AMENDMENT

Surface Mount Flange

PRODUCT: STAPLE BIKE RACK | MANUFACTURER: HUNTCO MATERIAL: MILD STEEL, 5/8" X 2 1/2" STEEL FLAT BAR. FINISH: THERMOPLASTIC BLACK.

BIKE RACK TO MEET CITY OF VANCOUVER STANDARDS, TYP

BIKE RACK - SURFACE MOUNT

3291-08

P-CO-18058-36

PREPARATION, INSTALLATION AND MAINTENANCE OF NEW TREES

1. TOPSOIL SHALL BE UTILIZED IN ALL PLANTING AREAS TO THE MAXIMUM EXTENT FEASIBLE. TOPSOIL REMOVED DURING CONSTRUCTION ACTIVITY SHALL BE CONSERVED FOR LATER USE ON AREAS REQUIRING REVEGETATION AND LANDSCAPING.

2. SOIL AMENDMENTS SHALL BE PROVIDED IN ACCORDANCE WITH THE RECOMMENDATIONS OF THE FERTILITY ANALYSIS PROVIDED BY AND APPROVED SOIL TESTING LAB. SOILS SHALL BE THOROUGHLY LOOSENED TO A DEPTH OF NOT LESS THAN EIGHT (8) INCHES AND SOIL AMENDMENT SHALL BE THOROUGHLY INCORPORATED INTO THE SOIL OF ALL LANDSCAPE AREAS TO A DEPTH OF AT LEAST SIX (6) INCHES BY TILLING, DISKING OR OTHER SUITABLE.

3. BARK MULCH SHALL BE PLACED AT A MINIMUM OF A 2 INCH DEPTH WITHIN ALL PLANTING AREAS.

4. ALL TREES SHALL BE SECURELY STAKED OR GUYED.

5. ALL PLANT MATERIAL SHALL BE FREE OF ANY DEFECTS, OF NORMAL HEALTH, HEIGHT, LEAF DENSITY AND SPREAD APPROPRIATE TO THE SPECIES AS DEFINED BY THE AMERICAN ASSOCIATION OF NURSERYMEN (AAN) STANDARDS. ALL TREES SHALL BE BALL AND BURLAP OR EQUIVALENT.

6. IRRIGATION: ALL LANDSCAPE AREAS WITHIN THE SITE INCLUDING TURF, SHRUB BEDS AND TREE AREAS SHALL BE IRRIGATED WITH AN AUTOMATIC IRRIGATION SYSTEM. THE IRRIGATION SYSTEM SHALL BE ADJUSTED TO MEET THE WATER REQUIREMENTS OF THE INDIVIDUAL PLANT MATERIAL

7. ALL LANDSCAPING SHALL BE MAINTAINED FREE FROM DISEASE, PESTS, WEEDS AND LITTER.

MAINTENANCE NOTES FOR EXISTING TREES

- 1. WASH OFF FOLIAGE WHICH BECOMES SOILED DURING CONSTRUCTION.
- 2. WATER TREES AND OTHER VEGETATION WHICH ARE TO REMAIN AS NECESSARY TO MAINTAIN THEIR HEATH DURING THE COURSE OF THE WORK. RATE AND FREQUENCY OF APPLICATION TO BE DETERMINED BY PROJECT ARBORIST.

METAL T-POST. DRIVEN 1/3RD OF FENCE HEIGHT INTO GROUND. NO CONCRETE FOOTING. PROTECTIVE FENCING PER ARBORIST REPORT EXISTING R.O.W. IMPROVEMENTS EXISTING **IMPROVEMENTS ELEVATION**

PLANTING ON SLOPES #1/#2

2 x DIA. OF

ROOTBALL

TRUNK CALIPER SHALL MEET ANSI Z60 CURRENT

ROUND-TOPPED SOIL BERM 4" HIGH X 8" WIDE ABOVE ROOT BALL

3" LAYER OF MULCH NO MORE THAN 1" OF MULCH ON TOP OF

TREE PLANTING ON SLOPE

DO NOT USE PLANT TABLETS IN

STORMWATER WATER QUALITY

ROOT BALL (SEE SPECIFICATIONS FOR MULCH)

SURFACE SHALL BE CONSTRUCTED AROUND THE ROOTBALL. BERM

EDITION FOR ROOT BALL SIZE

SHALL BEGIN AT ROOT BALL PERIPHERY

ROOT BALL MODIFIED AS

REQUIRED

EXISTING SOIL

3293-08

EXISTING SUBGRADE

SPECIFIED CONTAINER PLANT

COMPOST MULCH, 18" DIA. MIN. SEE SPECS

3" HIGH RETENTION BERM FORMED WITH

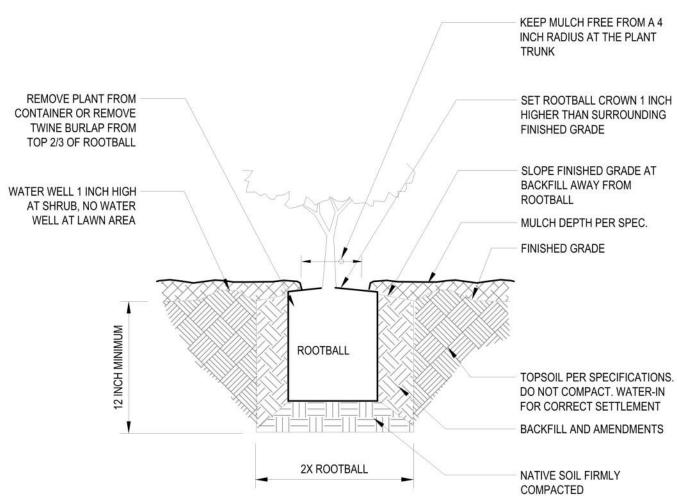
SOIL EXCAVATED FROM UPHILL SIDE OF

BACKFILL WITH AMENDED TOPSOIL, SEE SPECS

1:1 MAX. SLOPE OF SURFACE

EXISTING SLOPE GRADIENT

AMENDED TOPSOIL, SEE SPECS



NOTE: CHECK ROOTBALL FOR PRESENCE OF ROOT FLARE AT BASE OF TRUNK. REMOVE EXCESS SOIL OVER ROOT FLARE AND ADJUST DEPTH OF PLANTING HOLE TO ACCOMODATE REDUCED ROOTBALL DEPTH IF NEEDED. ROOT FLARE

1" WIDE CHAIN-LOCK TREE TIES, COLOR 2" CLEAR FROM STEM FINISH GRADE ORGANIC MULCH, PER SPECS TREE ROOTBALL BACKFILL PER SPECS

COMPACTED NATIVE SOIL NATIVE SOIL/ COMPACTED SUBGRADE * USE AN APPROVED ROOT BARRIER WHEN PLANTING WITHIN 10 FEET OF A BUILDING

329343-01

THAN 5 FEET FINISHED GRADE WALL OR **SIDEWALK** ROOT

REQUIRED FOR CONDITIONS LESS

PROTECTION FENCING - PER ARBORIST

LINEAL INSTALLED ROOT BARRIER BY NDS EP SERIES 24 INCHES DEEP OR APPROVED EQUAL. INSTALL ALONG SIDEWALK FOR TREES PLANTED 5 FEET OR CLOSER TO HARDSCAPE (MEASURED FROM BASE OF TRUNK). EXTEND 5 FEET BEYOND TRUNK IN EACH DIRECTION, UNLESS NOTED OTHERWISE ON PLANS. IF LENGTHS ARE NOT SPECIFIED REFER TO MANUFACTURER'S RECOMMENDATIONS

PLANTING AND LAWN AREA NOTES:

ANALYSIS REPORT. 2. COMPACTED SUBSOILS SHALL BE SCARIFIED (TILLED) EXCEPT WHERE DAMAGE TO TREE ROOTS, STRUCTURES OR AS DETERMINED BY LANDSCAPE ARCHITECT OR ARBORIST.

DESIGN

DEVELOPMENT

PLANTING DETAILS

PROJECT NUMBER 1.24.2020 192530

NOT FOR

CONSTRUCTION

Ankrom Moisan

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HEA

ANDY

REASON FOR ISSUE

P-CO-18058-32

L6.01

MUST BE VISIBLE ABOVE MULCH/SOIL/ROOTBALL. 329333-01 SET ROOT BALL CROWN 1" ABOVE FINISH GRADE AND REMOVE BURLAP/TWINE/WIRE FROM TOP HALF OF ROOTBALL, KEEP MULCH

ORIGINAL SLOPE SHOULD PASS THROUGH THE POINT WHERE THE TRUNK

LOOSEN SOIL. DIG AND TURN THE SOIL TO REDUCE THE COMPACTION

PRIOR TO MULCHING, LIGHTLY TAMP SOIL AROUND ROOT BALL IN 6" LIFTS TO BRACE TREE. DO NOT OVER COMPACT. WHEN THE PLANTING HOLE HAS BEEN BACKFILLED, POUR WATER AROUND THE ROOT BALL TO SETTLE THE

BASE MEETS SUBSTRATE/SOIL

SLOPE SIDES OF LOOSENED SOIL

BOTTOM OF ROOT BALL RESTS ON EXISTING OR

329343-04

OTHERWISE

329333.83-01

2" ROUND X 8'-0" TREATED WOOD STAKES, (3) PER TREE WHEN CALIPER IS 2" OR LARGER (2)

5FT TALL AND LARGER (2) PER SMALLER

EVERGREEN TREES. INSTALL CLEAR OF

PER SMALLER TREES. SET PERPENDICULAR TO PREVAILING WIND. (3) PER EVERGREEN TREE

SPECIFIED

RECOMPACTED SOIL

PLANT CENTER

EDGE OF PLANT BED, CURB,

S = SPACING ON CENTER (O.C.) AS SHOWN ON

WALK, FENCE OR WALL

GROUNDCOVER SPACING

TREE PLANTING ON GRADE

3X WIDEST **DIMENSION OF**

TREE ROOT BARRIER - LINEAR 329452-02 3. ALL PRUNING SHALL BE PERFORMED BY A CURRENT ARBORIST LICENSED WITHIN THE STATE/COUNTY/CITY WHERE THE WORK IS TO BE COMPLETED. MULCH AREA AT GRADE WITH ADJACENT SURFACING APPROVED COMPOST AND ROOT ZONE MIX, SEE AMENDMENTS TILLED INTO TOPSOIL PER SOIL ANALYSIS TURF AREA 1-INCH **BELOW ADJACENT** SURFACING TOP OF PAVING

GRADE STRUCTUAL WALL, FOOTING OR PAVING DO NOT DISTURB COMPACTION OF STRUCTURAL SUB-SOILS ADJACENT TURF AREA TO STRUCTURES WITHIN A 1:1 SLOPE (FROM TOP OF GRADE) SUB-SOILS SCARIFIED OR AS NOTED WITH A 2" DEPTH OF PLANTING AREA

1. SOILS DISTURBED OR COMPACTED DURING CONSTRUCTION SHALL BE AMENDED AS DESCRIBED PER SOIL

COMPOST BLENDED 6"

TOPSOIL / ROOT ZONE MIX

BELOW AMENDED

OTHERWISE.

P-CO-18058-38

SOIL PREPARATION



13"

(19.0 cm)

D-Series Size 1

LED Area Luminaire













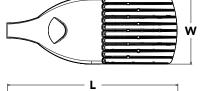
1.01 ft² EPA:

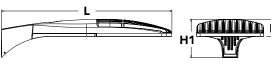
33" Length: (83.8 cm)

Width: (33.0 cm) 7-1/2" Height H1:

3-1/2" Height H2:

Weight 27 lbs (max): (12.2 kg)





S1 Fixture

H. Sandy Health Clinic - Exterior Light Fixture

Cut-Sheets

Introduction

The modern styling of the D-Series is striking yet unobtrusive - making a bold, progressive statement even as it blends seamlessly with its environment. The D-Series distills the benefits of the latest in LED technology into a high performance, high efficacy, long-life luminaire.

The outstanding photometric performance results in sites with excellent uniformity, greater pole spacing and lower power density. It is ideal for replacing up to 750W metal halide in pedestrian and area lighting applications with typical energy savings of 65% and expected service life of over 100,000 hours.



Ordering Information

EXAMPLE: DSX1 LED P7 40K T3M MVOLT SPA NLTAIR2 PIRHN DDBXD

DSX1 LED					
Series LE	.EDs	Color temperature	Distribution	Voltage	Mounting
P P P R P	Forward optics P1 P4 P7 P2 P5 P8 P3 P6 P9 Rotated optics P10¹ P12¹ P11¹ P13¹	30K 3000 K 40K 4000 K 50K 5000 K	T1S Type I short T5VS Type V very short T2S Type II short T5S Type V short T2M Type II medium T5M Type V medium T3S Type III short T5W Type V wide T3M Type III medium BLC Backlight control ² T4M Type IV medium LCCO Left corner cutoff ² TFTM Forward throw medium	MVOLT ³ 120 ⁴ 208 ⁴ 240 ⁴ 277 ⁴ 347 ⁴ 480 ⁴	Shipped included SPA Square pole mounting RPA Round pole mounting WBA Wall bracket SPUMBA Square pole universal mounting adaptor 5 RPUMBA Round pole universal mounting adaptor 5 Shipped separately KMA8 DDBXD U Mast arm mounting bracket adaptor (specify finish) 6

Control options					options	Finish (required)	
PIRHN Netwo PER NEMA PER5 Five-F PER7 Seven DMG 0-10v extern	ht AIR generation 2 enabled ⁷ vork, high/low motion/ambient sensor ⁸ IA twist-lock receptacle only (controls ordered separate) ⁹ -pin receptacle only (controls ordered separate) ^{9,10} en-pin receptacle only (controls ordered separate) ^{9,10} by dimming wires pulled outside fixture (for use with an mal control, ordered separately) ¹¹ switching ^{12,13,14}	PIR PIRH PIR1FC3V PIRH1FC3V FAO	High/low, motion/ambient sensor, 8-15' mounting height, ambient sensor enabled at 5fc ^{15,16} High/low, motion/ambient sensor, 15-30' mounting height, ambient sensor enabled at 5fc ^{15,16} High/low, motion/ambient sensor, 8-15' mounting height, ambient sensor enabled at 1fc ^{15,16} Bi-level, motion/ambient sensor, 15-30' mounting height, ambient sensor enabled at 1fc ^{15,16} Field adjustable output ¹⁴	HS SF DF L90 R90	ped installed House-side shield ¹⁷ Single fuse (120, 277, 347V) ⁴ Double fuse (208, 240, 480V) ⁴ Left rotated optics ¹ Right rotated optics ¹ ped separately Bird spikes ¹⁸ External glare shield	DDBXD DBLXD DNAXD DWHXD DDBTXD DBLBXD DNATXD	Dark bronze Black Natural aluminum White Textured dark bronze Textured black Textured natural aluminum Textured white



Ordering Information

Accessories

Ordered and shipped separately

DLI 127F 1.5 JU Photocell - SSL twist-lock (120-277V) 19 DLL347F 1.5 CUL JU Photocell - SSL twist-lock (347V) 19 DLL480F 1.5 CUL JU Photocell - SSL twist-lock (480V) 19

DSHORT SBK U Shorting cap 19

DSX1HS 30C U House-side shield for P1, P2, P3, P4 and P517 DSX1HS 40C U House-side shield for P6 and P717 House-side shield for P8, P9, P10, P11 and P1217 DSX1HS 60C II

Square and round pole universal mounting bracket (specify finish)²⁰ PUMBA DDBXD U*

KMA8 DDBXD U

Mast arm mounting bracket adaptor (specify finish) ⁶

DSX1EGS (FINISH) U External glare shield

For more control options, visit DTL and ROAM online.

NOTES

- P10, P11, P12 or P13 and rotated optics (L90, R90) only available together.
- Not available with HS.
- MVOLT driver operates on any line voltage from 120-277V (50/60 Hz).
 Single fuse (SF) requires 120V, 277V or 347V. Double fuse (DF) requires 208V, 240V or 480V.
- Universal mounting brackets intended for retrofit on existing, pre-drilled poles only. 1.5 G vibration load rating per ANCI C136.31.

 Must order fixture with SPA option. Must be ordered as a separate accessory; see Accessories information. For use with 2-3/8" mast arm (not included).
- Must be ordered with PIRHIN. Sensor cover available only in dark bronze, black, white and natural aluminum colors. Must be ordered with NLTAIR2. For more information on nLight Air 2 visit this link.
- 9 Photocell ordered and shipped as a separate line item from Acuity Brands Controls. See accessories. Not available with DS option. Shorting cap included. 10 If ROAM® node required, it must be ordered and shipped as a separate line item from Acuity Brands Controls. Node with integral dimming.
- 11 DMG not available with PIRHN, PER5, PER7, PIR, PIRH, PIR1FC3V or PIRH1FC3V.
 12 Provides 50/50fixture operation via (2) independent drivers. Not available with PER, PER5, PER7, PIR or PIRH. Not available P1, P2, P3, P4 or P5.
- 13 Requires (2) separately switched circuits with isolated neutrol. See Outdoor Control Technical Guide for details
- 14 Reference Motion Sensor table on page 4.

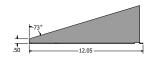
- 15 Reference controls options table on page 4 to see functionality.
 16 Not available with other dimming controls options
 17 Not available with BLC, LCCO and RCCO distribution. Also available as a separate accessory; see Accessories information.
- 18 Must be ordered with fixture for factory pre-drilling.

 19 Requires luminaire to be specified with PER, PER5 or PER7 option. See PER Table on page 3.
- 20 For retrofit use only.

Options

EGS - External Glare Shield

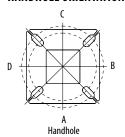


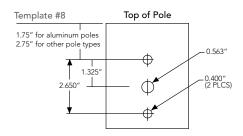




Drilling

HANDHOLE ORIENTATION





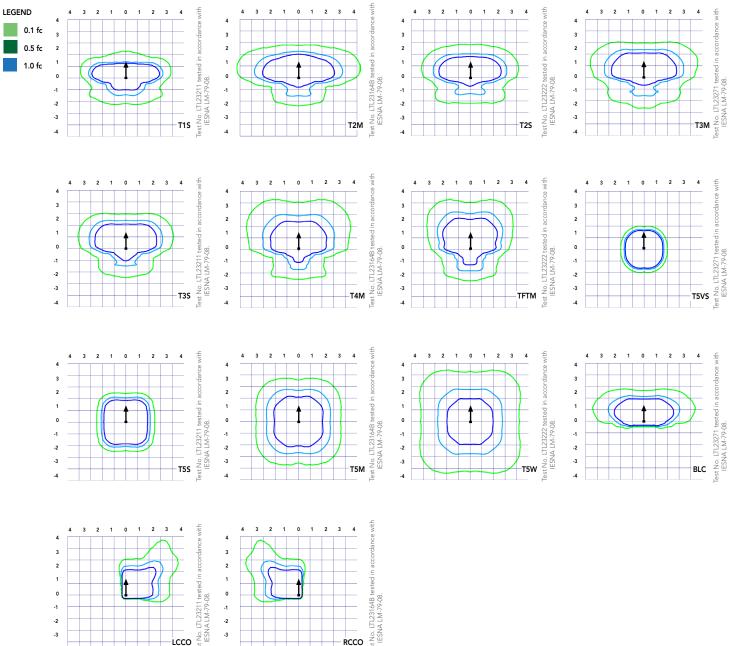
Tenon Mounting Slipfitter**

Tenon O.D.	Mounting	Single Unit	2 @ 180	2 @ 90	3 @120	3 @ 90	4 @ 90
	SPA/RPA	AS3-5 190	AS3-5 280	AS3-5 290	AS3-5 320	AS3-5 390	AS3-5 490
2-3/8"	SPUMBA	AS3-5 190	AS3-5 280	AS4-5 290	AS3-5 320	AS4-5 390	AS4-5 490
	RUPUMBA	AS3-5 190	AS3-5 280		AS3-5 320		
	SPA/RPA	AST25-190	AST25-280	AST25-290	AST25-320	AST25-390	AST25-490
2-7/8"	SPUMBA	AST25-190	AST25-280		AST25-320		
	RUPUMBA	AST25-190	AST25-280		AST25-320		
	SPA/RPA	AST35-190	AST35-280	AST35-290	AST35-320	AST35-390	AST35-490
4"	SPUMBA	AST35-190	AST35-280	AST35-290	AST35-320	AST35-390	AST35-490
	RUPUMBA	AST35-190	AST35-280		AST35-320		

		-		T.,	_!_	Y	
Mounting Option	Drilling Template	Single	2 @ 180	2@90	3 @ 90	3 @ 120	4@90
Head Location		Side B	Side B & D	Side B & C	Side B, C & D	Round Pole Only	Side A, B, C & D
Drill Nomenclature	#8	DM19AS	DM28AS	DM29AS	DM39AS	DM32AS	DM49AS

	Drilling Template		A	Minimum Accep	table Outside Po	ole Dimension	
SPA	#8	2-7/8"	2-7/8"	3.5"	3.5"	3"	3.5"
RPA	#8	2-7/8"	2-7/8"	3.5"	3.5"	3"	3.5"
SPUMBA	#5	2-7/8"	3"	4"	4"	3.5"	4"
RPIIMRA	#5	2-7/8"	3.5"	5"	5"	3.5"	5"

Isofootcandle plots for the DSX1 LED 60C 1000 40K. Distances are in units of mounting height (25').



Lumen Ambient Temperature (LAT) Multipliers

Use these factors to determine relative lumen output for average ambient temperatures from 0.40°C (32-104°F).

Am	bient	Lumen Multiplier
0°C	32°F	1.04
5°C	41°F	1.04
10°C	50°F	1.03
15°C	50°F	1.02
20°C	68°F	1.01
25°C	77°F	1.00
30°C	86°F	0.99
35°C	95°F	0.98
40°C	104°F	0.97

Projected LED Lumen Maintenance

Data references the extrapolated performance projections for the platforms noted in a **25°C ambient**, based on 10,000 hours of LED testing (tested per IESNA LM-80-08 and projected per IESNA TM-21-11).

To calculate LLF, use the lumen maintenance factor that corresponds to the desired number of operating hours below. For other lumen maintenance values, contact factory.

Operating Hours	Lumen Maintenance Factor
0	1.00
25,000	0.96
50,000	0.92
100,000	0.85

Ramp-down Time												
Tillic												
5 min												
*PIRTFC3V or PIRTFC3V or Output Output Output Output Output Sensitive Sensit												
*PIR1FC3V or 3V (37%) 10V (100%) Enabled @ 15C												

Electrical Load

					Current (A)					
	Performance Package	LED Count	Drive Current	Wattage	120	208	240	277	347	480
	P1	30	530	54	0.45	0.26	0.23	0.19	0.10	0.12
	P2	30	700	70	0.59	0.34	0.30	0.25	0.20	0.16
	P3	30	1050	102	0.86	0.50	0.44	0.38	0.30	0.22
	P4	30	1250	125	1.06	0.60	0.52	0.46	0.37	0.27
Forward Optics (Non-Rotated)	P5	30	1400	138	1.16	0.67	0.58	0.51	0.40	0.29
	P6	40	1250	163	1.36	0.78	0.68	0.59	0.47	0.34
	P7	40	1400	183	1.53	0.88	0.76	0.66	0.53	0.38
	P8	60	1050	207	1.74	0.98	0.87	0.76	0.64	0.49
	P9	60	1250	241	2.01	1.16	1.01	0.89	0.70	0.51
	P10	60	530	106	0.90	0.52	0.47	0.43	0.33	0.27
Rotated Optics	P11	60	700	137	1.15	0.67	0.60	0.53	0.42	0.32
(Requires L90 or R90)	P12	60	1050	207	1.74	0.99	0.87	0.76	0.60	0.46
	P13	60	1250	231	1.93	1.12	0.97	0.86	0.67	0.49

		Controls Options		
Nomenclature	Descripton	Functionality	Primary control device	Notes
FAO	Field adjustable output device installed inside the lumiaire; wired to the driver dimming leads.	Allows the lumiaire to be manually dimmed, effectively trimming the light output.	FAO device	Cannot be used with other controls options that need the 0-10V leads
DS	Drivers wired independantly for 50/50 luminaire operation	The luminaire is wired to two separate circuits, allowing for 50/50 operation.	Independently wired drivers	Requires two seperately switched circuits. Consider nLight AIR as a more cost effective alternative.
PER5 or PER7	Twist-lock photocell recepticle	Compatible with standard twist-lock photocells for dusk to dawn operation, or advanced control nodes that provide 0-10V dimming signals.	Twist-lock photocells such as DLL Elite or advanced control nodes such as ROAM.	Pins 4 & 5 to dimming leads on driver, Pins 6 & 7 are capped inside luminaire
PIR or PIRH	Motion sensors with integral photocell. PIR for 8-15' mounting; PIRH for 15-30' mounting	Luminaires dim when no occupancy is detected.	Acuity Controls SBGR	Also available with PIRH1FC3V when the sensor photocell is used for dusk-to-dawn operation.
NLTAIR2 PIRHN	nLight AIR enabled luminaire for motion sensing, photocell and wireless communication.	Motion and ambient light sensing with group response. Scheduled dimming with motion sensor over-ride when wirelessly connected to the nLight Eclypse.	nLight Air rSDGR	nLight AIR sensors can be programmed and commissioned from the ground using the CIAIRity Pro app.

Performance Data

Lumen Output

Lumen values are from photometric tests performed in accordance with IESNA LM-79-08. Data is considered to be representative of the configurations shown, within the tolerances allowed by Lighting Facts Contact factory for performance data on any configurations not shown here.

Forward 0	ptics																		
LED Count	Drive	Power	System	Dist.			30K K, 70 CRI	`				40K K, 70 CRI	`			(5000	50K K, 70 CRI)		
LED Count	Current	Package	Watts	Туре	Lumens	(3000 B	U U	G	LPW	Lumens	(4000 B	U U	G	LPW	Lumens	B	U	G	LPW
				T1S	6,457	2	0	2	120	6,956	2	0	2	129	7,044	2	0	2	130
				T2S T2M	6,450 6,483	1	0	2	119 120	6,949 6,984	2	0	2	129 129	7,037 7,073	2	0	2	130
				T3S	6,279	2	0	2	116	6,764	2	0	2	129	6,850	2	0	2	131 127
				T3M	6,468	1	0	2	120	6,967	1	0	2	129	7,056	1	0	2	131
				T4M	6,327	1	0	2	117	6,816	1	0	2	126	6,902	1	0	2	128
30	530	P1	54W	TFTM	6,464	2	0	0	120 124	6,963	3	0	2	129 134	7,051	3	0	2	131
				T5VS T5S	6,722 6,728	2	0	1	124	7,242 7,248	2	0	1	134	7,334 7,340	2	0	0	136 136
				T5M	6,711	3	0	1	124	7,229	3	0	1	134	7,321	3	0	2	136
				T5W	6,667	3	0	2	123	7,182	3	0	2	133	7,273	3	0	2	135
				BLC LCCO	5,299 3,943	1	0	2	98 73	5,709 4,248	1	0	2	106 79	5,781 4,302	1	0	2	107 80
				RCCO	3,943	1	0	2	73	4,248	1	0	2	79	4,302	1	0	2	80
				T1S	8,249	2	0	2	118	8,886	2	0	2	127	8,999	2	0	2	129
				T2S	8,240	2	0	2	118	8,877	2	0	2	127	8,989	2	0	2	128
				T2M T3S	8,283 8,021	2	0	2	118 115	8,923 8,641	2	0	2	127 123	9,036 8,751	2	0	2	129 125
				T3M	8,263	2	0	2	118	8,901	2	0	2	127	9,014	2	0	2	129
				T4M	8,083	2	0	2	115	8,708	2	0	2	124	8,818	2	0	2	126
30	700	P2	70W	TFTM	8,257	2	0	2	118	8,896	2	0	2	127	9,008	2	0	2	129
				T5VS T5S	8,588 8,595	3	0	1	123 123	9,252 9,259	3	0	0	132 132	9,369 9,376	3	0	0 1	134 134
				T5M	8,573	3	0	2	122	9,236	3	0	2	132	9,353	3	0	2	134
				T5W	8,517	3	0	2	122	9,175	4	0	2	131	9,291	4	0	2	133
				BLC	6,770	1	0	2	97	7,293	1	0	2	104	7,386	1	0	2	106
				LCCO RCCO	5,038 5,038	1	0	2	72 72	5,427 5,427	1	0	2	78 78	5,496 5,496	1	0	2	79 79
				T1S	11,661	2	0	2	114	12,562	3	0	3	123	12,721	3	0	3	125
				T2S	11,648	2	0	2	114	12,548	3	0	3	123	12,707	3	0	3	125
				T2M T3S	11,708 11,339	2	0	2	115 111	12,613 12,215	3	0	2	124 120	12,773 12,370	3	0	3	125 121
				T3M	11,680	2	0	2	115	12,582	2	0	2	123	12,742	2	0	2	125
				T4M	11,426	2	0	3	112	12,309	2	0	3	121	12,465	2	0	3	122
30	1050	P3	102W	TFTM	11,673	2	0	2	114	12,575	2	0	3	123	12,734	2	0	3	125
				T5VS T5S	12,140 12,150	3	0	1	119 119	13,078 13,089	3	0	1	128 128	13,244 13,254	3	0	1	130 130
				T5M	12,130	4	0	2	119	13,056	4	0	2	128	13,221	4	0	2	130
				T5W	12,040	4	0	3	118	12,970	4	0	3	127	13,134	4	0	3	129
				BLC	9,570	1	0	2	94	10,310	1	0	2	101	10,440	1	0	2	102
				LCCO RCCO	7,121 7,121	1	0	3	70 70	7,671 7,671	1	0	3	75 75	7,768 7,768	1	0	3	76 76
				T1S	13,435	3	0	3	107	14,473	3	0	3	116	14,657	3	0	3	117
				T2S	13,421	3	0	3	107	14,458	3	0	3	116	14,641	3	0	3	117
				T2M	13,490	2	0	2	108	14,532	3	0	3	116	14,716	3	0	3	118
				T3S T3M	13,064 13,457	3	0	2	105 108	14,074 14,497	3	0	3	113 116	14,252 14,681	3 2	0	3	114 117
				T4M	13,165	2	0	3	105	14,182	2	0	3	113	14,362	2	0	3	115
30	1250	P4	125W	TFTM	13,449	2	0	3	108	14,488	2	0	3	116	14,672	2	0	3	117
30	.250		12511	T5VS	13,987	4	0	1	112	15,068	4	0	1	121	15,259	4	0	1	122
				T5S T5M	13,999 13,963	3	0	2	112 112	15,080 15,042	3	0	2	121 120	15,271 15,233	3	0	2	122 122
				T5W	13,872	4	0	3	111	14,944	4	0	3	120	15,133	4	0	3	121
				BLC	11,027	1	0	2	88	11,879	1	0	2	95	12,029	1	0	2	96
				LCCO RCCO	8,205	1	0	3	66	8,839	1	0	3	71	8,951	1	0	3	72
				T1S	8,205 14,679	3	0	3	66 106	8,839 15,814	3	0	3	71 115	8,951 16,014	3	0	3	72 116
				T2S	14,664	3	0	3	106	15,797	3	0	3	114	15,997	3	0	3	116
				T2M	14,739	3	0	3	107	15,878	3	0	3	115	16,079	3	0	3	117
				T3S T3M	14,274 14,704	2	0	3	103 107	15,377 15,840	3	0	3	111 115	15,572 16,040	3	0	3	113 116
				T4M	14,704	2	0	3	107	15,840	3	0	3	112	15,692	3	0	3	114
30	1400	P5	138W	TFTM	14,695	2	0	3	106	15,830	3	0	3	115	16,030	3	0	3	116
30	1400	FJ	IJOVV	TSVS	15,283	4	0	1	111	16,464	4	0	1	119	16,672	4	0	1	121
				T5S T5M	15,295 15,257	3	0	2	111	16,477	4	0	2	119 119	16,686	4	0	2	121 121
				T5W	15,257	4	0	3	110	16,435 16,328	4	0	3	118	16,644 16,534	4	0	3	121
				BLC	12,048	1	0	2	87	12,979	1	0	2	94	13,143	1	0	2	95
				LCC0	8,965	1	0	3	65	9,657	1	0	3	70	9,780	1	0	3	71
				RCC0	8,965	1	0	3	65	9,657	1	0	3	70	9,780	1	0	3	71



Performance Data

Lumen Output

Lumen values are from photometric tests performed in accordance with IESNA LM-79-08. Data is considered to be representative of the configurations shown, within the tolerances allowed by Lighting Facts. Contact factory for performance data on any configurations not shown here.

Forward O	ptics																		
LED Count	Drive	Power	System	Dist.			30K K, 70 CRI)					40K K, 70 CRI)				50K K, 70 CRI		
	Current	Package	Watts	Туре	Lumens	В	U	G	LPW	Lumens	В	U	G	LPW	Lumens	В	U	G	LPW
				T1S	17,654	3	0	3	108	19,018	3	0	3	117	19,259	3	0	3	118
				T2S	17,635	3	0	3	108	18,998	3	0	3	117	19,238	3	0	3	118
				T2M	17,726	3	0	3	109	19,096	3	0	3	117	19,337	3	0	3	119
				T3S	17,167	3	0	3	105	18,493	3	0	3	113	18,727	3	0	3	115
				T3M	17,683	3	0	3	108	19,049	3	0	3	117	19,290	3	0	3	118
				T4M	17,299	3	0	3	106	18,635	3	0	4	114	18,871	3	0	4	116
40	1250	P6	163W	TFTM	17,672	3	0	3	108	19,038	3	0	4	117	19,279	3	0	4	118
40	1230		10511	T5VS	18,379	4	0	1	113	19,800	4	0	1	121	20,050	4	0	1	123
				T5S	18,394	4	0	2	113	19,816	4	0	2	122	20,066	4	0	2	123
				T5M	18,348	4	0	2	113	19,766	4	0	2	121	20,016	4	0	2	123
				T5W	18,228	5	0	3	112	19,636	5	0	3	120	19,885	5	0	3	122
				BLC	14,489	2	0	2	89	15,609	2	0	3	96	15,806	2	0	3	97
				LCC0	10,781	1	0	3	66	11,614	1	0	3	71	11,761	2	0	3	72
				RCCO	10,781	1	0	3	66	11,614	1	0	3	71	11,761	2	0	3	72
				T1S	19,227	3	0	3	105	20,712	3	0	3	113	20,975	3	0	3	115
				T2S	19,206	3	0	3	105	20,690	3	0	3	113	20,952	3	0	3	114
				T2M	19,305	3	0	3	105	20,797	3	0	3	114	21,060	3	0	3	115
				T3S	18,696	3	0	3	102	20,141	3	0	3	110	20,396	3	0	4	111
				T3M	19,258	3	0	3	105	20,746	3	0	3	113	21,009	3	0	3	115
				T4M	18,840	3	0	4	103	20,296	3	0	4	111	20,553	3	0	4	112
40	1400	P7	183W	TFTM T5VS	19,246	3	0	1	105 109	20,734	4	0	1	113 118	20,996		0	4	115 119
				T5S	20,017		-	2	109	21,564	4	0	2	118	21,837	4	0	2	119
				T5M	20,033 19,983	4	0	2	109	21,581	5	0	3	118	21,854	5	0	3	119
				T5W	19,852	5	0	3	109	21,527 21,386	5	0	3	117	21,799 21,656	5	0	3	118
				BLC	15,780	2	0	3	86	16,999	2	0	3	93	17,214	2	0	3	94
				LCCO	11,742	2	0	3	64	12,649	2	0	3	69	12,809	2	0	3	70
				RCCO	11,742	2	0	3	64	12,649	2	0	3	69	12,809	2	0	3	70
				T1S	22,490	3	0	3	109	24,228	3	0	3	117	24,535	3	0	3	119
				T2S	22,466	3	0	4	109	24,202	3	0	4	117	24,509	3	0	4	118
				T2M	22,582	3	0	3	109	24,327	3	0	3	118	24,635	3	0	3	119
				T3S	21,870	3	0	4	106	23,560	3	0	4	114	23,858	3	0	4	115
				T3M	22,527	3	0	4	109	24,268	3	0	4	117	24,575	3	0	4	119
				T4M	22,038	3	0	4	106	23,741	3	0	4	115	24,041	3	0	4	116
	1050	D 0	20714	TFTM	22,513	3	0	4	109	24,253	3	0	4	117	24,560	3	0	4	119
60	1050	P8	207W	T5VS	23,415	5	0	1	113	25,224	5	0	1	122	25,543	5	0	1	123
				T5S	23,434	4	0	2	113	25,244	4	0	2	122	25,564	4	0	2	123
				T5M	23,374	5	0	3	113	25,181	5	0	3	122	25,499	5	0	3	123
				T5W	23,221	5	0	4	112	25,016	5	0	4	121	25,332	5	0	4	122
				BLC	18,458	2	0	3	89	19,885	2	0	3	96	20,136	2	0	3	97
				LCC0	13,735	2	0	3	66	14,796	2	0	4	71	14,983	2	0	4	72
				RCCO	13,735	2	0	3	66	14,796	2	0	4	71	14,983	2	0	4	72
				T1S	25,575	3	0	3	106	27,551	3	0	3	114	27,900	3	0	3	116
				T2S	25,548	3	0	4	106	27,522	3	0	4	114	27,871	3	0	4	116
				T2M	25,680	3	0	3	107	27,664	3	0	3	115	28,014	3	0	3	116
				T3S	24,870	3	0	4	103	26,791	3	0	4	111	27,130	3	0	4	113
				T3M	25,617	3	0	4	106	27,597	3	0	4	115	27,946	3	0	4	116
				T4M	25,061	3	0	4	104	26,997	3	0	4	112	27,339	3	0	4	113
60	1250	P9	241W	TFTM	25,602	3	0	4	106	27,580	3	0	4	114	27,929	3	0	4	116
""	.250			T5VS	26,626	5	0	1	110	28,684	5	0	1	119	29,047	5	0	1	121
				T5S	26,648	4	0	2	111	28,707	5	0	2	119	29,070	5	0	2	121
				T5M	26,581	5	0	3	110	28,635	5	0	3	119	28,997	5	0	3	120
				T5W	26,406	5	0	4	110	28,447	5	0	4	118	28,807	5	0	4	120
				BLC	20,990	2	0	3	87	22,612	2	0	3	94	22,898	2	0	3	95
				LCC0	15,619	2	0	4	65	16,825	2	0	4	70	17,038	2	0	4	71
				RCC0	15,619	2	0	4	65	16,825	2	0	4	70	17,038	2	0	4	71



Performance Data

Lumen Output

Lumen values are from photometric tests performed in accordance with IESNA LM-79-08. Data is considered to be representative of the configurations shown, within the tolerances allowed by Lighting Facts. Contact factory for performance data on any configurations not shown here.

Rotated Op	otics																		
LED Count	Drive	Power	System	Dist.			30K K, 70 CRI					40K K, 70 CRI	`				50K K, 70 CRI)		
LED Count	Current	Package	Watts	Туре	Lumens	(3000 B	U U	G	LPW	Lumens	(4000 B	U	G	LPW	Lumens	(3000 B	U	G	LPW
				T1S	13,042	3	0	3	123	14,050	3	0	3	133	14,228	3	0	3	134
				T2S	12,967	4	0	4	122	13,969	4	0	4	132	14,146	4	0	4	133
				T2M	13,201	3	0	3	125	14,221	3	0	3	134	14,401	3	0	3	136
				T3S	12,766	4	0	4	120	13,752	4	0	4	130	13,926	4	0	4	131
				T3M	13,193	4	0	4	124	14,213	4	0	4	134	14,393	4	0	4	136
				T4M	12,944	4	0	4	122	13,945	4	0	4	132	14,121	4	0	4	133
60	530	P10	106W	TFTM	13,279	4	0	4	125	14,305	4	0	4	135	14,486	4	0	4	137
				TSVS	13,372	3	0	1	126	14,405	4	0	1	136	14,588	4	0	1	138
				T5S T5M	13,260 13,256	3	0	2	125 125	14,284 14,281	3 4	0	2	135 135	14,465 14,462	3	0	2	136 136
				T5W	13,137	4	0	3	123	14,153	4	0	3	134	14,402	4	0	3	135
				BLC	10,906	3	0	3	103	11,749	3	0	3	111	11,898	3	0	3	112
				LCCO	7,789	1	0	3	73	8,391	1	0	3	79	8,497	1	0	3	80
				RCCO	7,779	4	0	4	73	8,380	4	0	4	79	8,486	4	0	4	80
				T1S	16,556	3	0	3	121	17,835	3	0	3	130	18,061	4	0	4	132
				T2S	16,461	4	0	4	120	17,733	4	0	4	129	17,957	4	0	4	131
				T2M	16,758	4	0	4	122	18,053	4	0	4	132	18,281	4	0	4	133
				T3S	16,205	4	0	4	118	17,457	4	0	4	127	17,678	4	0	4	129
				T3M	16,748	4	0	4	122	18,042	4	0	4	132	18,271	4	0	4	133
				T4M	16,432	4	0	4	120	17,702	4	0	4	129	17,926	4	0	4	131
60	700	P11	137W	TFTM T5VS	16,857	4	0	4	123	18,159	4	0	1	133 133	18,389	4	0	1	134 135
				T5S	16,975 16,832	4	0	1	124 123	18,287 18,133	4	0	2	132	18,518 18,362	4	0	2	134
				T5M	16,828	4	0	2	123	18,128	4	0	2	132	18,358	4	0	2	134
				T5W	16,677	4	0	3	122	17,966	5	0	3	131	18,193	5	0	3	133
				BLC	13,845	3	0	3	101	14,915	3	0	3	109	15,103	3	0	3	110
				LCC0	9,888	1	0	3	72	10,652	2	0	3	78	10,787	2	0	3	79
				RCCO	9,875	4	0	4	72	10,638	4	0	4	78	10,773	4	0	4	79
				T1S	22,996	4	0	4	111	24,773	4	0	4	120	25,087	4	0	4	121
				T2S	22,864	4	0	4	110	24,631	5	0	5	119	24,943	5	0	5	120
				T2M	23,277	4	0	4	112	25,075	4	0	4	121	25,393	4	0	4	123
				T3S	22,509	4	0	4	109	24,248	5	0	5	117	24,555	5	0	5	119
				T3M	23,263	4	0	4	112	25,061	4	0	4	121	25,378	4	0	4	123
				T4M TFTM	22,824 23,414	5	0	5	110 113	24,588 25,223	5	0	5	119 122	24,899 25,543	5	0	5	120 123
60	1050	P12	207W	T5VS	23,579	5	0	1	114	25,223	5	0	1	123	25,722	5	0	1	123
				TSS	23,380	4	0	2	113	25,187	4	0	2	122	25,722	4	0	2	123
				T5M	23,374	5	0	3	113	25,181	5	0	3	122	25,499	5	0	3	123
				T5W	23,165	5	0	4	112	24,955	5	0	4	121	25,271	5	0	4	122
				BLC	19,231	4	0	4	93	20,717	4	0	4	100	20,979	4	0	4	101
				LCC0	13,734	2	0	3	66	14,796	2	0	4	71	14,983	2	0	4	72
				RCCO	13,716	4	0	4	66	14,776	4	0	4	71	14,963	4	0	4	72
				T1S	25,400	4	0	4	110	27,363	4	0	4	118	27,709	4	0	4	120
				T2S	25,254	5	0	5	109	27,205	5	0	5	118	27,550	5	0	5	119
				T2M	25,710	4	0	4	111	27,696	4	0	4	120	28,047	4	0	4	121
				T3S T3M	24,862 25,695	5	0	5	108 111	26,783 27,680	5	0	5	116 120	27,122 28,031	5	0	5	117 121
				T4M	25,093	5	0	5	109	27,000	5	0	5	118	27,502	5	0	5	119
				TFTM	25,861	5	0	5	112	27,136	5	0	5	121	28,212	5	0	5	122
60	1250	P13	231W	T5VS	26,043	5	0	1	113	28,056	5	0	1	121	28,411	5	0	1	123
				TSS	25,824	4	0	2	112	27,819	5	0	2	120	28,172	5	0	2	122
				T5M	25,818	5	0	3	112	27,813	5	0	3	120	28,165	5	0	3	122
				T5W	25,586	5	0	4	111	27,563	5	0	4	119	27,912	5	0	4	121
				BLC	21,241	4	0	4	92	22,882	4	0	4	99	23,172	4	0	4	100
				LCC0	15,170	2	0	4	66	16,342	2	0	4	71	16,549	2	0	4	72
				RCCO	15,150	5	0	5	66	16,321	5	0	5	71	16,527	5	0	5	72



+ Capable Luminaire

This item is an A+ capable luminaire, which has been designed and tested to provide consistent color appearance and system-level interoperability.

- All configurations of this luminaire meet the Acuity Brands' specification for chromatic consistency
- This luminaire is A+ Certified when ordered with DTL® controls marked by a shaded background. DTL DLL equipped luminaires meet the A+ specification for luminaire to photocontrol interoperability1
- This luminaire is part of an A+ Certified solution for ROAM® or XPoint™ Wireless control networks, providing out-of-the-box control compatibility with simple commissioning, when ordered with drivers and control options marked by a shaded background¹

To learn more about A+, visit www.acuitybrands.com/aplus.

- 1. See ordering tree for details.
- 2. A+ Certified Solutions for ROAM require the order of one ROAM node per luminaire. Sold Separately: Link to Roam; Link to DTL DLL

FEATURES & SPECIFICATIONS

INTENDED USE

The sleek design of the D-Series Size 1 reflects the embedded high performance LED technology. It is ideal for many commercial and municipal applications, such as parking lots, plazas, campuses, and streetscapes.

CONSTRUCTION

Single-piece die-cast aluminum housing has integral heat sink fins to optimize thermal management through conductive and convective cooling. Modular design allows for ease of maintenance and future light engine upgrades. The LED drivers are mounted in direct contact with the casting to promote low operating temperature and long life. Housing is completely sealed against moisture and environmental contaminants (IP65). Low EPA (1.01 ft²) for optimized pole wind loading.

FINISH

Exterior parts are protected by a zinc-infused Super Durable TGIC thermoset powder coat finish that provides superior resistance to corrosion and weathering. A tightly controlled multi-stage process ensures a minimum 3 mils thickness for a finish that can withstand extreme climate changes without cracking or peeling. Available in both textured and non-textured finishes.

OPTICS

Precision-molded proprietary acrylic lenses are engineered for superior area lighting distribution, uniformity, and pole spacing. Light engines are available in standard 3000 K, 4000 K and 5000 K (70 CRI) configurations. The D-Series Size 1 has zero uplight and qualifies as a Nighttime Friendly™ product, meaning it is consistent with the LEED® and Green Globes™ criteria for eliminating wasteful uplight.

ELECTRICAL

Light engine configurations consist of high-efficacy LEDs mounted to metal-core circuit boards to maximize heat dissipation and promote long life (up to L85/100,000 hours at 25°C). Class 1 electronic drivers are designed to have a power factor >90%, THD <20%, and an expected life of 100,000 hours with <1% failure rate. Easily serviceable 10kV surge protection device meets a minimum Category C Low operation (per ANSI/IEEE C62.41.2).

STANDARD CONTROLS

The DSX1 LED area luminaire has a number of control options. Dusk to dawn controls can be utilized via optional NEMA twist-lock photocell receptacles. Integrated motion sensors with on-board photocells feature field-adjustable programing and are suitable for mounting heights up to 30 feet.

nLIGHT AIR CONTROLS

The DSX1 LED area luminaire is also available with nLight® AIR for the ultimate in wireless control. This powerful controls platform provides out-of-the-box basic motion sensing and photocontrol functionality and is suitable for mounting heights up to 40 feet. Once commissioned using a smartphone and the easy-to-use CLAIRITY app, nLight AIR equipped luminaries can be grouped, resulting in motion sensor and photocell group response without the need for additional equipment. Scheduled dimming with motion sensor over-ride can be achieved when used with the nLight Eclypse. Additional information about nLight Air can be found here.

INSTALLATION

Included mounting block and integral arm facilitate quick and easy installation. Stainless steel bolts fasten the mounting block securely to poles and walls, enabling the D-Series Size 1 to withstand up to a 3.0 G vibration load rating per ANSI C136.31. The D-Series Size 1 utilizes the AERIS™ series pole drilling pattern (template #8). NEMA photocontrol receptacle are also available.

LISTINGS

UL Listed for wet locations. Light engines are IP66 rated; luminaire is IP65 rated. Rated for -40°C minimum ambient. U.S. Patent No. D672,492 S. International patent pending.

DesignLights Consortium® (DLC) Premium qualified product and DLC qualified product.

Not all versions of this product may be DLC Premium qualified or DLC qualified. Please check the DLC Qualified Products List at www.designlights.org/QPL to confirm which versions are qualified.

International Dark-Sky Association (IDA) Fixture Seal of Approval (FSA) is available for all products on this page utilizing 3000K color temperature only.

WARRANTY

5-year limited warranty. Complete warranty terms located at: www.acuitybrands.com/CustomerResources/Terms_and_conditions.aspx

Note: Actual performance may differ as a result of end-user environment and application.

All values are design or typical values, measured under laboratory conditions at 25 $^{\circ}\text{C}.$

Specifications subject to change without notice.



Application

LED bollard with shielded 180° light distribution. This luminaire is designed to provide one sided illumination of ground surfaces. Provided with mounting system that allows the luminaire to be adjusted independent of anchor bolt orientation.

Materials

Luminaire housing and base constructed of die-cast and extruded marine grade, copper free (≤0.3% copper content) A360.0 aluminum alloy Borosilicate glass lens

Reflector made of pure anodized aluminum

High temperature silicone gasket

Mechanically captive stainless steel fastener

NRTL listed to North American Standards, suitable for wet locations

Protection class IP65

Weight: 9.7 lbs

Electrical
Operating voltage 120-277VAC
Minimum start temperature -20°C
LED module wattage 7.2W
System wattage 10.0W

Controllability 0-10V dimmable

Color rendering index Ra > 80

 Luminaire lumens
 411 lumens (3000K)

 Lifetime at Ta = 15° C
 77,000 h (L70)

 Lifetime at Ta = 55° C
 53,000 h (L70)

LED color temperature

4000K - Product number + **K4** 3500K - Product number + **K35** 3000K - Product number + **K3** 2700K - Product number + **K27**

BEGA can supply you with suitable LED replacement modules for up to 20 years after the purchase of LED luminaires - see website for details

Finish

All BEGA standard finishes are matte, textured polyester powder coat with minimum 3 mil thickness.

Available colors Black (BLK) White (WHT) RAL:

Bronze (BRZ) Silver (SLV) CUS:



H. Sandy Health Clinic

Type: - Exterior Light Fixture

BEGA Cut-Sheets

Project: Modified:



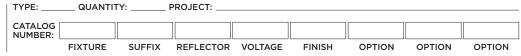


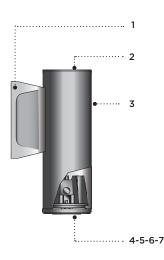
 LED
 A
 B
 Anchorage

 77752
 7.2 W
 6 ½
 8 %
 79817



3" WALL UP OR DOWN LIGHT





- 1- Cast aluminum driver housing, includes galvanized steel wall mount pressure plate.
- 2- Cast aluminum top cover.
- 3- Extruded aluminum cylindrical housing.
- 4- Fully sealed cast aluminum light assembly.
- 5- Sealed cast aluminum lens frame.
- 6- Clear tempered glass lens.
- 7- Faceted specular aluminum reflector.

All stainless steel hardware.



MATERIALS

Syrios LED is made of corrosion resistant 356 aluminum alloy with a copper (CU) content of less than 0.1%.

The main housing is made of seamless extruded aluminum, with an integrally sealed LED light module designed for optimal heat dissipation, and lighting performance.

Syrios LED SY300 series is standard with 29º optic. See options section for alternate selection.

ELECTRICAL

DRIVER

Standard driver is 0-10V dimming-ready (dims to 10%) with: 120-277 multi-volt compatibility (50-60Hz), operating temperature range of -30°C/-22°F to 55°C/131°F, output over voltage protection, output over current protection and output short circuit protection with auto-recovery.

LED Standard 4000K /80CRI, Optional 2700K, 3000K & 3500K.

Optional Amber LED for turtle sensitive areas.

Wavelengths: 584.5nm to 597nm.

LIFE

60,000hrs $L_{70}B_{50}$ (based on IESNA TM-21 Test Method and LM-80 data). Up to 95,000hrs L₇₀B₅₀ (calculated projection from LM-80 data).

FINISH

Five-stage preparation process including preheating of cast aluminum parts for air extraction, and an environmentally friendly alloy sealant. Polyester powder coating is applied through an electrostatic process and oven cured for long term finish.

MOUNTING

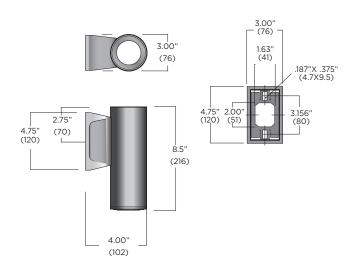
Maximum weight: 2.5lbs (1.1kg)

The mounting plate is designed to fit on a 2X4" (51x102) rectangular electrical box using 3.156" (80) C/C mounting holes.

Optional trimming plate for octagonal jbox (option MT4).

CERTIFICATION

Tested to UL1598 and CSA 22.2 #250. ETL listed wet location. Rated IP66. CE Certification on request.



LUMINAIRE SELECTION

MODEL#	LED LIGHT	SELECTION				REFLEC.	TORS*	VOLTAGE	FINISH
	SUFFIX	INPUT WATTS	DELIVERED LUMENS	CRI	CCT ºK				STANDARD COLORS
□ SY300	□ L1L10 AMBER L □ L1L1K:	. ED IDA - Dark Sky	924 y Approved 124	80 AMBER	4000	*Dependir installed a downlight	Flood optics 29° (standard) Wide flood optics 42° ng on direction fixture is add U (for uplight) or D (for t) to suffix for all reflectors ove. (i.e. R40U is 42° uplight)	□ 120V □ 277V	□ WHT Snow white □ BKT Jet black □ BZT Bronze □ MST Matte silver □ GRT Titanium gray □ DGT Gun metal □ CHT Champagne (Refer to color chart) OPTIONAL COLORS
	VERY NA □ L1L5N	.rrow distribu IR 10W	TION 539	80	4000	□ R9	Very narrow optics 9° Field angle 21° (12,018 candela)		☐ CS Custom color ☐ RAL RAL# color NATATORIUM SUITED COLORS ☐ NWHT White ☐ NBKT Black
OPTIONS									

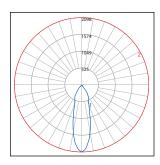
ELECTRICAL		LIGHT & OI	PTICS
☐ FS ☐ REML2-50	Fuse 7W remote emergency battery backup for LED, 90 min. Remote mount 50ft - 12" (305) square enclosure with access cover¹	Alternate ☐ K27 ☐ K3 ☐ K35	e CCT ⁹ K LED (LCF: Lumen conversion factor) 2700K CCT 80 CRI (LCF: 0.91) ³ IDA - Dark Sky Approved 3000K CCT 80 CRI (LCF: 0.94) IDA - Dark Sky Approved 3500K CCT 80 CRI (LCF: 0.983) ³
MOUNTING		NOTE: O	ther CCT & higher CRI available, please consult factory.
□ SWK □ MT4	Adaptor box for surface 3/4" conduit feed Trimming plate for octagonal box		
ACCESSORIES			
☐ SL ☐ LSL ☐ SNT ☐ HL	Solite lens Linear spread lens 1.5" (38) snoot ² Hexcell louver		

NOTES

- 1- The remote enclosure must be interior.
- 2- To prevent reflections, interior painted black when a light color finish is selected (ex. WHT, MST, GRT and CHT).
 3- Please consult factory when selecting K27 or K35 in conjuction with R9 (very narrow optics).

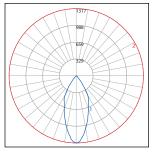


TYPICAL PHOTOMETRY SUMMARY



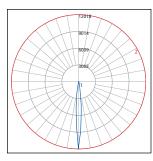
Descriptive Information

SY300-L1L10-R30 Total Lms: 924 Lumens Total Input Watts: 13 W Efficacy: 74 Lumens/Watt BUG: B1-U0-G0 CCT/CRI: 4000K/80 Maximum Candela: 2098 @ 0 deg



Descriptive Information

SY300-L1L10-R40 Total Lms: 846 Lumens Total Input Watts: 13 W Efficacy: 68 Lumens/Watt BUG: B1-U0-G0 CCT/CRI: 4000K/80 Maximum Candela: 1317 @ 0 deg

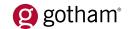


Descriptive Information

SY300-L1L5NR-R9
Total Lms: 539 Lumens
Total Input Watts: 10 W
Efficacy: 53 Lumens/Watt
BUG: B1-U0-G0
CCT/CRI: 4000K/80
Maximum Candela: 12018 @ 0 deg

Please visit our web site www.luminis.com for complete I.E.S. formatted download data.



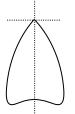


H. Sandy Health Clinic
- Exterior Light Fixture
Cut-Sheets



Luminaire Ty Catalog Number (autopopulated):





Gotham Architectural Downlighting LED Downlights









OPTICAL SYSTEM

- Self-flanged semi-specular, matte-diffuse or finishing trim
- Patented Bounding Ray[™] optical design (U.S. Patent No. 5,800,050)
- 45° cutoff to source and source image
- Top-down flash characteristic
- Polycarbonate lens integral to light engine

MECHANICAL SYSTEM

- Heavy-gauge aluminum construction
- Ceiling mount and wall mount for direct installation to 4" octagonal or square junction box
- Pendant mount entry for 3/8" National Pipe Thread stem; wires supplied by others
- Unique mounting mechanism at top of cylinders for easy one-person installation
- EDXB driver includes 3-foot DMX signal cable when ordered with FCM or WM mounting option. Fixture includes 10-foot DMX signal cable when ordered with PM or ACC mounting option.
- ACC180 provided with 15' 5-wire cord for power and 0-10V dimming

ELECTRICAL SYSTEM

- Fully serviceable and upgradeable LED light engine
- 70% lumen maintenance at 60,000 hours
- Tested according LM-79 and LM-80 standards
- 2.5 SDCM; 85 CRI typical, 90+ CRI optional
- Overload and short circuit protected
- Dimming wires supplied by others

LISTINGS

 Fixtures are CSA certified to meet US and Canadian standards; wet location, covered ceiling. ENERGY STAR® certified product.

WARRANTY

 5-year limited warranty. Complete warranty terms located at: www.acuitybrands.com/CustomerResources/Terms_and_conditions.aspx

Note: Actual performance may differ as a result of end user environment and application.

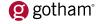
All values are design or typical values, measured under laboratory conditions at 25° C.



EXAMPLE: EVO CYL 35/10 6AR MWD LSS MVOLT EZ1 FCM DWHG

Series	Туре	Color	r erature		ninal en values			Aperture/ Trim colo		Trim type	e	Distri	bution ²	Finish	
EVO	CYL	27/ 30/ 35/ 40/ 50/	2700 K 3000 K 3500 K 4000 K 5000 K	10 15 20 25 30	1000 lumens 1500 lumens 2000 lumens 2500 lumens 3000 lumens	35 40 45	3500 lumens 4000 lumens 4500 lumens	6AR 6PR 6WTR 6GR 6WR ¹ 6BR ¹ 6WRAMF ¹	Clear Pewter Wheat Gold White Black White anti- microbial	(blank) W	Downlight Wallwash	ND MD MWD WWD	Very narrow (0.5 s/mh) Narrow (0.7 s/mh) Medium (0.9 s/mh) Medium wide (1.0 s/mh) Wide (1.2 s/mh)	LSS LD LS	Semi- specular Matte- diffuse Specular

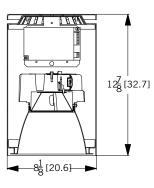
Voltage	Driver ³		Mountin	ng	Options			
MV0LT 120 277	GZ10 GZ1 EZ10 EZ1 EZB EDAB4 EDXB4 EXAB5 ECOS24.6	0-10V driver dims to 10% 0-10V driver dims to 1% eldoLED 0-10V ECOdrive. Linear dimming to 10% min. eldoLED 0-10V ECOdrive. Linear dimming to 1% min. eldoLED 0-10V SOLOdrive. Logarithmic dimming to <1%. eldoLED SOLOdrive DALI. Logarithmic dimming to <1%. eldoLED POWERdrive DMX with RDM (remote device management). Square Law dimming to <1%. Includes termination resistor. Refer to DMXR Manual. XPoint Wireless, eldoLED 0-10V ECOdrive. Linear dimming to 1%. Refer to XPoint tech sheet. XPoint Wireless, eldoLED 0-10V SOLOdrive. Logarithmic dimming to <1%. Refer to XPoint tech sheet. Lutron® Hi-Lume® 2-wire forward-phase driver. 120V only. Minimum dimming level 1%. Minimum lumen 1000/Maximum lumen 3000. Lutron® Hi-Lume® 3-wire or EcoSystem® dimming driver. Minimum dimming level 1%. Minimum lumen 1000/Maximum lumen 4500.	FCM WM ⁷ PM ACC ⁸ ACC180 ⁸	Ceiling mount Wall mount Pendant 3/8" thread mount 10ft aircraft cable and cord mount 15ft aircraft cable and cord mount	SF CRI90 NPP16D9 NPP16DER9 NPS80EZ8,10	Single fuse. Specify of High CRI (90+) nLight® network powe pack with 0-10V dimn non-eldoLED drivers (6Z1). nLight® network powe pack with 0-10V dimn non-eldoLED drivers (6Z1). ER controls fixtu emergency circuit. Sensor Switch® nLight dimming pack control eldoLED drivers (EZ_) Sensor Switch® nLight dimming pack controls eldoLED drivers. ER co fixtures on emergency operation (EZ_).	Powd et/relay ming for GZ10, DDB DBL et/relay DWH ming for GZ10, DMB GZ10, ures on DNA to DSS is 0-10V DGC TGC DTG	(standard) Dark bronze Black Gloss white

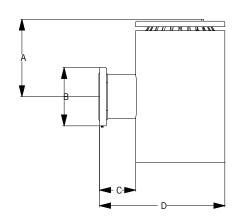


ELECTRICA

ACCESSORIES

NOTES





Reflector aperture: 6-1/4 (15.9) Housing diameter: 8-1/8 (20.3) Wall mount dimensions

A = 7-3/4 (19.7)

B = 5-5/16 (13.5)

C = 3-1/4 (8.3)

D = 10-7/8 (27.6)

	WATTAGE CO	NSUMPTION MAT	RIX
LUMENS	LM ACTUAL	WATTAGE	LUMENS per WATT
1000	1,059	11.8	90.1
1500	1,572	18.5	85.0
2000	2,058	23.2	88.9
2500	2,612	29.5	88.5
3000	3,077	36.6	84.1
3500	3,591	42.1	85.3
4000	4,046	48.1	84.2
4500	4,555	46.9	97.1

ACCESSORIES order as separate catalog numbers (shipped separately)

 ${
m CYS}^{12}$ 3/8" stem and canopy with 5° "hang straight" swivel

CRS¹² 3/8" stem and canopy with 45° swivel

CYSX¹² 3/8" stem and canopy with 5° "hang straight" swivel. Use this nomenclature

when ordering EDXB driver

CRSX¹²

3/8" stem and canopy with 45° swivel. Use this nomenclature when

ordering EDXB driver

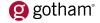
SDT 347/120 75VA¹³

347V Step-down transformer

ORDERING NOTES

- 1. Not available with finishes.
- 2. Not available with wallwash trim type.
- Refer to <u>TECH-240</u> for compatible dimmers.
 Not available with nLight[®] and XPoint options.
- 5. XPoint® CMRB ships separately.
- 6. Specify voltage 120V.
- Access panel (supplied by others) recommended for use with nLight® and XPoint®
- 8. White cord with white housings. All others black cord.

- Specify voltage. For use with generator supply EM power. Will require an emergency hot feed and normal hot feed.
- 10. Interface remote mounted.
- 11. Additional architectural colors available; see www.lithonia.com/archcolors.
- Color and length of stem must be specified (from 6" to 240" in even increments in maximum sections of 48"). Ex.: CYSO6 DWHG. Ceiling attachment for interior use. Consult factory for exterior use. Wire not included.
- 13. Transformer must be field-installed to an accessible remote-mounted junction box.



10% beam -

78.2°

6.0

12.2

15.4 3.8

55.2°

7.8 30.2 18.8

9.9

Inital FC Mounting Center Height 8.0

Beam

112.4

60.4 37.7

18.7

10.0 12.0

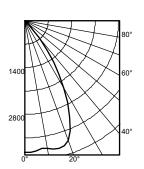
16.0



Distribution Data **Distribution Curve Output Data** Coefficient of Utilization Illuminance: Single Luminaire 30" Above Floor

EVO 35/40 6AR LS

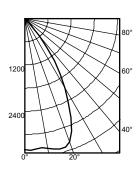
INPUT WATTS: 48.1, DELIVERED LUMENS: 4046, LM/W=84.1 , 1.03 S/MH, TEST NO. LTL27768



						pc		80%			70%			50%							
	Ave	Lumens	Zone	Lumens	% Lamp	pw	50%	30%	10%	50%	30%	10%	50%	30%	10%						
0	3935		0° - 30°	2904.3	71.8	0	119	119	119	116	116	116	111	111	111			50% be		10% be	
5	3901	371	0° - 40°	3830.0	94.7	1	111	108	106	109	106	104	105	103	101			54.4	l°	78.	1°
15	3944	1106	0° - 60°	4043.4	99.9	2	103	99	96	101	98	95	98	95	93		Inital FC				
25	3172	1427	0° - 90°	4046.3	100.0	3	96	91	87	95	90	87	92	88	85	Mounting	Center				
35	1508	926	90° - 180°	0.0	0.0	4	90	84	80	89	84	80	87	82	79	Height	Beam	Diameter	FC	Diameter	· FC
45	221	203	0° - 180°	4046.3	*100.0	5	84	78	74	83	78	74	81	77	73	8.0	130.1	5.7	65.1	8.9	13.0
55	6	10	*	Efficiency		6	79	73	69	78	73	68	77	72	68	10.0	70.0	7.7	35.0	12.2	7.0
65	2	2		-		7	74	68	64	73	68	64	72	67	63	12.0	43.6	9.8	21.8	15.4	4.4
75	1	1				8	70	64	60	69	63	60	68	63	59	14.0	29.8	11.8	14.9	18.7	3.0
85	0	0				9	66	60	56	65	60	56	64	59	56	16.0	21.6	13.9	10.8	21.9	2.2
90	0					10	62	56	52	62	56	52	61	56	52						

EVO 35/35 6AR LS

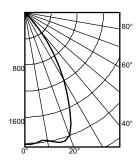
INPUT WATTS: 42.1, DELIVERED LUMENS: 3591, LM/W=85.3, 1.05 S/MH, TEST NO. LTL27767



						рс		80%			70%			50%	
	Ave	Lumens	Zone	Lumens	% Lamp	pw	50%	30%	10%	50%	30%	10%	50%	30%	10%
0	3400		0° - 30°	2579.3	71.8	0	119	119	119	116	116	116	111	111	111
5	3390	324	0° - 40°	3399.8	94.7	1	111	108	106	109	106	104	105	103	101
15	3497	981	0° - 60°	3586.3	99.9	2	103	99	96	101	98	95	98	95	93
25	2830	1274	0° - 90°	3590.5	100.0	3	96	91	87	95	90	87	92	88	85
35	1335	820	90° - 180°	0.0	0.0	4	90	84	80	89	84	80	87	82	79
45	193	177	0° - 180°	3590.5	*100.0	5	84	78	74	83	78	74	81	77	73
55	5	9	*	Efficiency		6	79	73	69	78	72	68	77	72	68
65	2	2				7	74	68	64	73	68	64	72	67	63
75	1	1				8	70	64	60	69	63	59	68	63	59
85	1	1				9	66	60	56	65	60	56	64	59	55
90	1					10	62	56	52	62	56	52	61	56	52

EVO 35/20 6AR LS

INPUT WATTS: 23.2, DELIVERED LUMENS: 2058, LM/W=88.7, 1.02 S/MH, TEST NO. LTL27777



	Ave	Lumens	Zone	Lumens	% Lamp
0	2018		0° - 30°	1498.5	72.8
5	1997	190	0° - 40°	1958.0	95.1
15	2053	576	0° - 60°	2056.6	99.9
25	1618	733	0° - 90°	2058.3	100.0
35	749	459	90° - 180°	0.0	0.0
45	105	94	0° - 180°	2058.3	*100.0
55	3	5	*	Efficiency	
65	1	1			
75	0	0			
85	0	0			
	•				

	pf		20%	
	рс	80%	70%	50%
р	pw	50% 30% 10%	50% 30% 10%	50% 30% 10%
	0	119 119 119	116 116 116	111 111 111
	1	111 108 106	109 107 105	105 103 101
	2	103 99 96	102 98 95	98 95 93
	3	96 92 88	95 91 87	92 89 86
	4	90 85 81	89 84 80	87 83 79
	5	84 79 74	83 78 74	82 77 73
	6	79 73 69	78 73 69	77 72 68
	7	74 68 64	74 68 64	72 67 64
	8	70 64 60	69 64 60	68 63 60
	9	66 60 56	66 60 56	65 60 56
	10	62 57 53	62 56 53	61 56 53

		50% be		10% beam - 77.3°	
	Inital FC				
Mounting	Center				
Height	Beam	Diameter	FC	Diameter	FC
8.0	66.7	5.6	33.4	8.8	6.7
10.0	35.9	7.7	17.9	12.0	3.6
12.0	22.4	9.7	11.2	15.2	2.2
14.0	15.3	11.8	7.6	18.4	1.5
16.0	11.1	13.8	5.5	21.6	1.1

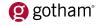
LUMEN OUTPUT MULTIPLIER - CRI						
CRI	FACTOR					
80 CRI	1					
90 CRI	0.79					

LUMEN OUTPUT MULTIPLIER - CCT						
CRI	FACTOR					
5000 K	1.101					
4000 K	1.035					
3500 K	1					
3000 K	0.973					
2700 K	0.938					

LUMEN OUTPUT MULTIPLIER - TRIM FINISH							
FINISH	CLEAR (AR)	PEWTER (PR)	WHEAT (WTR)	GOLD (GR)	WHITE (WR/WRAMF)	BLACK (BR)	
Specular (LS)	1.00	0.88	0.83	0.95	N/A	N/A	
Semi-specular (LSS)	0.95	0.84	0.79	0.90	N/A	N/A	
Matte-diffuse (LD)	0.85	0.73	0.69	0.80	N/A	N/A	
Paint	N/A	N/A	N/A	N/A	0.87	0.73	

PHOTOMETRY NOTES

- Tested in accordance with IESNA LM-79-08.
- Tested to current IES and NEMA standards under stabilized laboratory conditions.
- CRI: 85 typical.



Choose Wall Controls.

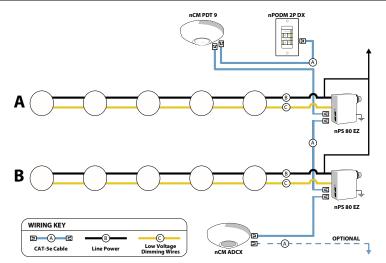
nLIGHT o ers multiple styles of wall controls – each with varying features and user experience.



Push-Button WallPod Traditional tactile buttons and LED user feedback



Graphic WallPodFull color touch screen provides a sophisticated look and feel



EXAMPLE

Group Fixture Control*

*Application diagram applies for fixtures with eldoLED drivers only.

nPS 80 EZ Dimming/Control Pack (qty 2 required)
nPODM 2P DX Dual On/Off/Dim Push-Button WallPod
nCM ADCX Daylight Sensor with Automatic Dimming Control
nCM PDT 9 Dual Technology Occupancy Sensor

Description: This design provides a dual on/off/dim wall station that enables manual control of the fixtures in Row A and Row B separately. Additionally, a daylight harvesting sensor is provided so the lights in row B can be configured to dim automatically when daylight is available. An occupancy sensor turns off all lights when the space is vacant.

nLight® Control Accessories: Order as separate catalog number. Visit <u>www.sensorswitch.com/nLight</u> for complete listing of nLight controls.

WallPod stations On/Off On/Off & Raise/Lower Graphic Touchscreen Photocell controls Dimming Model number nPODM [color]

nPODM DX [color] nPOD GFX [color] **Model number** nCM ADCX Occupancy sensors

Small motion 360°, ceiling (PIR / dual tech) Large motion 360°, ceiling (PIR / dual tech) Wide view (PIR / dual tech)

Wall Switch w/ Raise/Lower (PIR / dual tech)
Cat-5 cables (plenum rated)

10', CAT5 10FT 15', CAT5 15FT Model number

nCM 9 / nCM PDT 9 nCM 10 / nCM PDT 10 nWV 16 / nWV PDT 16

nWSX LV DX / nWSX PDT LV DX **Model number**

CAT5 10FT J1

****** Capable Luminaire

This item is an A+ capable luminaire, which has been designed and tested to provide consistent color appearance and out-of-the-box control compatibility with simple commissioning.

- All configurations of this luminaire meet the Acuity Brands' specification for chromatic consistency
- This luminaire is part of an A+ Certified solution for nLight* control networks when ordered with drivers marked by a shaded background*
- This luminaire is part of an A+ Certified solution for nLight control networks, providing advanced control functionality
 at the luminaire level, when selection includes driver and control options marked by a shaded background*

To learn more about A+, visit www.acuitybrands.com/aplus.

*See ordering tree for details



TARGETTI

BULLETTO

Compact Adjustable Flood Light Projector

Concept: Compact projector flood light for high intensity applications.

Materials: Aluminum body and joints for maximum heat dissapation powder coated in Ferrite Grey or Bronze finish. Modular body for toolless maintenance. Lens cover assymbly for simple toolless field interchangability of accessories.

Optics: NSP, SP, FL, MW, and WF use high efficiency LED Chip on Board. Equipped with collimating optic with angle specific holigraphic spread lens filters.

Mounting: Adjustable up to 180° on the vertical plane with aim locking set screw. Brass strain release gland with $\frac{1}{2}$ " NPT thread nipple that can be screwed directly to recieving mounting.

Installation: Pre-cabled with 10' Belden direct burial 18ga 3 Conductor Cable for Connection to remote power supply.

Finish: Ferrite Grey / Bronze

Power Supply: Remote Class 2, 120V-277VAC power supply required, see page 2

for options.

Wattage: 10W (NSP) / 12W (SP/FL/MF/WF)

Color Temperature: 2700°K / 3000°K / 3500°K / 4000°K

CRI: Ra84

Delivered Lumens: 3000°K

Narrow Spot 10° = 473Lm IMax: 24,196cd/klm Spot 15° = 858Lm IMax: 7,292cd/klm Flood 25° = 812Lm IMax: 2,883cd/klm Medium Wide Flood 30° = 819Lm IMax: 1,916cd/klm

Wide Flood 43° = 801Lm IMax: 1,009cd/klm

Lumen Maintenance (L70): 50,000hrs

Calculation for LED fixtures are based on measurements that comply with IES LM-80.

CRI: Ra84 Voltage: 24V DC IK Rating: IK10 IP Rating: IP66

Certifications: cULus Class 2 Wet Location Listed

Tested in accordance with LM-79-08 ^A Title 24 commercial installation compliant.

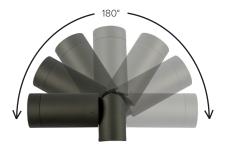
Warranty: 5 year limited warranty





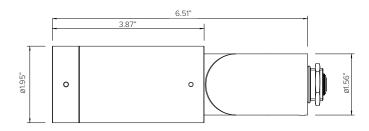






PRODUCT CODE	DRIVER	FINISH	ОИТРИТ	OPTICS	COLOR TEMP	+ POWER SUPPLY
BLT — BULLETTO	RP — Remote Power	FE - Ferrite Grey	L1 — 10W	NS — Narrow Spot 10°	27 — 2700K	See page 4
		BZ — Bronze	L2 — 12W	SP — Spot 15°	30 — 3000K	
				FL — Flood 25°	35 — 3500K	
				MF— Medium Wide Flood 30°	40 — 4000K	
				WF— Wide Flood 43°		

Views



TARGETTI

BULLETTO

INTERNAL OP	INTERNAL OPTICAL ACCESSORIES:						
Maximum of t	wo optical accessories per fixture.						
1E3798	Chromatic filter Red. Dimensions Ø50mm						
1E3799	Chromatic filter Green. Dimensions Ø50mm						
1E3800	Chromatic filter Blue. Dimensions Ø50mm						
1E3801	Chromatic filter Yellow. Dimensions Ø50mm						
1E3802	Chromatic filter Magenta. Dimensions Ø50mm						
1E3790	'Blade of Light' linear spread lens filter. Dimensions Ø50mm						
1E3792	Honeycomb filter. Dimensions Ø50mm						







EXTERNAL OPTICAL ACCESSORIES:			
Description		Description	
1E3788	1E3806	Asymmetric screen. Powder coated finish.	



Asymmetric Screen

INSTALLATION ACCESSORIES:				
Maximum of one installation accessory per fixture.				
Description				
1E3786	1E3804	Plate for fitting rotation. Powder coated stainless steel.		
1E3785	1E3803	Earthspike. Powder coated stainless steel.		
1BLTSMCVRFE	1BLTSMCVRBZ	Low Profile surface canopy. Powder coated aluminum with ½" NPT to mount over 4" Dia. X .5" H pancake j-box.		



Plate for Rotation Earthspike

Surface Mount Canopy



BULLETTO

Tree Mounting Accessories

TREE STRAP (REQUIRED) - CHOOSE 1

Durable 1.5 inch wide Nylon webbing Strap is flexible with High Strength Aircraft Aluminum V-ring Buckle in Gunmetal finish and lock in loop to prevent slipping. The strap is made to coordinate with up to 6 fixtures and 1 wiring connection box.

	The strup is mu	de to coordinate with up to o fixtures and I willing conficction box.
	TTS0101	Tree strap for trees 39" in circumference or smaller. Olive Green nylon strap with Gunmetal cinch buckle.
TTS0102 Tree strap for trees 39" in circumference or smaller. Coyote Brown nylon strap with Gunmetal cinch buckle. Tree strap for trees 39" in circumference or smaller. Graphite Grey nylon strap with Gunmetal cinch buckle.		· '
		· '



Shown with Tree Strap and Fixture Bracket

INSTALLATION STRAP (OPTIONAL)

Durable 1.5 inch wide Nylon webbing Strap is flexible with Metal Cinch Buckle and lock in loop to prevent slipping. The installation strap comes with 4 each 12 inch Rubber Loops used to hold up to 6 fixtures in place while positioning and tightening the Tree Strap in position during Installation or Maintenance and then removed for operation. *For use with 2 or more fixtures.*

TTIS0101

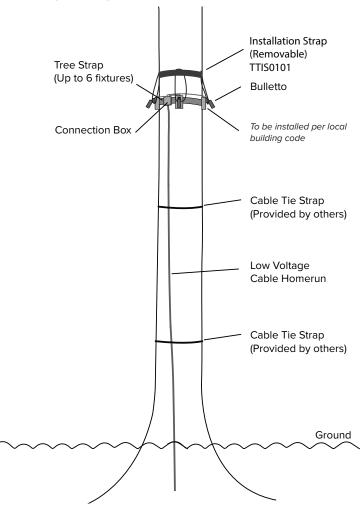
Installation strap flexible nylon webbing strap with metal cinch buckle and lock in loop. Includes 4 each 150mm rubber loops to hold up to 6 fixtures in place while positioning.

FIXTURE BRACKETS (REQUIRED) - CHOOSE 1			
Buckle style B	Buckle style Brackets for securing onto Tree Straps.		
Description		Description	
TTBLT0101	TTBLT0102	Bracket with stainless steel mounting screws.	

TREE STRAP	TREE STRAP CONNECTION BOX (OPTIONAL)			
Tree strap connection boxes are used to connect all multiple low voltage cables for one continuous cable connection down the tree, additional cable provided by others.				
Tree Strap Connection Box. Grey ABS plastic with internal terminal block for wire connections and 3 each ½" knockout for connections to 1 or 4 fixtures. Dimensions: 3¼" x 2½" x 13				
TTCB0104	Tree Strap Connection Box. Grey ABS plastic with internal terminal block for wire connections and 4 each ½" knockouts for connections to 5 or 6 fixtures. Dimensions: 4½" x 2½" x 1¾".			

MESH WIRE PROTECTION COVER (OPTIONAL)		
A braided polyethylene terepthalate (PET) monofilament yarn resistant to chemical degradation, UV radiation, and abrasion.		
TTSJS01	Carbon Grey 3/8" SJO Cord Sleeve (Sold per foot)	
TTSJS02 Brown 3/8" SJO Cord Sleeve (Sold per foot)		
TTSJS03	TTSJS03 Forest Green 3/8" SJO Cord Sleeve (Sold per foot)	

Wiring Configuration



Adjust the strap every 6 months in order to prevent tree damage.

TARGETTI

BULLETTO

Power Supply (REQUIRED)	Туре	Wattage	Input/Output Voltage	Dimmable	IP Rating	Output	Dimensions
DEL60PWM	ELECTRONIC PWM DRIVER STANDALONE, UL LISTED ENCLOSURE PROVIDED BY OTHERS	60W	120-277V / 24V	0-10V/PWM 10%	IP67	UR CLASS 2	5.9" X 2.09" X 1.38"
DEL90PWM	ELECTRONIC PWM DRIVER STANDALONE, UL LISTED ENCLOSURE PROVIDED BY OTHERS	90W	120-277V / 24V	0-10V/PWM 10%	IP67	UR CLASS 2	6.73" X 2.48" X 1.48"
DEDD10010	ELECTRONIC 0-10V DRIVER STANDALONE, UL LISTED ENCLOSURE PROVIDED BY OTHERS	100W	120-277V / 24V	0-10V DIMMING 0.1%	IP20	UR CLASS 2	6.02" x 1.97" x 0.91"
DELV40124D	ELECTRONIC LOW VOLTAGE TRANSFORMER	40W	120-277V / 24V	PHASE (120V ONLY) /0-10V DIMMING < 1%	IP66 / NEMA4 ENCLOSURE	UL CLASS 2	11" × 4" × 2.21"1
DELV60124D	ELECTRONIC LOW VOLTAGE TRANSFORMER	60W	120-277V / 24V	PHASE (120V ONLY) /0-10V DIMMING < 1%	IP66 / NEMA4 ENCLOSURE	UL CLASS 2	11" × 4" × 2.21"1
DELV96124D	ELECTRONIC LOW VOLTAGE TRANSFORMER	96W	120-277V / 24V	PHASE (120V ONLY) /0-10V DIMMING < 1%	IP67 / NEMA4 ENCLOSURE	UL CLASS 2	11" × 4" × 2.21"1
DELX601241CPWM	ELECTRONIC PWM DRIVER	60W	120-277V / 24V	0-10V/PWM 10%	IP67 / NEMA3R ENCLOSURE	UL CLASS 2	10" × 10" × 4"1
DELX901241CPWM	ELECTRONIC PWM DRIVER	90W	120-277V / 24V	0-10V/PWM 10%	IP67 / NEMA3R ENCLOSURE	UL CLASS 2	10" × 10" × 4"1
DELX1802242CPWM	ELECTRONIC PWM DRIVER	2X90W	120-277V / 24V	0-10V/PWM 10%	IP67 / NEMA3R ENCLOSURE	UL CLASS 2	12" × 12" × 4"1
DELX2703243CPWM	ELECTRONIC PWM DRIVER	3X90W	120-277V / 24V	0-10V/PWM 10%	IP67 / NEMA3R ENCLOSURE	UL CLASS 2	12" × 12" × 4" ¹
PS060	LUTRON HI-LUME PREMIER 0.1% CONSTANT VOLTAGE DRIVER WITH UL LISTED ENCLOSURE	96W	UNIVERSAL 120-277 VAC	HI-LUM DIMMABLE 0.1%	IP20/NOM CERTIFIED	UL CLASS 2	10.5" × 5.5" × 2" ¹
QOMELED1002410BK	QTRAN QOM-eLED CONSTANT VOLTAGE DRIVER WITH UL LISTED ENCLOSURE	100W	100-277V / 24V	0-10V	IP67	UR CLASS 2	15.4" X 9.22" X 4.90"
QOMELED2002410BK	QTRAN QOM-eLED CONSTANT VOLTAGE DRIVER WITH UL LISTED ENCLOSURE	2X100W	100-200V / 24V	0-10V	IP67	UR CLASS 2	15.4" X 9.22" X 4.90"
QOMDRIVE10024VBKDMX	QTRAN QOM-DRIVE-PS CONSTANT VOLTAGE DRIVER WITH UL LISTED ENCLOSURE	100W	100-277V / 24V	DMX CONTROL 4 CHANNEL	IP67	UR CLASS 2	15.4" X 9.22" X 4.90"
QOMDRIVE20024VBKDMX	QTRAN QOM-DRIVE-PS CONSTANT VOLTAGE DRIVER WITH UL LISTED ENCLOSURE	2X100W	100-200V / 24V	DMX CONTROL 4 CHANNEL	IP67	UR CLASS 2	15.4" X 9.22" X 4.90"

MAX FIXTURES PER DRIVER

a. 0				D	river W	attage			
ixture attage		40W	60W	96W	90W	2X90W	3X90W	100W	2X100
Fixture Wattage	10W	3	4	7	7	14	21	8	16
	12W	2	4	6	6	12	18	6	13

¹ Dimensions include enclosure with mounting bracket.

* Constant voltage drivers 50/60HZ, voltage regulated with short circuit protection. Operating temperature -40 C- 80° C

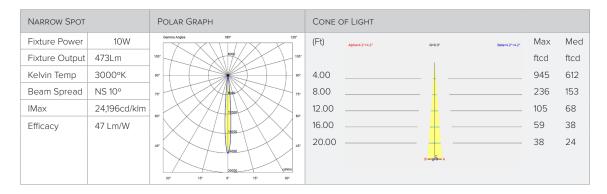
* Installation of power supply must be compliant to Class 2 installation standards. Refer to NEC and local building code requirements.

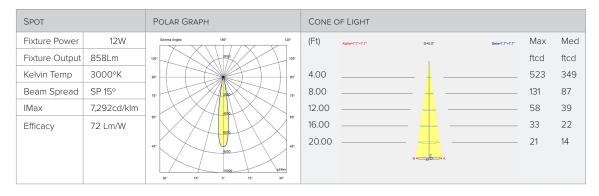
* Consult factory for additional driver options (ie: DMX, DALI, wattage, size, shape, Lutron, ELDO, or others).

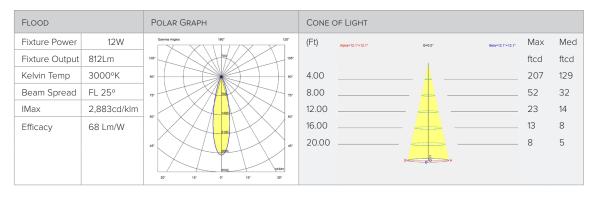
TARGETTI

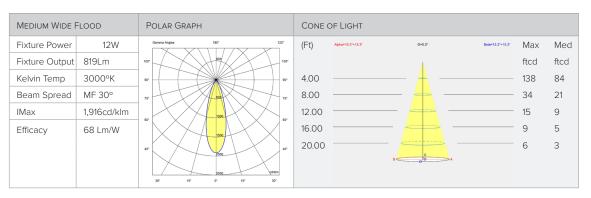
BULLETTO

Photometry





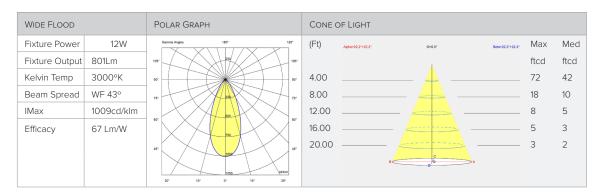






BULLETTO

Photometry Cont.

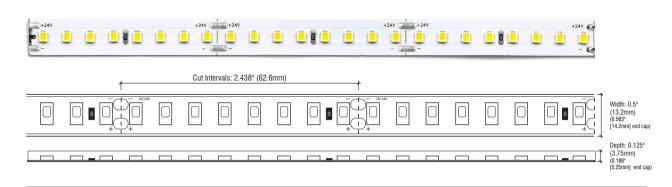




PERFORMANCE 500 (OUTDOOR)

PQ-SERIES | RUBBER COATED | LINEAR LED LIGHTING

ixture Type:	
Project:	
•	
Location:	



MODEL:	PQ27K-WR-24V	PQ3K-WR-24V	PQ35K-WR-24V	PQ41K-WR-24V	PQ5K-WR-24V
Kelvin	2700K	3000K	3500K	4100K	5000K
Lumens	508 lm/ft	530 lm/ft	551 lm/ft	572 lm/ft	594 lm/ft
Rating	IP67	IP67	IP67	IP67	IP67

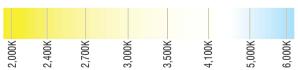
PRODUCT FEATURES

- 90+ CRI
- Dimmable
- 50,000 hour life
- 5-year warranty
- UL-listed for indoor and outdoor use
- 3M™ Industrial adhesive backing
- For use with 24V power supplies

SPECIFICATIONS

Series	PQ - Performance 500 (Outdoor)
Input Voltage	24V DC / Constant Voltage
Watts per Foot	2.6W/ft @ Maximum Run Length
Beam Spread	120°
Max Run Length	Unlimited, power every 25ft
Production Intervals	2.438" (62.6mm)
End Cap Dimensions	0.563" (14.2mm) × 0.188" (5.25mm)
Tape Dimensions	0.5" (13.2mm) × 0.125" (3.75mm)
CRI	90+
Diode	2835
Dimming Options	PWM, Triac, 0-10V, DMX, Hi-lume
Temp Range	-40°F (-40°C) to 149°F (65°C)

KELVIN COLOR TEMPERATURE SCALE



TOTAL WATTAGE USED AT EACH LENGTH

1ft	2ft	3ft	4ft	5ft	6ft	7ft	8ft	9ft	10ft	11ft	12ft	13ft
4.1	7.4	11.3	15.3	19.0	22.5	25.8	28.6	32.3	35.5	37.8	41.0	42.7
14ft	15ft	16ft	17ft	18ft	19ft	20ft	21ft	22ft	23ft	24ft	25ft	26ft
45.0	48.2	50.3	52.4	54.8	56.5	58.8	60.7	61.7	62.5	63.1	63.8	n/a

Conforms to ANSI/UL Standard 2108 Certified to CAN/CSA Standard C22.2 No. 250.0











TARGETTI

ZEDGE LINE

Professional Small Scale LED Steplight

S7 Fixture

H. Sandy Health Clinic
- Exterior Light Fixture
Cut-Sheets



Materials: Die-cast anodized aluminum body and external frame; powder coated frame.

Source: LED High Efficiency Board.

 $\begin{tabular}{ll} \textbf{Optic:} Polycarbonate opal screen. Floor Washer frame allows for uniform \\ \end{tabular}$

optical distribution on the floor and excellent visual comfort.

 $\textbf{Mounting:} \ \textbf{To be completed with a special nylon outer casing fitted for parallel} \\$

connection.

Driver: Integrated 4/1 driver (Non-dimmable / 0-10V / Reverse Phase / Forward

Phase). Dimmable to 1%. **Finish:** Ferrite Grey **Wattage:** 9W

Color Temperature: 2700°K / 3000°K / 3500°K / 4000°K

CRI: Ra84

Delivered Lumens: 2700°K 3000°K 3500°K 4000°K

230Lm 245Lm 251Lm 257Lm

Lumen Maintenance (L70): 50,000hrs

Calculation for LED fixtures are based on measurements that comply with IES LM-80.

Voltage: Universal Voltage 120-277V AC 50/60Hz

IK Rating: IK10 IP Rating: IP66

Certifications: cULus Listed Wet Location Tested in accordance with LM-79-08 ^ATitle 24 commercial installation compliant.

^B Consult factory for marine grade cataphoresis treatment.

Warranty: 5 year limited warranty

Designed in collaboration with Gensler as Product Design Consultant



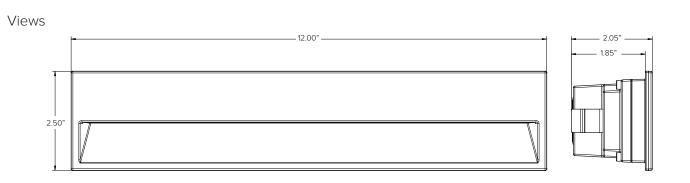








PRODUCT CODE	DRIVER	FACEPLATE	FINISH	WATTAGE	COLOR TEMP	+	INSTALLATION	
ZEL – ZEDGE LINE	(Non-Dimming /	FW – Floor Washer	FE — Ferrite Grey		27 — 2700K 30 — 3000K		See page 2	
	0-10V / Reverse Phase / Forward Phase)				35 — 3500K			
					40 — 4000K			



TARGETTI

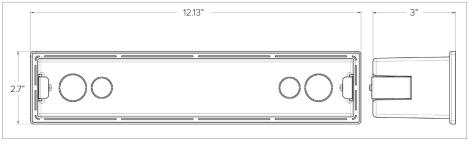
ZEDGE LINE

INSTALLATION (REQUIRED)

1E3447

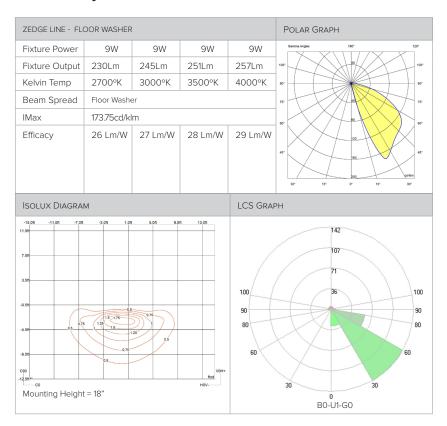
Nylon outer casing fitted for parallel connection with feed through-wiring. 34" and 1/2" knock-outs made for EMT connectors and conduit entry. Suitable for concrete pour, drywall, or stucco applications.

Dimensions: 12.13"W x 2.7"H x 3"D



1E3447

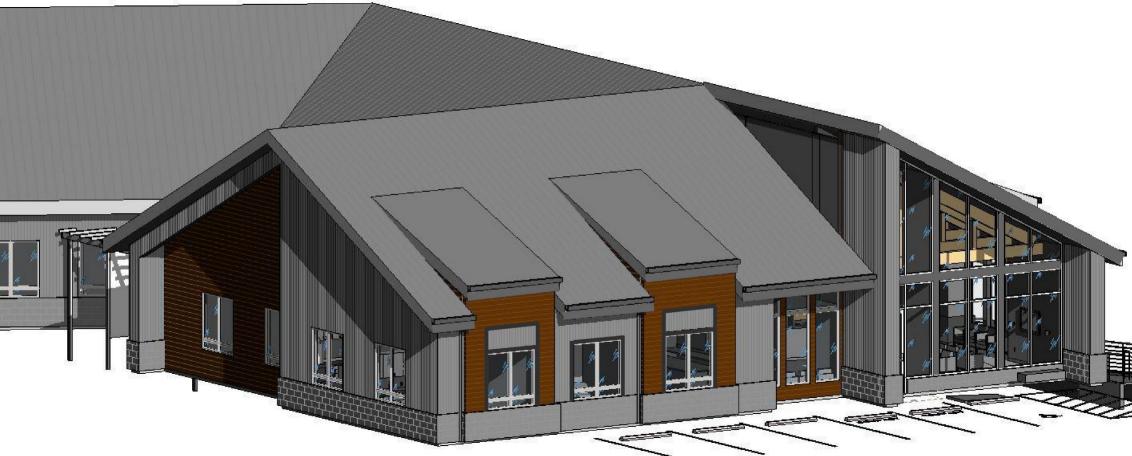
Photometry





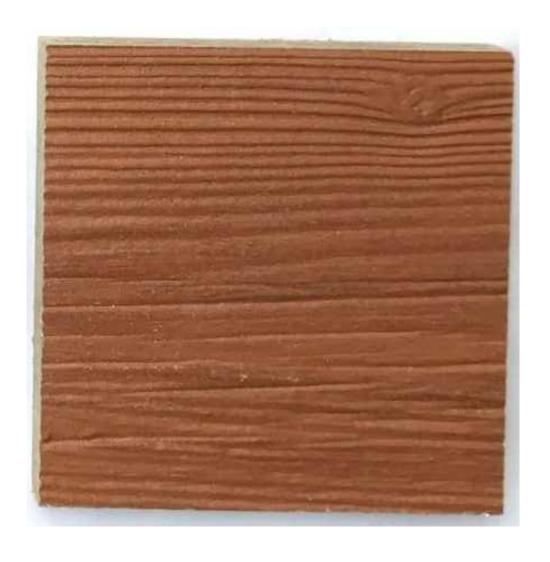




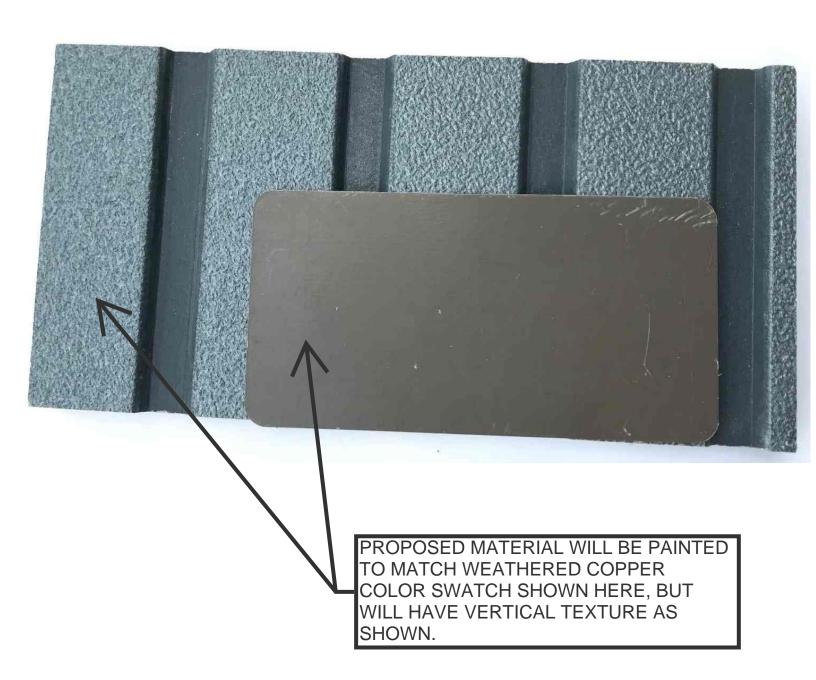




HORIZONTAL FIBER-CEMENT SIDING

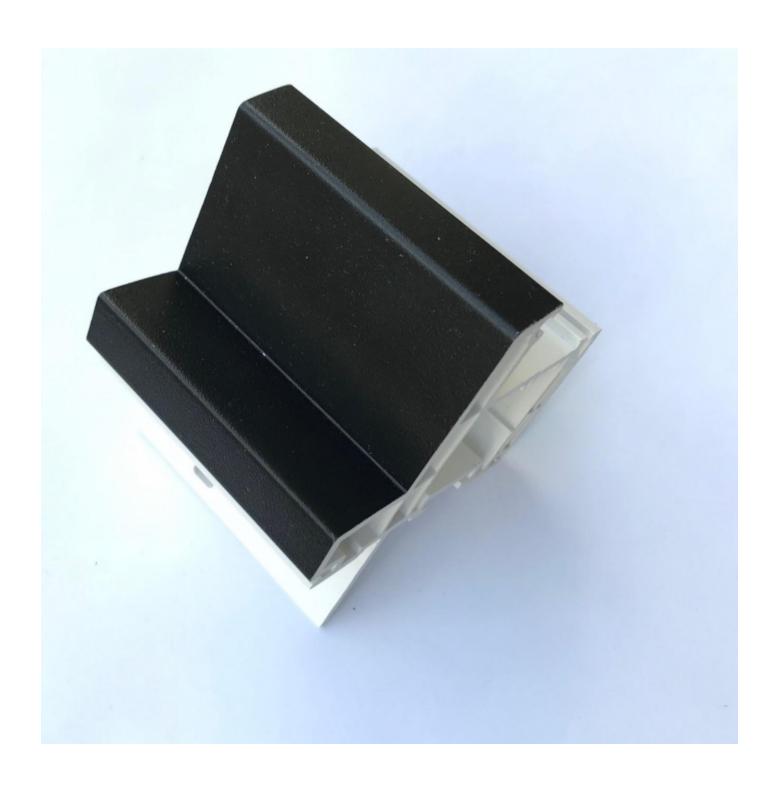


VERTICAL FIBER-CEMENT PANEL SIDING



STANDING SEAM METAL ROOFING





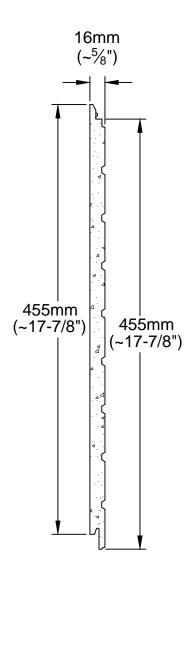
STURGIS GRAY TRIM AND FASCIA PAINT

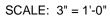


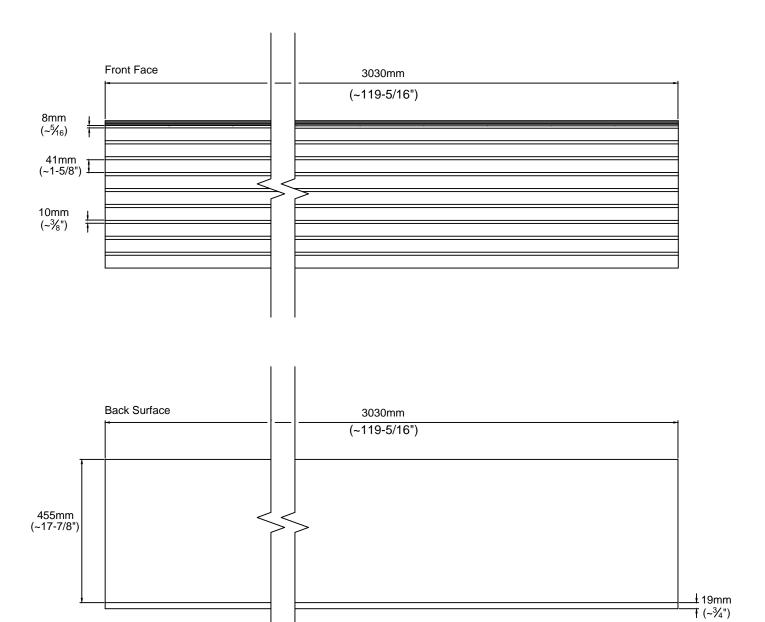
COMBINED BUILDING MATERIALS



Exhibit G







AWP-3030 - RIBBED - PANEL DETAIL

SCALE: 1" = 1'-0"









ARCHITECTURAL WALL PANELS | AWP3030 | JULY 2019

Vertical Installation Guide

AWP-3030 VERTICAL INSTALLATION GUIDE

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GENERAL

This guide is intended to provide the key information needed to successfully install Nichiha's 3030mm Architectural Wall Panels (AWP3030) in a vertical application. Further installation information and technical resources such as animated instructional videos, Technical Bulletins, three-part specifications, product testing and certifications, architectural details in AutoCAD, Revit, and PDF versions, and other technical documents are available on our website: nichiha.com/resource-center.

Install products in accordance with the latest installation guidelines and all applicable building codes and other laws, rules, regulations, and ordinances. Review all installation instructions and other applicable product documents before installation. This install guide's effective date is July 2019.

PRODUCT INSPECTION

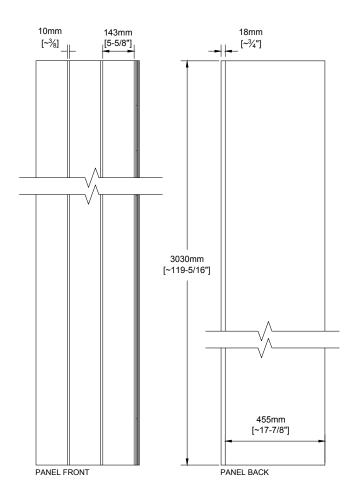
Inspect all products thoroughly prior to installation. Do not install any product which may have been damaged in shipment or appears to have a damaged or irregular finish. Should you have a question or problem with your order, contact your local dealer or Nichiha Customer Service, toll-free, at 1.866.424.4421. Keep the products dry prior to installation. It is best to store the products indoors, otherwise keep them covered. Do not stack pallets more than two high.

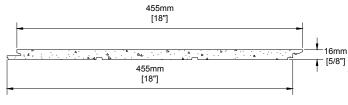
BASICS OF THE AWP3030 SYSTEM

Nichiha AWP3030 dimensions are 455mm (h) \times 3,030mm (l) \times 16mm (t). It is important to keep in mind the actual metric dimensions when considering panel layout, placement of control and compression joints, and with respect to sizing window and door openings. Approximate Imperial dimensions are 17-7/8" (h) \times 119-5/16" (l) \times 5/8" (t).

AWP3030 panel edges are shiplapped on the long edges and a factory sealant gasket is included on one edge, providing a factory seal on all vertical joints. AWP attachment hardware engages the long edges, holding the panels off the substrate surface by 10mm (~3/8") and creating a closed-joint, drained/back-ventilated rainscreen system with concealed fastening. When accounting for the overall thickness of the AWP system, add this 10mm plus the thickness of the panel (16mm) for total system thickness of 26mm.

AWP3030 may be installed horizontally or vertically. See also *Horizontal Installation Guide AWP1818*, AWP3030.





PANEL SECTION

VINTAGE WOOD PANEL DETAIL SCALE: 1" = 1'-0"

LIMITATIONS AND TECHNICAL DESIGN REVIEWS

Natural limitations on product usage are inherent to any cladding product's design, physical characteristics, and attachment system. Nichiha AWP are intended as a low-to-mid-rise cladding product.

Any project of more than three stories or 45 feet, as well as those located in high wind coastal areas (Exposure Categories C and D with Basic Wind Speed in excess of 130 mph), or those with any wall assembly not described in *Framing & Sheathing Requirements*, require a technical review by Nichiha to evaluate feasibility via our Technical Design Review process.

By evaluating a project's unique criteria and design, we can reference independently test-derived and calculated wind load performance data for our products to determine whether and how the panels can safely be installed on the project. Contact your local rep or Nichiha technical department for details or to initiate a Technical Design Review.

AWP are not to be used in any applications/uses not specified or described in this installation guide or other Nichiha technical documents. Any such use shall not be backed by the manufacturer's product warranty.

Do not use AWP on open screen walls.

Insulated Concrete Forms (ICFs) require additional measures.

Installation of AWP products on modular structures that are factory-constructed and then transported to a final site are not approved; and further, excluded from the Limited Product Warranty, per Section 2.F.

AWP installed as soffit is **not** covered by the Nichiha Product Warranty or the Nichiha Finish Warranty. Refer to pages 38-41 of the AWP Horizontal Installation Guide.

Please contact Nichiha Technical Services for assistance.

SAFETY

As with any natural stone, masonry, or concrete based product, when cutting, drilling, sawing, sanding, or abrading fiber cement cladding, proper safety measures must be taken due to the potential for airborne silica dust, an OSHA-identified hazardous substance that can pose serious medical risks.

Always wear safety glasses and a NIOSH/OSHA approved respirator with a rating of N, O, or P 100. Carefully follow the respirator manufacturer's instructions as well as applicable governmental safety regulations concerning silica. Refer to Nichiha's SDS for more information.

Always cut fiber cement panels outside and with a dust-collecting HEPA system. Do not cut the products in an enclosed area.

Use a dust-reducing circular saw with diamond-tipped or carbide-tipped fiber cement saw blades.

Always clean panels after cutting. Fiber cement dust can bind to the panel finish. Vacuum dust with a HEPA-filtered vacuum.

FRAMING AND SHEATHING REQUIREMENTS

Prior to Nichiha installation, closely inspect exterior wall substrate and correct any problems. Walls that are out of plumb, for example, can negatively impact the installation quality of AWP. Nichiha Spacer may be used in conjunction with panel attachment hardware if necessary to ensure a smooth, even substrate.

With conventional stud spacing, 7/16" or thicker APA rated OSB or Plywood sheathing *must* be used as the fastening base for Vertical AWP3030 as the panel size module will not align with framing. If nail-base insulation sheathing is considered, please contact Nichiha Technical as additional measures may be required. Alternatively, studs or furring may be spaced at 45.5cm (17-7/8") o.c. to allow fastening of AWP hardware directly to framing.

Refer to our third party building code certification(s) and/or state/local approvals for allowable wind design pressures at nichiha.com/resource-center.

Nichiha AWP cladding may be installed on vertical walls only. No tilted/sloped walls, nor true radius/curved walls. Vertical AWP installations are not compatible with PEMBs. AWP may be installed on wood or steel framing, concrete/masonry with furring, and Structural Insulating Panels (SIP) meeting the following requirements:

WOOD STUDS

Structural Sheathing Method Size: minimum 2"x4" studs

Spacing: 16" o.c. max

Sheathing: APA rated exterior grade minimum

7/16" plywood/OSB required

Custom Stud/Furring Spacing Method

Size: minimum 2"x4" studs Spacing: 45.5cm (17-7/8") o.c.

Sheathing: APA rated exterior grade minimum 7/16" plywood/OSB, 1/2" or 5/8" gypsum

METAL STUDS

Structural Sheathing Method

Gauge: minimum 18 Spacing: 16" o.c. max

Sheathing: APA rated exterior grade minimum 7/16"

plywood/OSB required

Custom Stud/Furring Spacing Method

Gauge: minimum 18

Spacing: 45.5cm (17-7/8") o.c.

Sheathing: APA rated exterior grade minimum 7/16"

plywood/OSB, 1/2" or 5/8" gypsum

CONCRETE/MASONRY

Furring is required for installation of AWP over concrete and masonry structures.

Wood Furring: pressure treated lumber 2"x4", oriented vertically, spaced 45.5cm (17-7/8") o.c. max with additional vertical furring segments at Vertical Starter Track locations to enable 9" o.c. fastener spacing for track.

Metal Furring: hat channel, c-stud, or z-furring, minimum 18 gauge with 1"- 2" flanges, oriented vertically, spaced 45.5cm (17-7/8") o.c. max. with additional vertical furring segments at Vertical Starter Track locations to enable 9" o.c. fastener spacing for track.

Sheathing: exterior grade minimum 7/16" plywood/ OSB required with furring spacing other than 45.5cm (17-7/8") o.c.

STRUCTURAL INSULATING PANELS (SIP)

SIPs should be installed in accordance with manufacturer's instructions and local building codes. Additional special Nichiha installation requirements for SIPs are discussed in the Fasteners and Installing the First Course sections to follow.

For buildings greater than one story, contact Technical Department for assistance.

CONTINUOUS INSULATION

When exterior/continuous insulation is to be used with AWP3030 in vertical applications, please contact Nichiha *Technical Services* for assistance. Framing/sheathing/furring alternatives will be necessary.

Also refer to the Technical Bulletin:

Continuous Insulation and AWP available at
Nichiha.com/resource-center.

VERTICAL AWP3030 OVER C.I. ATTACHMENT REQUIREMENTS

When adding a furring grid* to enable AWP installation over c.i., the following general criteria are applicable:

Special attention must be paid to supporting the Vertical Starter Track, which bears the weight of AWP3030 in vertical applications. The clips do not share the dead loads for vertical panels.

- 1. Shaped metal furrings (Z, hat channel, C, etc.)
 - Minimum 18 gauge
 - Aligned vertically
 - Spaced 16" o.c. (max)
 - Min. 7/16" APA Rated OSB or Plywood

- or -

2. Pressure treated lumber

- Minimum 2x (1.5") thickness
- Aligned vertically
- Spaced 16" o.c. (max.)
- Min. 7/16" APA Rated OSB or Plywood

- or -

- 3. Shaped metal furrings (one layer)
 - Minimum 18 gauge
 - Aligned vertically at 17-7/8" o.c.
 - Additional vertical furring segments at Vertical Starter Track locations to enable
 9" o.c. fastener spacing for track

- or -

- 4. Shaped metal furrings (two layers)
 - (Z, hat channel, C, etc.)
 - Layer One
 - Minimum 18 gauge
 - Aligned horizontally
 - Spaced per engineer's design
 - Layer Two
 - Minimum 18 gauge
 - Aligned vertically at 17-7/8" o.c.
 - Additional vertical furring segments at Vertical Starter Track locations to enable 9" o.c. fastener spacing for track.

- or -

5. CL-TALON® 300

- Base Track and Wall Mount T-Tracks (vertical) at 16" o.c. (aligned with framing), and Therme Clips spaced per project loading requirements
- Wall Mount Supports (horizontal) at 16" o.c.

*Consult a structural engineer to design the furring system to manage the AWP system dead load of minimum 4 psf and also meet the project wind load design criteria. Furring must account for expected building compression. Nichiha does not provide fastener design for anchoring the furring to structure. Refer to IBC 2015 Table 2603.12.2 for more info.

ACCESSORY ATTACHMENTS

Nichiha Double and Single Flange Sealant Backers and metal trims, such as H-Mold and Corner Key, must be fastened to furring, blocking, or 18 gauge flat stock. Sealant backers must be fastened every 12"-14" vertically, so any use of flat stock must accommodate this fastening schedule.

Outside corners may be wrapped with 18 gauge flat stock fabricated to fit the corner. Attach the stock to furring on both sides of the corner. Corner Clips are used to secure Nichiha factory panel Corners and may be fastened to the flat stock wrapping, as can metal trim corners.

IBC 2015 TABLE 2603.12.2

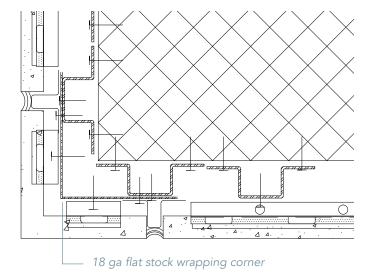
The model building code for 2015 includes information in Chapter 26 about foam plastic insulation/sheathing and furring minimum fastening requirements. Table 2603.12.2 shows various configurations depending upon framing gauge and spacing, fastener size and spacing, thickness of insulation and cladding weight. As an example, according to the table, 3 inches is the maximum thickness of foam sheathing on which a furring can be added directly on top, spaced at 16" o.c. and fastened with #8 screws every 12"-16" (into 18 gauge wall framing), that can support a cladding weight of 3 psf.

ENERGY CODE FRIENDLY MARKET OPTIONS

A number of engineered third party systems exist that are designed to solve the conflicts between energy code compliance and the safe installation of exterior claddings over continuous insulation.

Nichiha has direct experience with these products:

- Bracket and rail systems:
 - Cascadia Clips®
 - FERO Cladding Support
 - ISO Clip
 - Knight Wall MFI®
- CL-TALON®
- Knight Wall CI® and HCI™ Systems
- SMARTci GreenGirts



WEATHER RESISTIVE BARRIERS

A weather resistive barrier (WRB) is required when installing Nichiha panels over stud walls and SIPs. For CMU/concrete assemblies, Nichiha defers to local code requirements. Use an approved WRB as defined by the 2015 IBC. Refer to local building codes.

A permeable WRB is highly recommended when installing Nichiha panels for residential applications.

Permeable WRB is required for all commercial applications. A fluid applied WRB is acceptable.

Sheathings and insulations with an integrated code-compliant WRB such as ZIP System® and DensElement™ are acceptable.

All openings must have appropriate flashing to prevent moisture penetration. Follow manufacturer's guidelines and all local building codes.

STORAGE & HANDLING

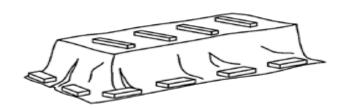
AWP are a finished product and care must be taken to protect them against damage prior to and during installation. Panels must be stored flat and kept dry. Indoor storage is best. Refer to the storage information included on product pallets.

Ensure panels are completely dry before installing. Direct contact between the panels and the ground must be avoided at all times. It is necessary to keep panels clean during the installation process.

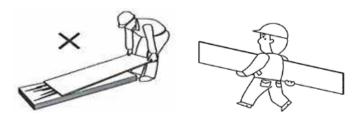
Cut panels face down.

Always clean panels with a clean, soft, dry cloth after cutting. Dust can bind to the finish.

When sidewalks are poured after awp installation, take steps to cover/protect panels near grade. Cement dried on AWP cannot be removed.



Always cover pallets with a tarp or store indoors!



Don't unpackage and re-stack panels! Always carry panels on edge!

FASTENERS

All Applications

Fasteners must be corrosion resistant. Stainless steel or corrosion resistant screws such as hot-dipped zinc or ceramic coated are recommended. Comply with all local building codes for fastener requirements.

Number 10, pan-head screws (HD .365") were used as clip fasteners for AWP wind load testing. The minimum size for clip fasteners is #8. Ultimate Clip and Starter Track screws must have a pan, wafer, or hex type full head.

Min. Number 7 finish screws with a bugle or flat head (min. head diameter 0.255") are appropriate for face fastening locations. These must penetrate framing per the minimum requirements below. Refer to the *Face Fastening Best Practices* section for face fastening procedure.

When installing AWP with the Structural Sheathing Method, ensure clip fasteners are at least 1" in length to fully penetrate the plywood or OSB. Wherever possible when face fasteners are needed, screws must be long enough to penetrate all the way through the sheathing and into the framing.

For the Custom Stud Spacing Method, the fasteners must always penetrate the studs or furring with minimum 1" penetration for wood or 1/2" for metal.





FACE FASTENING BEST PRACTICES

To minimize the appearance of face fasteners, utilize the following steps:

- 1. Apply low adhesive tape such as painters tape to the panel at face fastening locations.
- 2. Pre-drill panels 1" from the cut edge to be face fastened. Use a countersink drill bit with chamfer matching the head diameter of the bugle-head type screws to be used for face fastening.
- 3. Fill counter-sunk fastener holes with exterior cementitious filler, such as MH Ready Patch® and later dab touch-up paint with cotton swabs or artist brush.
- 4. Remove the painter's tape only after applying patch and touch up paint.





INSTALLATION HARDWARE & ACCESSORIES



ULTIMATE VERTICAL STARTER TRACK

Ultimate Vertical Starter Track serves as the foundational support for the AWP system while also providing faster and greater ease of installation. With Vertical AWP3030, the Starter Track carries the entirety of the dead loads and is required for each course.

FA 710 T Vertical Starter Track – 10mm rainscreen



ULTIMATE CLIP II

Ultimate Clips are secured to the vertical panels' shiplaps, securing AWP to the wall while holding their back surface off the substrate to create the 10mm (3/8") rainscreen space. In vertical applications, clips do not support panel weight.

JEL 778 CLIP Compatible with all 3030mm AWP - 10mm rainscreen

Joint Tab Attachments included with Ultimate Clips are not needed for vertical panel installations.



CORRUGATED SPACER

At termination points where Ultimate Clips cannot be used, Nichiha Corrugated Spacer is required to maintain the rainscreen space and prevent panel deflection at face fastening locations such as window jambs and outside corners.

FS 1005 SPACER – 5mm rainscreen

FS 1010 SPACER - 10mm rainscreen



SEALANT BACKERS

Nichiha Sealant Backers provide exact spacing for expansion and termination joints and the recommended depth of sealant (75-80%).

They provide faster installation than a foam backer rod and require less sealant. At sealant joints, use a sealant that complies with ASTM C920, Class 35 (min.). Refer to the Sealant section on page 19 for more information.



Single Flange Sealant Backer: FHK 1015 – 10mm rainscreen

Double Flange Sealant Backer: FH 1015 – 10mm rainscreen



METAL TRIM OPTIONS

Nichiha metal trim provides aesthetically pleasing design options for corners, openings, and transitions.

TRIM	APPLICATIONS
Corner Key	Outside Corners
H-Mold	Vertical Joints
Open Outside Corner	Outside Corners
J-Mold	Terminations
Inside Corner	Inside Corners



ESSENTIAL FLASHING SYSTEM	APPLICATIONS
Starter*	Base/Clearance Concealment
Compression Joint	Horizontal/Compression Joints
Overhang*	Fascia-to-Soffit Transitions

^{*} Inside and outside corner segments are available.



PLANNING AND PANEL LAYOUT

To ensure a successful installation, it is important to first plan how the panels will be laid out, where horizontal/ compression joints will be located for each course, and line of sight regarding inside corners decided.

Reminder: AWP3030 actual dimensions are metric: 455mm (h) x 3,030mm (l). Imperial equivalents: 17-7/8" (h) x 119-5/16" (l).

Horizontal/Compression Joints (Page 25):

1/2" (min.) Horizontal, flashed break detail to allow for building compression at floor lines. *Horizontal joints may not be staggered*.

Inside Corner Line of Sight (Page 20): Sealant joints at inside corners can be placed out of view from the primary line of sight of a wall. Place the sealant joint on the less-viewed corner wall. Alternatively, utilize Inside Corner metal trim.

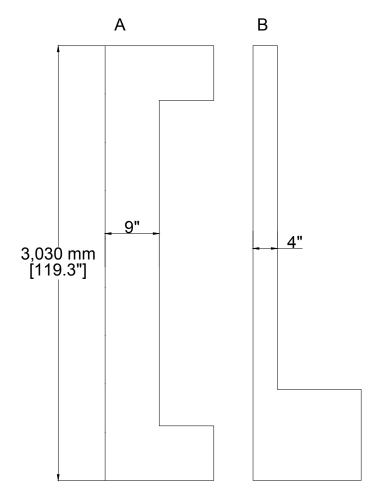
Cut Panels: In general, it is best to avoid cutting AWP to short or narrow strips and segments of less than 9". The hard minimum width or height is 4". Adjust the layout or use alternate materials when needed to avoid cutting AWP smaller than 4".

Specifically, when an individual panel is taller than a window or other opening and is used over the head or under the sill, do not cut it to less than 9" in width along the opening jamb. (see image A)

When an opening is taller than an individual panel and two or more are needed to cap over the header or cup the sill, do not cut the panel to less than 4" in width along the jamb. (see image B)

Design Wind Pressures: Refer to our code approval documents when determining the best vertical panel installation method for a specific project.

The Structural Sheathing Method and Custom Stud Spacing methods result in different allowable design pressures, dependent upon thickness of wood sheathing or type/gauge of custom spaced studs/furring. Refer also to Limitations, Technical Reviews section regarding Nichiha's technical review process.



AWP3030 - VERTICAL: INSTALLING THE FA 710 T VERTICAL STARTER TRACK

All Applications

Without custom stud/furring spacing outlined in the Framing & Sheathing Requirements section, 7/16" or thicker APA rated OSB or plywood sheathing MUST be used to enable vertical installation of AWP3030. Plywood/OSB shall be secured to building framing in compliance with best practices and local building codes. In any case, Vertical Starter Track must be secured to framing and never sheathing alone as it fully carries the weight of the vertical panels. With respect to nail-base insulation sheathings, please contact Nichiha Technical Services for guidance.

Starter Track must remain continuous. Staggering of horizontal joints is not permitted.

MINIMUM CLEARANCES

The Starter must be level and attached at a minimum of 6" above finished soil grade or per local building codes (use a laser level to verify). When installing over a hard surface such as driveways or sidewalks, a 2" clearance is acceptable.

Keep AWP at least 1" above roofs.

Essential Starter Flashing may be installed prior to the Starter Track to conceal the clearance gap above hardscape and decking. Beginning with outside and inside corner segments, fasten trim at each stud location or every 10" o.c. to sill plate. Fasten inside and outside corner segments to framing on both sides of the trim, keeping at least 1" from trim vertical edges. Main segments will slide into/overlap the corner trim. Position Starter Track to leave 1/4" clearance between the panel edge and trim/flashing.



Vertical Starter Track fastened every 6" to 9" to framing.

ALL APPLICATIONS

To fully secure Vertical Starter Track, use corrosion resistant screws of sufficient length to ensure full penetration of the sheathing and into framing by 1" for wood or 1/2" for metal. *Starter must be level*.

WOOD & METAL STUDS

Vertical Starter Track must be secured every 6"-9" into the sill plate or to the studs and, if applicable, halfway between into the wood sheathing.

CONCRETE/MASONRY

When installing over concrete construction, the wall must be furred out with pressure treated lumber, metal hat channel, or z-furring. Install APA rated 7/16" OSB or plywood to furring when the spacing is other than 45.5cm (17-7/8") o.c.. Starter Track must be secured at each furring location and halfway between into the sheathing or blocking at an overall fastener spacing of 6"-9" o.c.

STRUCTURAL INSULATING PANELS (SIP)

Secure Starter Track every 6"-9" o.c. max into the sill/horizontal base framing of the SIP.

NAIL-BASE INSULATION SHEATHING

Contact Nichiha Technical Services for guidance.



GENERAL PANEL & ACCESSORY BASICS

PANEL SELECTION

Nichiha AWP are packaged with two panels in a pack, which are placed on pallets consisting of two stacks. Due to alternating patterns of texture and color between individual panels as well as how the panels are manufactured and packaged, it is best to install all panels from each individual stack before taking and installing panels from the second stack on the same pallet. Do not alternate installing from one stack and the second, which may result in undesirable patterns.



SEALING CUT PANEL EDGES

When cutting AWP, it is best to cut with the panel face down, except when cutting brick finish panels as it is easier to follow the simulated mortar lines.

Cut and exposed panel edges must be primed or sealed with fiber cement sealer (e.g. DryLock®) or paint such as Kilz Premium® or Kilz Max®. Do not use supplied Illumination Touch-Up paint. (Fig. 14)

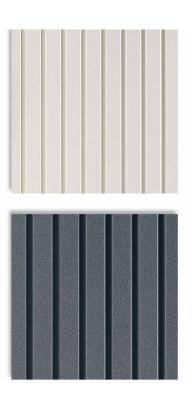
Be sure to clean panels with a dry, soft, clean cloth after cutting to prevent dust from bonding to the finish.

CUTTING ULTIMATE CLIPS

JEL778 Ultimate Clips are 26" long. Where full length clips can be used, they are required. However, there may be conditions where clips must be cut to accommodate panels in smaller areas or segments such as short columns, pilasters, or insets/recesses.

Notches on the upward panel engagement flanges indicate where clips can be cut evenly into thirds. These 1/3 segments can be further reduced evenly into two or four pieces each with weep holes serving as dividing points. The smallest segment must include at least one downward panel engagement flange. Always use the widest clip segment possible. Cut with a non-ferrous saw blade on a band or chop saw.







SEALANT

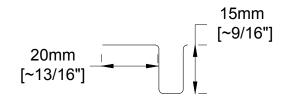
Sealants to be used with AWP must match the following requirements:

- Comply with ASTM C920
- Have a Class of 35, 50, or 100/50 (minimum 35% joint movement)
- Be a polyurethane, polyurethane hybrid, or Adfast Adseal 4580
- Provide two-sided adhesion at joints

OSI® QUAD® may not be used for Nichiha expansion joints:

- It is a class 25 product.
- QUAD® MAX is acceptable since it is a Class 50.

Refer to the Technical Bulletin: *Sealants* available at *nichiha.com/resource-center*.



Single Flange Sealant Backer (FHK1015R) (Galvalume)

SEALANT JOINTS/CAULKING

Fasten Single Flange Sealant Backers at inside corners (one wall at corner), along window and door jambs, and transition points with other cladding. Fasten to framing, blocking or plywood/OSB sheathing at 12"-14" o.c. with the 3/8" bump/ sealant portion butting the corner or jamb.

Sealant complying with ASTM C920, Class 35 (min.) is required where Single and/or Double Flange Sealant Backer is used.

Refer to the sealant manufacturer's instructions or requirements.

Place low-adhesive tape (masking or painter's) over the panel along the areas requiring sealant joints for a clean caulk line. Fill the gap between the panels with a color-matched/coordinating ASTM C920, Class 35 (min.) sealant. The Nichiha Sealant Backer allows for the proper depth of sealant (75-80%).

Before removing tape, press the surface of the sealant with a caulk spatula or similar tool to ensure an even surface.

Remove masking tape before sealant cures.

If excess sealant adheres to panel, remove completely using a putty knife or soft cloth.

AWP3030 - VERTICAL INSTALLATION

Without custom stud/furring spacing outlined in Framing & Sheathing Requirements section, 7/16" or thicker APA rated OSB or plywood sheathing MUST be used to enable vertical installation of AWP3030. Wall surfaces must be flat.

Use corrosion resistant screws of sufficient length to ensure full penetration of wood sheathing (Structural Sheathing Method), or the 17-7/8" o.c. studs with the Custom Stud/Furring Spacing Method (minimum penetration 1" into wood, 1/2" into metal), to secure Ultimate Clips. Face fasteners must be at least 1-1/2" in length.

Single Flange Sealant Backer and metal trim should be installed before panels. Refer to Inside Corners, Windows & Doors and Outside Corners sections.

AWP installation proceeds by working from left to right.

If starting at an inside corner, predetermine which wall will include the Single Flange Sealant Backer. Consider the location to minimize the visibility of the sealant line. Clad the higher visibility wall without the sealant joint first so that the adjoining wall panels can terminate to it with the Single Flange Sealant Backer detail. Or utilize Inside Corner metal trim.

Prior to installing the first vertical panel, add 10mm corrugated Spacer at the left edge of the wall at the starting point. The Spacer should extend upwards to where the panel will end.

Looking at an AWP3030 oriented horizontally, remove the bottom ship-lapped edge and then rotate the panel 90 degrees clockwise to set the short panel edge on the FA 710T Vertical Starter Track. The freshly cut and sealed edge should butt to the corner/starting point and will cover the 10mm Spacer. Be sure to clean dust from cut panels with a dry, soft cloth or HEPA vacuum.

Pre-drill panels after applying low-adhesive tape to be removed after patching/touch-up. Fasten every 12"-16" o.c., spaced vertically, with a minimum 1" distance from the edge (Fig. 19a).

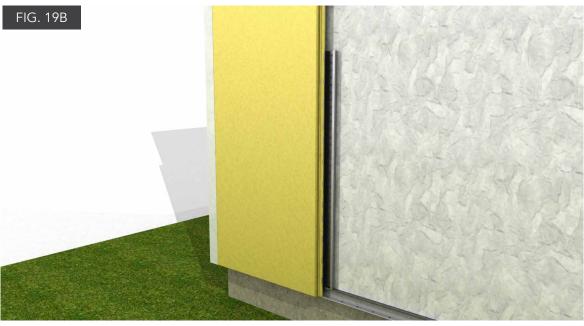
Fill counter-sunk fastener holes with exterior cementitious filler, such as MH Ready Patch® and later dab touch-up paint with cotton swabs. Remove painter's tape.

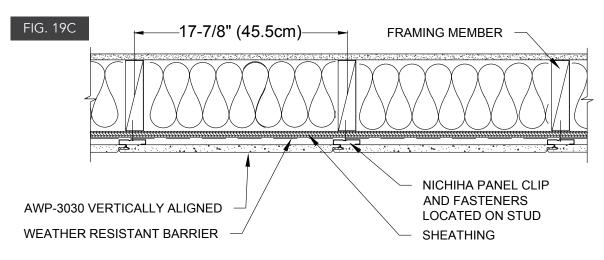
Whenever possible, use face fastening screws long enough to penetrate all the way through the sheathing and into the framing by 1/2" for metal, 1" into wood. Refer to the Touch-up Paint, Minor Repairs sections for more info on patching face fasteners.

On the right, factory edge, add four Ultimate Clips evenly spaced along the full AWP3030 panel, with the first at the Starter Track edge. Add four fasteners per clip, evenly spaced (Fig. 19b). In the Structural Sheathing Method, the clips will be fastened only to the plywood/osb sheathing. With the Custom Stud Spacing, the clips will align with vertical framing and the fasteners will be secured to the studs or furring (Fig. 19c).

Working from left to right, install the next panel with its ship-lapped edges intact. A rubber mallet or block may be used to seat panels firmly in place and tighten together on vertical panel joints. Do not hammer directly on the panels as direct contact may cause cracks, gouges, or chipping. Install four Ultimate Clips as with the first panel, each with four screws. (Continued p. 20)







Continue likewise until reaching a termination or transition point. The factory edge must be removed from the last panel, and this cut edge must be face fastened over 10mm Spacer. Space the fasteners every 12"-16" o.c. vertically, with a minimum 1" distance from the edge. Again, whenever possible, use face fastening screws long enough to penetrate all the way through the sheathing and into the framing, 1/2" into metal, 1" into wood. Refer to *Face Fastening Best Practices* for info on patching face fasteners.

To begin a second course of panels, install appropriate horizontal joint flashing or Essential Compression Joint Flashing above the top edge of the bottom/first course of panels. Then repeat the steps beginning with FA 710 T Vertical Starter Track a minimum 1/2" above the top edge of the first course of panels (See Horizontal/Compression Joint section). Horizontal joints may not be staggered.

INSIDE CORNERS, WINDOWS & DOORS All Applications

Appropriate flashing should be used to prevent moisture penetration on all inside corners, doors, and windows. Refer to local building codes for best practices.

Cut and exposed panel edges must be coated with exterior acrylic latex paint.

INSIDE CORNERS

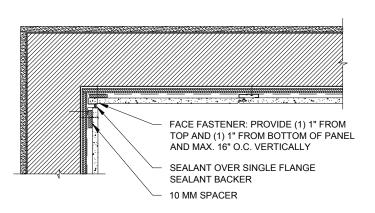
Single Flange Sealant Backer (FHK 1015):

Decide primary line of sight in order to minimize visibility of the sealant joint.

Install the panel on the front wall (more visible) first. Ensure panel is butted up tight to the inside corner wall. Fasten the Single Flange Sealant Backer onto the side wall right up against the front wall panel's edge at 12"-14" o.c. to framing, plywood/osb sheathing, or blocking.

Add 10mm Spacer over the fastening flange of the Sealant Backer.

Install side wall panel, with factory edge removed and sealed, directly against the sealant backer, over the Spacer, and secure with face fasteners*. Fill space with ASTM C920, Class 35 (min.) sealant.



Inside Corner Metal Trim: Install Nichiha Inside Corner metal trim directly against the inside corner sheathing. Fasten metal trim every 12"-16" in a staggered fashion on alternating flanges.

Remove the shiplapped edges that will be inserted into the trim, treating the cuts, and install panels normally, butting to the Inside Corner trim in moderate contact.

Trim Boards: Install trim boards at inside corner first and then add Single Flange Sealant Backer. Add ASTM C920, Class 35 (min.) compliant sealant to the gap.

*Face fasteners should fully penetrate OSB or plywood sheathing and into the framing whenever possible. Refer to Face Fastening Best Practices for info on patching face fasteners.

WINDOWS AND DOORS

Window Sills (J-Mold optional): For recessed windows, add a flashing where the panels will terminate so that the top edge is covered or capped.

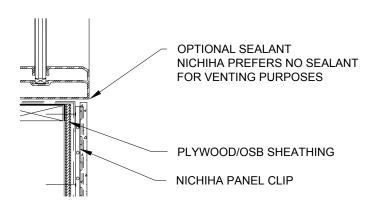
As needed, cut the panel to the required height to fit below the window sill, leaving a 1/4" gap between the top of the cut panel edge and the window sill or trim board.

Cut panel edges must be sealed with 100% acrylic latex exterior primer or paint, such as Kilz Premium or Kilz Max. Clean any dust off the panels with a dry, soft clean cloth.

Fasten Ultimate Clips along the sides of the panel to sheathing, framing, or furring with a clip positioned within an inch of the top end of the panel meeting the sill and the lowest clip at Vertical Starter Track edge.

If the top edge of the panel is fully sheltered under the sill, it is not necessary to seal the 1/4" gap. For better system performance, Nichiha recommends the vented approach.

If desired, install J-Mold trim, fastened every 12"-16", under the sill prior to panels.



WINDOW/DOOR JAMBS

A minimum gap of 1/4" is required when butting panels into windows, doors, and trim boards. Refer to window/door manufacturer guidelines for spacing trims around windows.

Single Flange Sealant Backer: Install the Single Flange Sealant Backer first, butting to the door/window jamb or trim pieces prior to installing the panels.

The Single Flange Sealant Backer must be fastened a minimum of 12" to 14" o.c. to framing, plywood/osb sheathing, or blocking.

Add 10mm Corrugated Spacer along the jamb.

Remove appropriate ship-lapped edge of panel, clean off dust with soft, dry cloth, and treat cut edge.

Install panels, face fastening through Spacer along the jamb edge every 12"-16", keeping a minimum 1" from panel edge. Use face fasteners long enough to penetrate framing.

Fill gap with recommended sealant.

J-Mold: Pre-install J-Mold trim, fastening every 12"-16", with a 1/4" gap between it and the jamb or per window/door manufacturer instructions

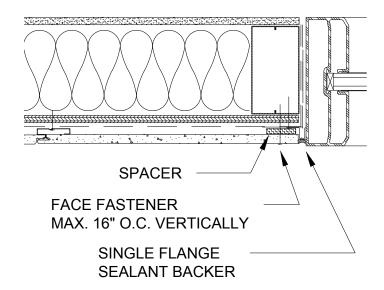
After installing the next-to-last panel, measure from the edge of the face of this panel to the J-Mold edge (the 90 degree angle edge). From this measurement, subtract 1/4" and cut the last panel to this width. Paint or prime cut edges and clean off dust from panel.

Install 10mm Corrugated Spacer next to the metal trim.

Install panels by inserting the cut edge into the metal channel and then shifting the panel over onto the side Ultimate Clips along the adjacent panel, fitting ship-lapped edges together.

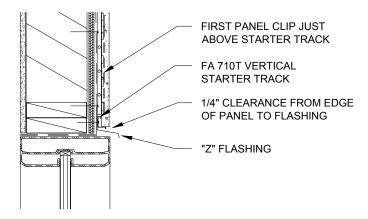
Face fasten through Spacer along the jamb edge every 12"-16". Use face fasteners long enough to penetrate framing.

Lastly, add foam backer rod and sealant to the 1/4" gap, if applicable, between the J-Mold and jamb.



WINDOW/DOOR HEADERS

Starter Track: When starting a course of vertical panels above a window or door, add flashing and FA 710 T Vertical Starter Track at the header, installed with fasteners every 6"-9" into the opening header.



OUTSIDE CORNERS

There are two primary outside corner installation options for vertical AWP3030:

Trim Boards: Fiber Cement, Wood, or PVC

Metal (Open Outside, Corner Key) or Vinyl Trim Channels.

Appropriate flashing must be used as required to prevent moisture penetration at outside corners.

FIBER CEMENT & PVC TRIM BOARDS

Nichiha manufactures a full line of fiber cement trim boards - NichiTrim[™], which are available in the Southeast U.S. Refer to Nichiha.com for more information.

When panels are to be butted to fiber cement, wood or other trim pieces, use Nichiha Single Flange Sealant Backer.

Add 10mm Spacer, remove the appropriate panel shiplap, and face fasten panel edge every 12"-16", vertically, keeping 1" from edge. Apply sealant to joint width. Sealant must be compliant with ASTM C920, Class 35 (min).

METAL & VINYL TRIM

(including Nichiha Corner Key and Open Outside Corner trim)

When installing Nichiha AWP3030 in a vertical orientation, pre-fasten corner trim channels, securing trim to framing every 12"-16", alternating/staggering the fasteners on both flanges.

At the starting point, such as an outside corner, remove the panel edge, add 10mm Spacer to the wall at the corner. Set the panel on the Starter and into the corner trim channel, and then face fasten the panel as described at the beginning of the AWP3030 Vertical Panel Installation section.

Working from left to right, when reaching the next outside corner, follow the steps for the appropriate trim profile:

Corner Key: After installing the next-to-last panel, measure from the edge of the face of this panel to the Corner Key edge (the 90 degree corner angle edge). From this measurement, subtract 1-3/8" and cut the panel to this width. Paint or prime cut edges and clean off dust from panel. (Fig. 24a)

Open Outside Corner: After installing the next-to-last panel, measure from the edge of the face of this panel to the Open Outside Corner edge (the 90 degree angle edge). From this measurement, subtract 1/4" and cut the panel to this width. Paint

or prime cut edges and clean off dust from panel.

Install 10mm Spacer next to the metal trim. Install panels by inserting the cut edge into the metal channel, rotating into the wall plane, and then shifting the panel over onto the side clips along the adjacent panel, fitting ship-lapped edges together.

Face fasten panels through Spacer along the corner edge every 12"-16" (Fig. 24b). Use face fasteners long enough to penetrate framing.

Fit panels into channel trim so that panel edges are not exposed.

Nichiha metal trim pieces are each 10' in length. To cut metal trim, use a non-ferrous carbide miter saw blade. When butting/stacking metal trim pieces, add a bead of polyurethane sealant at the seam/joint.

Metal trim can be pre-finished when purchased to match Nichiha Color Xpressions color(s). Otherwise, for field painting primed metal trim refer to Tamlyn's XtremeTrim Painting Guide.





NON-90 DEGREE CORNERS

Corners other than 90 degrees can be achieved with custom metal trim, butting panels to trim board with a minimum 1/4" sealant gap, or with the use of Double Flange Sealant Backer to set cut panel edges at the desired corner angle. Please contact Nichiha Technical.

VERTICAL CONTROL/EXPANSION JOINTS All Applications

Because thermal expansion occurs in the long (3030mm) dimension of the panels, Vertical Control/ Expansion Joints are not required for vertical installations of AWP3030.

HORIZONTAL/COMPRESSION JOINTS

All Applications

The module of Vertical AWP3030 necessitates a continuous Horizontal/Compression Joint every 119-5/16" (repeating after each course).

Do not stagger horizontal joints.

Do not span floor lines with panels.

INSTALLING A HORIZONTAL COMPRESSION JOINT

Install Essential Compression Joint Flashing or heavy
gauge z-shaped metal flashing or
drip cap over the top edge of the
course of panels terminating under the
Horizontal Compression Joint location.
Fasten Essential Flashing at each stud

location.

Install Vertical Starter Track over the flashing and check for level. Place Vertical Starter at least 1/2" above the course below and 1/4" above flashing/ trim. A best practice is to add flashing tape to cover the fasteners of the flashing, sealing it to the WRB.

Continue to install panels according to these guidelines with compression joints every 119-5/16" (max).



LARGE OPENINGS

All Applications

Install Vertical Starter Track at the wall base in keeping with standard instructions on both sides of the opening.

Install Vertical Starter Track at the head of the opening, either the width of the opening or all the way across the wall.

Add panels per the standard procedure as in a typical *Window or Door Opening* for the jamb conditions.

Do not span floor lines with panels. Plan for a *Horizontal/Compression Joint* at the head of the opening or above, at the same level where the panels along the sides of the opening terminate, assuming the garage or other large opening is shorter than full length panels.

Horizontal/Compression joint detail Starter Track 1" above garage door casing Starter Track 2-6" above grade

PENETRATIONS, RAILINGS, AND SIGNAGE

Openings for small penetrations for pipes or conduits may be cut through a panel with the hole sealed with ASTM C920 compliant sealant. For larger penetrations greater than 1-1/2", it is best to block or frame out the opening. Treat the penetration like a small window.

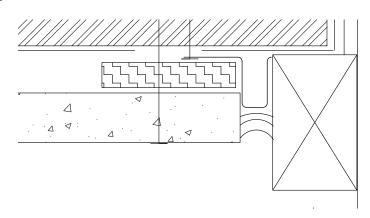
Along the jambs of the opening install Single Flange Sealant Backer. Cut panel edge as needed to butt to Sealant Backer and add recommended sealant.

Underneath the opening block out, terminate panel with 1/4" gap. Sealant here is optional, depending on the depth of the blocking.

Above the penetration, add flashing and install FS1010 Spacer as needed for face fastening panel edge at framing locations. Ensure minimum 1/4" gap between bottom of panel edge and penetration blocking.

Keep any face fasteners 1" away from panel edges.

If installing railings or signage over AWP, ensure fasteners are secured through to framing or other structural support. Do not fasten any attachments solely to panels. Add a small spacer (up to 10mm) between the signage and AWP to prevent moisture pooling on top of the attachment and seeping between it and the AWP, becoming trapped.

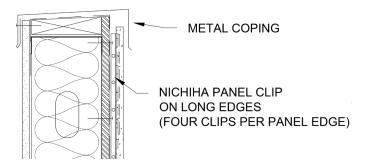


LAST COURSE

All Applications

Cut panels (horizontally) to properly fit at the roof line under soffit or parapet cap (or at the proper transition point). Ensure Ultimate Clips along factory edges are secured no more than 1"-2" from the top of the panels.

Cover top panel row edge with roof cap/coping, where applicable.



GABLE & OVERHANG

Allow a minimum of 1" clearance (as per local building codes) above the roof line.

At the top, cut the panel to follow the slope of the gable or overhang.

When installing soffit, the wall panels should be installed first, with the soffit installed over the panels.

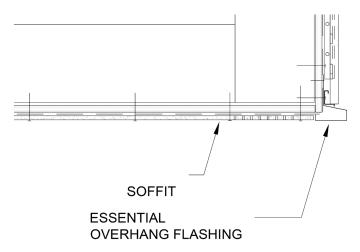
Seal all cut panel edges with 100% acrylic primer or paint. Do not leave any panel edges exposed.

Essential Overhang Flashing may be used at the base of overhangs/bump-outs or porte-cocheres.

Prior to panel installation, fasten Overhang Flashing at each stud location, beginning with corner segments. Main segments will slide under/overlap corner segments.

Use Joint Clip segments to join main segments together. After first piece is secured, add a Joint Clip, fastening through both it and the first main segment. The next main segment will slide behind the Joint Clip.

Position Overhang so that its bottom/return flange butts to or overlaps soffit. The bottom return portion must extend beyond the face of the fascia substrate.



Essential Overhang Flashing & Joint Clip



TRANSITIONS WITH HORIZONTAL AWP

On projects also utilizing horizontally-installed AWP, expansion and compression type joints will be required as there is no way to naturally joint horizontal and vertical AWP directly.

VERTICAL JOINTS

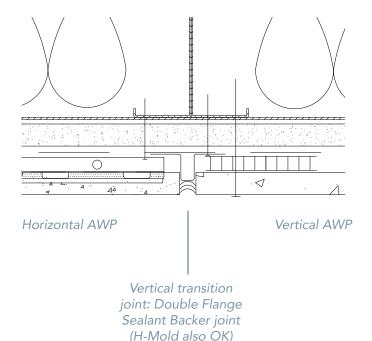
A Double Flange Sealant Backer or H-Mold trim is necessary at vertical joints/transitions between horizontally oriented panels and vertically oriented ones.

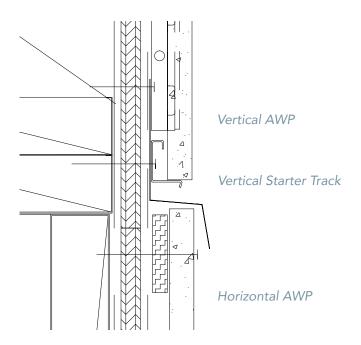
HORIZONTAL JOINTS

A horizontal/compression joint style detail is necessary to transition between horizontal and vertical AWP. Please refer to *Horizontal/Compression Joints* on page 25.

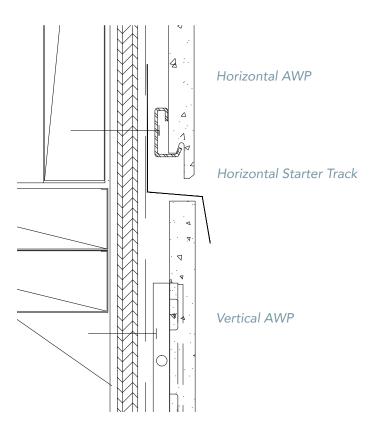
Horizontal panel to Vertical panel Transitions
Face fasten the top, cut edge of the horizontal AWP,
cap it with Essential Compression Joint Flashing
or Z-flashing. To then install vertical AWP, add
the Vertical Starter Track following the standard
procedure and fastening requirements.

Vertical panel to Horizontal panel Transitions
Install vertical panels to the desired transition level
and cap with Essential Compress Joint Flashing or
Z-flashing. Install the Horizontal Starter Track 1-1/4"
above the flashing, following the standard procedure
and fastening requirements. Refer to the Horizontal
Installation Guide AWP1818, AWP3030.





Horizontal transition joint: Compression Joint details



CLEANING & MAINTENANCE

CLEANING PANELS

After completion of the installation or for periodic maintenance, it may be necessary to clean panels.

When cleaning panels, use no more than 400 psi of water pressure at 10" to 12" away. Do not pressure wash custom color panels.

To clean heavily soiled areas, a mild household detergent and/or soft bristle brush may be required.

Do not allow any detergent/cleaner to dry on panels. Rinse immediately after cleaning.

PAINT TOUCH-UP

Touch up paint must be exterior grade 100% acrylic latex and can be color matched by taking a panel sample to your local paint or home improvement store.

A small amount of touch-up paint is supplied with your custom color panel order. Do not use touch-up paint for edge treatment/sealing due to the limited quantity provided.

Utilize low-adhesive tape to isolate patching and touchup locations such as face fastened areas. Where face fasteners have been used and patched by cementitious filler, use a cotton swab to lightly dab touch-up paint.

For scratches, use a cotton swab for small ones or 1" foam brush for longer ones, again using a dabbing motion rather than brushing in order to minimize the amount of paint applied.

REMOVAL OF EXTERIOR ACRYLIC LATEX PAINT

Wet Paint Removal - While the paint is still wet, flush the area with clean water, using mild abrasion with a clean cloth or soft brush.

Semi-Dry Paint Removal - If paint has set, but not dried, flush and clean as above, followed by light scrubbing with alcohol to remove any remaining paint residue. Rinse with water and a clean cloth.

Dry Paint Removal - Please refer to paint-removal guide in the next section.

OTHER PAINT & GRAFFITI REMOVAL

The following products have been tested on Nichiha panels to aid in the removal of graffiti type markings.* These citrus-based products can also be used for basic panel cleaning purposes. The panels were sprayed with an indoor/outdoor aerosol spray paint and left to dry overnight, and then the paint removal products were applied following the manufacturer's guidelines.

All products tested achieved good results. However, the outcome may vary depending on the amount of paint that needs to be removed. Be sure to follow all manufacturer's guidelines and first test in an inconspicuous area before working on a larger area.

Do NOT use these cleaners with custom color panels. *Nichiha is not liable for any damage caused by the use of these cleaners.

CITRISTRIP

www.citristrip.com

Products tested:

Citristrip Stripping Gel - One Quart container Citristrip Stripping Aerosol - 18 oz. spray can

GOOF OFF GRAFFITI REMOVER

www.goof-off.com

Products tested:

Goof Off Aerosol - 16 oz. spray can Goof Off - 22 oz. trigger spray bottle

TAGAWAY

www.tagaway.com

Product tested:

Tagaway - 32 oz. trigger spray bottle

REPAIRING MINOR DAMAGE

Isolate the blemish with a low adhesive tape such as painters tape. This will help protect the surrounding area of the panel and aide in creating a more polished, clean repair.

Lightly brush/abrade the surface within the taped off area in order to remove any loose material.

Carefully fill and smooth the resultant prepped area with cementitious patching material such as MH Ready Patch. Allow to dry/cure fully.

Gently smooth the patch and then apply touch-up paint to the affected area. Allow touch-up paint to dry and remove the tape.

PANEL REPLACEMENT

Set the depth of the circular saw blade slightly deeper than the panel so the saw blade does not cut into the building wrap or sheathing.

Make cuts into the damaged panel and break into pieces for easier removal.

Remove damaged panel.

If necessary, cut new panel to appropriate height.

Looking at the panel oriented horizontally, cut the top ship-lapped edge off the panel (*Figure 33a*).

Clean off dust and seal the cut edge.

Add 10mm Spacer along the right side of the uncovered wall surface. (*Figure 33b*)

Set the new panel in place on the Vertical Starter Track with the intact factory edge fitting on the exposed clips on the left side of the uncovered space.

Pre-drill and face fasten the right edge of panel through the Spacer with a screw every 12"-16" into framing, furring, or blocking (*Figure 33c*). When only wood sheathing is available for the face fasteners, reduce the screw spacing to 6"-8" o.c.

Fill countersunk screw heads per *Paint Touch Up* and *Minor Repairs*.

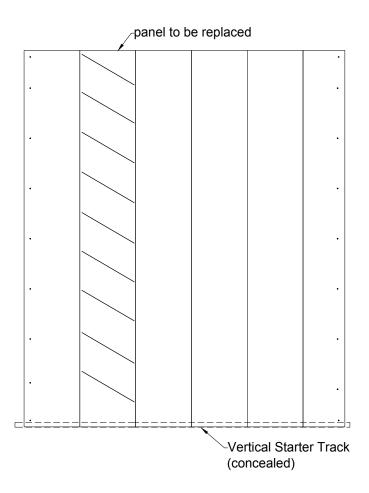
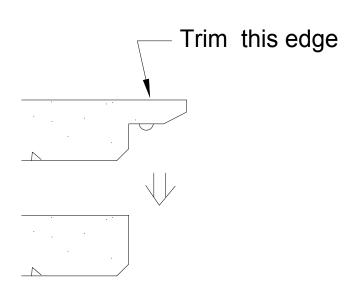


FIG. 33A



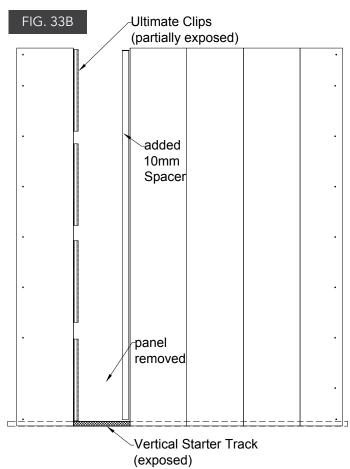
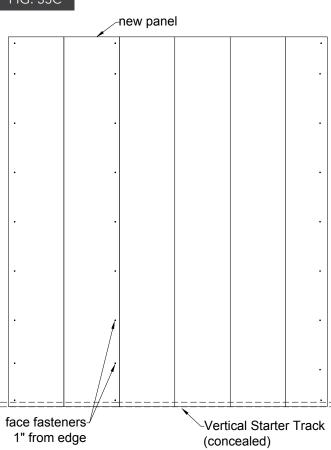


FIG. 33C



Behind our Architectural Wall Panels is SOME SERIOUS TECHNOLOGY.



EASY INSTALLATION

Time-saving Clip Installation
System that reduces construction
time and minimizes mistakes.



NO MORTAR, NO MESS

Pre-finished panels that eliminate the need for messy mortar or costly masonry-skilled labor.



ANY WEATHER PRODUCT

Products that can be installed year round in any climate across the country. No geographical restrictions means more possibilities.



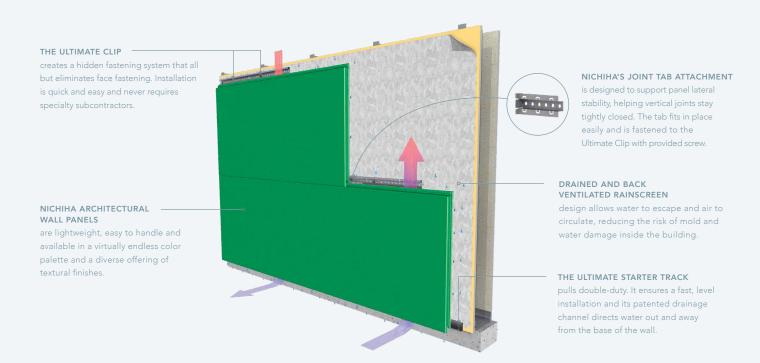
LOW MAINTENANCE

No-fuss products. Little ongoing cleaning or regular maintenance needed. You get to bring your vision to life and ensure it looks great for a long time.



ENGINEERED FOR PERFORMANCE

Go beyond our durable panels and discover a meticulously engineered moisture management system that provides a vertical drainage point for air and moisture to exit.



Never underestimate the power of REALLY GOOD TOOLS.

Whether you are an architect, a builder or a contractor, Nichiha wants to ensure that you have all the information you need to make your project go as smoothly as possible. The way we see it, we are partners. Our website offers a comprehensive collection of technical information, installation videos, Architectural details, in-depth specifications and everything you'll ever need to know about installing Nichiha products.



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- ILLUMINATION SERIES PANELS
 15-year limited warranty* on panels,
 15-year limited warranty* on finish.
- ARCHITECTURAL WALL PANELS
 (Brick, Block, Stone, Wood, Kurastone)
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 15-year limited warranty* on finish.
- METAL TRIM
 Tamlyn warrants defective-free products for a period of 10 years for the original purchaser. Please visit tamlyn.com for detailed information on terms, conditions and limitations.

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CERTIFICATION & TESTING







Code Compliance CCRR-0299

Florida Approval 12875









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March 12, 2020

Steve Kelly, Project Coordinator Clackamas County Community Development 2051 Kaen Road, Suite 245 Oregon City, Oregon 97045

Via email: stevekel@clackamas.us

Regarding: Traffic Impact Analysis Letter

Sandy Health Clinic 39831 Highway 26 Sandy, Oregon 97055 PBS Project 71524.000

Dear Mr. Kelley:

This document represents a traffic impact analysis (TIA) letter to meet the submittal requirements of the City of Sandy (City) and the Oregon Department of Transportation (ODOT). The TIA letter was scoped based on consultation with the City, ODOT, and Clackamas County.

PROJECT DESCRIPTION

The Clackamas County Health Department proposes to consolidate its health services from two offices in Sandy, Oregon, to one location. The existing offices are Sandy Health Clinic located at Sandy High School, 37400 Bell Street, and Clackamas County Health Center, located downtown at 38872 Proctor Boulevard. The proposed site has an existing 6,300-square-foot building used as a warehouse that will be replaced with a 9,600-square-foot health clinic. See Figure 1 for a vicinity map.

The site is within the city under its jurisdiction at the northeast corner of the Highway 26/Ten Eyck Road intersection, and the site will send all of its trips through the Highway 26/Ten Eyck Road intersection. See Figure 2 for the site plan. ODOT recommended a TIA be prepared to determine if a right-turn lane is warranted on westbound Highway 26 at Ten Eyck Road. The intersection of Highway 26 and Ten Eyck Road is under ODOT authority, and Ten Eyck Road is under Clackamas County jurisdiction. After contacting each of the three public agencies and holding discussions with Ankrom Moisan Architects, Inc., the TIA was focused toward two intersections: Highway 26 and Ten Eyck Road, related to the need for a westbound right-turn lane, and Pleasant Street and Ten Eyck Road, related to queueing on southbound Ten Eyck Road.

ODOT recommended that, as a condition of approval, a TIA be prepared to determine if a right-turn lane is warranted for westbound Highway 26 at Ten Eyck Road. If a right-turn lane is not warranted, ODOT recommended that the sidewalk along the site frontage of Highway 26 be extended into the roadway in such a way as to eliminate the existing slip lane and define the bicycle lane through the intersection. Figure 3 shows the existing lane configuration of the intersections in the vicinity of the project.

City staff directed PBS to include an evaluation of queueing on Ten Eyck Road to verify it will not block access to Pleasant Street.

TRAFFIC VOLUMES

PBS contracted with All Traffic Data to collect AM and PM peak hour traffic counts for the adjacent streets at Ten Eyck Road/Highway 26, Ten Eyck Road/Pleasant Street (east leg), and Ten Eyck Road/Pleasant Street (west leg). The traffic data were collected on February 19, 2020. Detailed traffic volume reports are provided in Appendix A

Background Growth

Background growth is a generic increase in traffic volumes that either is not attributable to specific developments in process (in process) or is attributable to influences outside the study area. No in process projects contributed trips to the studied intersections. A linear background growth rate of 2.0% per year was applied to 2020 peak hour volumes between public roadways at the studied intersections. The 2.0% growth rate was based on evaluation of ODOT count volumes on Highway 26 through traffic east and west of Ten Eyck Road between 2013 and 2018. The background growth volumes are included in the 2022 build-out year and the 2029 forecast year traffic volumes. Details of the background growth rate estimate are in Appendix A

Seasonal Adjustment Factor

A 28% seasonal adjustment factor (SAF) was applied to the through movements on Highway 26 based on the ODOT *Analysis Procedure Manual*, Version 2 (APMv2). Since no ODOT automatic traffic recorders (ATRs) are located within the study area, and no ATRs offer similar characteristics or reasonable adjustments, the seasonal trend table method was used. The 28% SAF was calculated based on the average of the commuter and summer trends, adjusting from the mid-February counts to the seasonal peak period. Figure 5 presents the 30th highest-volume hour, including the SAF. Details of the seasonal adjustment factor estimate are in Appendix A

Baseline Volumes

The 2020, 2022, and 2029 baseline volumes represent the study area traffic volumes without the Sandy Health Clinic project development trips. The baseline volumes are calculated as the sum of existing traffic, background growth, and season factors. The 2029 forecast year is used to compare to the City of Sandy's Transportation System Plan (TSP).

TRIP GENERATION AND DISTRIBUTION

The following section relies on data provided in the Institute of Transportation Engineers' (ITE) *Trip Generation Manual*, 10th Edition (2017). Detailed trip generation calculations are provided in Appendix B.

Trip Generation

The proposed Sandy Health Clinic will utilize a site with an existing building. The net new trips to the site are based on the replacement of a 6,300-square-foot building used for food distribution and warehouse space with a 9,600-square-foot health clinic. Figure 2 provides a site plan for the proposed site. Trip generation for both the existing warehouse and the proposed health clinic are based on an independent variable of 1,000 square feet in the respective buildings. The trip generation estimates were calculated using the ITE weighted average trip rates for the peak hours of the adjacent streets. Table 1 summarizes the trip generation calculations.

¹ Noting that Highway 26 is a primary route connecting between the Portland metro area and the Mount Hood winter recreation areas, the recreational summer-winter seasonal trend was also evaluated. Averaging the commuter and recreational summer-winter trends, while not an approved blend per ODOT APMv2, also yields a 28% SAF.

Table 1. Trip Generation

ITE Land Use:	Existing W Code		Propose Code	ed Clinic e 630		
Independent Variable:	1,000 squ	uare feet	1,000 sq	uare feet	Net Ne	w Trips
Size:	6	3	9.	.6		
Weekday ADT:	1	1	36	56	3!	55
Total Peak Hour Trips:	AM	PM	AM	PM	AM	PM
In:	1	0	27	9	26	9
Out:	0	1	8	22	8	21
Total:	1	1	35	31	34	30

Findings: The proposed Sandy Health Clinic project will generate 355 net new trips on an average weekday, 34 net new trips in the AM peak hour of the adjacent streets, and 30 net new trips in the PM peak hour of the adjacent streets

Proposed Trip Distribution

The proposed distribution of new trips is based on a review of the land uses within the study area, consultation with Clackamas County health clinic staff, and on engineering judgment. See Appendix B for correspondence on the trip distribution of the existing Sandy Health Clinic. All trips from northwest, southwest, and west of the site intersect Highway 26, and approach from the west of the site on Highway 26. All traffic southeast, northeast, and east of the site will approach the site from the east on Highway 26. The overall distribution pattern is proposed as follows:

- 90% to and from the site via Highway 26 from the west
- 10% to and from the site via Highway 26 from the east

The distribution pattern above represents an external distribution of the net new trips entering and exiting the study area. The distribution and assignment of the project's net new trips are shown on Figure 4.

INTERSECTION OPERATIONS AND ROADWAY CAPACITY ANALYSES

Operation Standards

The City of Sandy Minimum Requirements for Traffic Analysis cites a minimum level of service (LOS) D for signalized intersections and for stop conditions. The LOS is based on the volume-to-capacity ratio (v/c) for signalized intersections when the development is in full service. ODOT has a mobility standard of a v/c ratio 0.85 for highways categorized as Freight Route on a statewide highway for locations inside an urban growth boundary and a posted speed equal to or under 35 miles per hour (mph).

Analysis Methodology

Traffic impacts were estimated to determine the extent of change in traffic conditions caused by future development. In order to make this determination, the following assumptions were employed:

- The individual peak hour volumes were analyzed for 2020 existing year, 2022 assumed full operation, and 2029 forecast year.
- The analysis is based on the AM and PM peak hour of the adjacent streets.
- No in-process trips were included in the analysis.

- An SAF of 28% increase was applied to the through movement volumes on Highway 26 based on the ODOT APMv2 Seasonal Trend Table method.
- The peak hour factor (PHF) for the overall intersection, as calculated from the count data, was applied for each analysis scenario.
- A minimum value of 2.0% was assumed for each movement in the future conditions for heavy vehicle percentage (HV%).
- As noted previously, trip generation, distribution, and assignment estimates for the project were prepared for the weekday AM and PM peak hours on the surrounding street system.
- Cumulative traffic impacts of the proposed project were determined by superimposing the project-generated traffic onto the baseline volumes for the weekday AM and PM peak hour at studied intersections. This sum is termed the "With Project" conditions.
- The LOS for the signalized intersection was calculated with Trafficware's Synchro software, Version 10, based on *Highway Capacity Manual* (HCM) 6th Edition (2016) methodologies. The ODOT protocol for Synchro analysis at signalized intersections was used to calculate the intersection v/c ratio.
 - o Signalized intersection results are reported as the v/c ratio for the intersection.
 - ODOT right-turn lane warrants at a signalized intersection are based on volume threshold and LOS standards per ODOT APMv2.
 - o Traffic signal timing values were supplied by ODOT and used throughout the LOS analysis without modification.
 - The analysis includes a 2029 With Project alternative with a right-turn lane for westbound Highway 26.
- No site driveways were analyzed for this report.
- The queueing was estimated for 2029 conditions with and without the project using SimTraffic following ODOT APMv2.
- Right-turn lane impacts on bicycle safety are based on bicycle level of traffic stress (LTS) methodology, noted in APMv2.
- The results of the TIA were compared to the City's TSP related to the Highway 26/Ten Eyck Road improvements.

Level of Service Analyses

Table 2 presents the LOS analysis for the Highway 26/Ten Eyck Road intersection for 2020 existing conditions during the studied peak hours. Detailed LOS calculation reports are provided in Appendix C.

Table 2. Estimated Level of Service at Study Area Intersection for 2020 Existing Conditions

		AM Peak	Hour		PM Peak	Hour
INTERSECTION	LOS	Delay (sec/veh)	Intersection v/c Ratio	LOS	Delay (sec/veh)	Intersection v/c Ratio
Highway 26/Ten Eyck Road	Α	9.1	0.56	С	20.8	0.67

Finding: The existing Highway 26/Ten Eyck Road intersection operates above LOS standards.

Table 3 presents the LOS analysis for the Highway 26/Ten Eyck Road intersection for 2022 without the project during the studied peak hours. Detailed LOS calculation reports are provided in Appendix C.

Table 3. Estimated Level of Service at Study Area Intersection for 2022 Without Project Conditions

		AM Peak	Hour		PM Peak	Hour
INTERSECTION	LOS	Delay (sec/veh)	Intersection v/c Ratio	LOS	Delay (sec/veh)	Intersection v/c Ratio
Highway 26/Ten Eyck Road	Α	9.5	0.58	С	21.4	0.70

Finding: In 2022 without the project, the Highway 26/Ten Eyck Road intersection will operate above LOS standards.

Table 4 presents the LOS analysis for the Highway 26/Ten Eyck Road intersection for 2022 with the project during the studied peak hours. Detailed LOS calculation reports are provided in Appendix C.

Table 4. Estimated Level of Service at Study Area Intersection for 2022 With Project Conditions

		AM Peak	Hour		PM Peak	Hour
INTERSECTION	LOS	Delay (sec/veh)	Intersection v/c Ratio	LOS	Delay (sec/veh)	Intersection v/c Ratio
Highway 26/Ten Eyck Road	В	10.2	0.59	С	21.8	0.72

Finding: In 2022 with the project, the Highway 26/Ten Eyck Road intersection will operate above LOS standards.

Table 5 presents the LOS analysis for the Highway 26/Ten Eyck Road intersection for 2029 without the project during the studied peak hours. Detailed LOS calculation reports are provided in Appendix C.

Table 5. Estimated Level of Service at Study Area Intersection for 2029 Without Project Conditions

		AM Peak	Hour		PM Peak	Hour
INTERSECTION*	LOS	Delay (sec/veh)	Intersection v/c Ratio	LOS	Delay (sec/veh)	Intersection v/c Ratio
Highway 26/Ten Eyck Road	В	11.1	0.64	С	24.0	0.81

^{*}This TIA evaluates the intersection in its existing configuration. The northbound and southbound left-turn lanes called for in City of Sandy's TSP are not evaluated.

Finding: In 2029 without the project, the Highway 26/Ten Eyck Road intersection will operate above LOS standards.

Table 6 presents the LOS analysis for the Highway 26/Ten Eyck Road intersection for 2029 with the project during the studied peak hours. It includes the LOS results with a westbound right-turn lane. Detailed LOS calculation reports are provided in Appendix C.

Table 6. Estimated Level of Service at Study Area Intersection for 2029 With Project Conditions

		AM Peak	Hour		PM Peak	Hour
INTERSECTION*	LOS	Delay (sec/veh)	Intersection v/c Ratio	LOS	Delay (sec/veh)	Intersection v/c Ratio
Highway 26/Ten Eyck Road	В	12.0	0.66	С	24.4	0.84
Highway 26/Ten Eyck Road With Westbound Right-Turn Lane	В	11.4	0.66	С	23.0	0.83

^{*}This TIA evaluates the intersection in its existing configuration and with the addition of a westbound right-turn lane. The northbound and southbound left-turn lanes called for in City of Sandy's TSP are not evaluated.

Findings: In 2029 with the project, the Highway 26/Ten Eyck Road intersection will operate above LOS standards. The operation of the Highway 26/Ten Eyck Road intersection will not significantly improve with the installation of a westbound right-turn lane on Highway 26.

Recommendation: Do not install a right-turn lane for westbound Highway 26 at Ten Eyck Road.

The City's TSP calls for left-turn lanes on Ten Eyck Road and Wolf Drive at Highway 26, project M8. This improvement alternative was not evaluated for LOS, but the findings of the evaluation without M8 improvements did not support this relatively expensive improvement. The applicant is advised to maintain the existing 39-foot street width on Ten Eyck Road frontage to allow this improvement in the future.

Finding: Maintain the width of 39 feet on Ten Eyck Road to provide the necessary width a for future left-turn lane.

Queueing Analysis

Table 7 presents the 95th percentile queue analysis for the Highway 26/Ten Eyck Road and Ten Eyck Road/Pleasant Street intersections to verify the queuing at the intersections do not conflict with each other and that the existing lane storage is not exceeded. The queue analysis is based on procedures and settings outlined in ODOT APMv2 when using Trafficware's SimTraffic (Version 10) simulation software. Table 7 includes a column with queue model results with the inclusion of the southbound left-turn lane on Ten Eyck Road, City TSP project M8, between Highway 26 and the east segment of Pleasant Street. The detailed queuing reports are provided in Appendix C.

Table 7. 95th Percentile Queue Analysis for 2029 Conditions

	lana/lana	Available		y AM Pea Queue (ft)	k Hour		y PM Pea Queue (ft)	k Hour
Intersection	Lane/Lane Group	Storage ² (ft)	2029 Without Project	2029 With Project	Add SB LT Lane	2029 Without Project	2029 With Project	Add SB LT Lane
	EB LT	120	100	125	125	225	250	250
	EB TH	400	250	275	275	375	475	450
	EB TH	1,000	200	200	200	350	425	400
	EB RT	100	75	50	50	175	175	175
Highway 26/Ten Eyck Road	WB LT	100	0	0	0	50	75	75
Lyck Rodd	WB TH	1,200	275	275	300	500	500	500
	WB TH+RT	1,200	250	250	275	475	475	475
	NB	275	175	175	175	275	250	250
	SB	120	200	200	175	325	350	225
Ten Eyck	EB	120	75	50	50	75	100	75
Road/Pleasant Street ¹	WB	120	0	50	50	50	125	75

BOLD font indicates the queue exceeds the noted available storage.

Eastbound left-turn queues at the Highway 26/Ten Eyck Road signal are anticipated to spill beyond the 120 feet of available storage lane during the PM peak hour, both without and with the project trips. The queue will block the eastbound-to-westbound Highway 26 connector and the ARCO gas station driveway. These queues will be made slightly longer by the addition of the Sandy Health Clinic project trips due to the eight new PM peak hour trips turning left on to Ten Eyck Road.

Eastbound through queues at the Highway 26/Ten Eyck Road signal are anticipated to spill beyond several driveways during the PM peak hour; with the addition of the Sandy Health Clinic project trips, the queues could spill beyond the Revenue Avenue intersection, likely due to the eastbound left-turn lane overflow.

Eastbound right-turn queues at the Highway 26/Ten Eyck Road signal are anticipated to spill beyond the 100 feet of available storage lane during the PM peak hour, both without and with the project trips. The Sandy Health Clinic project trips will have negligible effect on these queues.

Southbound queues at the Highway 26/Ten Eyck Road signal are anticipated to spill beyond the upstream intersections, both without and with the project trips. The queue will routinely block the driveways closest to the intersection (serving the lot on the northwest intersection corner) and the east segment of Pleasant Street. During the PM peak hour, the west segment of Pleasant Street also will be blocked by the southbound queue. The southbound queues will be made slightly longer by the addition of the Sandy Health Clinic project trips due to most trips turning right in the PM peak hour (19 of 21 trips). The queueing is much more impacted by the 2.0%

¹ The queue lengths are reported for both intersections.

² For exclusive turn lanes, the available storage noted represents the length of the full-width lane, exclusive of the taper or transition. For continuous lanes, the available storage noted represents the distance from the intersection stop bar to the next upstream intersection or major driveway.

growth for each turning movement over the next nine years. This may be overly conservative as the 2.0% growth used in this report was based on ODOT through movements on Highway 26.

Finding: The trips from the Sandy Health Clinic do not significantly contribute to the queueing. The addition of a southbound left-turn lane to Ten Eyck Road with the future City project may reduce southbound queues at Highway 26. However, the 95th percentile queues will still extend beyond the east segment of Pleasant Street.

Recommendation: Collect additional turning movement counts in the future to verify the intersection volumes, especially the eastbound left-turn and southbound traffic movements, are growing at 2.0% annually. Reevaluate the queuing with the next TSP update.

SAFETY EVALUATION

The safety evaluation focused on crash history at the existing intersection, bike evaluation, pedestrian safety, and Americans with Disabilities Act (ADA) access.

Traffic Safety

The proposed Sandy Health Clinic was evaluated for traffic safety based on the existing crash history of the Highway 26/Ten Eyck Road intersection, sight distance of driveways, and driveway/intersection spacing. The crash history was reviewed for the last available 5-year period (January 1, 2014 to December 31, 2018). The records show 11 crashes at the Highway 26/Ten Eyck intersection with 6 rear-end crashes (5 of those on Highway 26) and 2 right-angle crashes. None were related to the right-turning vehicles and none were related to bicycles. The intersection crash rate per million vehicles entering is 0.26. The mean critical crash rate for a four leg, signalized intersection in an urban area is 0.40. See Appendix D for the crash history and crash rate calculations.

Finding: The intersection crash rate is lower than the mean critical crash rate. No further investigation is necessary.

The stopping sight distance necessary is based on the existing speed limit and the likely travel speeds on the east leg of Pleasant Street. As a local street, Pleasant Street is assumed to have a 25 mph speed limit, but based on the dead end 450 feet to the east of the proposed site driveway and an intersection of Ten Eyck Road 150 feet to the west of the proposed site driveway, speeds are assumed to be 20 mph approaching the driveway. The stopping sight distance is adequate for looking east and west, but care should be taken not to install landscaping or signs along the site frontage that may restrict sight distance below 200 feet.

Finding: The proposed driveway will meet stopping sight distance standards.

Recommendation: The site plan should take care to maintain approximately 200 feet of sight distance in both directions on Pleasant Street.

The applicant proposes elimination of an existing site driveway on Ten Eyck Road. No crashes were noted associated with this driveway, but removing it will likely reduce risk of crashes in the future. The driveway's proximity to the Highway 26 signal (70 feet) may have contributed to past crashes. The same is true of eliminating the existing driveway on Pleasant Street that is close to Ten Eyck Road but is much less likely to be a safety concern due to the low traffic volume on Pleasant Street.

Finding: The project should improve safety on Ten Eyck Road and Pleasant Street by eliminating two driveways.

Bicycle Safety

The multi-model safety evaluation is related to the bike lane and motor vehicle lane interaction at the westbound bike lane approaching the Highway 26/Ten Eyck Road intersection. The existing and future conditions are evaluated using the bicycle LTS. The westbound Highway 26 approach to Ten Eyck Road has a 135-foot-long taper (slip lane) with a dropped bike lane. The right-turn lane is approximately 50 feet long with a dashed merge area approximately 50 feet long. Based on ODOT APMv2: "A roadway with no marked bike lanes and a right-turn lane will be a high stress location unless the right-turn lane is short and rarely used. This condition will also occur if a bike lane is dropped ahead of an intersection. If the turn lane is short (less than 75') then there is no impact on the LTS."

With the development, the right-turn volume will increase from 16 vehicles per hour to approximately 22 vehicles in the AM and PM peak hour. In the AM hours only one bicycle used the westbound bike lane. In the PM peak hours, no bicycles were counted. With the short length of the right-turn lane, there is no impact on the bicycle LTS.

Finding: No mitigation is necessary for the existing slip lane and bike lane due to short length of the lane and the low turning movement volumes.

Recommendation: Make no change to the existing westbound slip lane.

Pedestrian Safety

The current site does not have a sidewalk on the east side Ten Eyck Road. The City has a sidewalk project in process to install a sidewalk on Ten Eyck Road and Pleasant Street, referred to as the SE Ten Eyck Road & Pleasant Street Curb and Sidewalk Improvements. The project will provide ADA access to the Sandy Health Clinic.

The project may be modified to reduce the turning radius on northeast corner of the Highway 26/Ten Eyck Road intersection. This will reduce vehicle speeds and provide more area for ramp improvements at the corner. This should improve pedestrian safety.

Finding: The proposed modification to the City's sidewalk project will improve pedestrian safety but not reduce the width of Ten Eyck Road below 36-feet to allow future installation of a left-turn lane.

FINDINGS

The TIA findings are summarized below:

- The proposed Sandy Health Clinic project will generate 355 net new trips on an average weekday, 34 net new trips in the AM peak hour of the adjacent streets, and 30 net new trips in the PM peak hour of the adjacent streets.
- The existing Highway 26/Ten Eyck Road intersection operates above LOS standards.
- In 2022 without the project, the Highway 26/Ten Eyck Road intersection will operate above LOS standards.
- In 2022 with the project, the Highway 26/Ten Eyck Road intersection will operate at above LOS standards.
- In 2029 without the project, the Highway 26/Ten Eyck Road intersection will operate above LOS standards
- In 2029 with the project, the Highway 26/Ten Eyck Road intersection will operate above LOS standards.
- In 2029 with the project, the operation of the Highway 26/Ten Eyck Road intersection will not significantly improve with the installation of a westbound right-turn lane on Highway 26.

- The trips from the Sandy Health Clinic do not significantly contribute to queueing at the Highway 26/Ten Eyck Road intersection.
- Maintain the width of 39 feet on Ten Eyck Road to provide the necessary width a for future left-turn lane.
- The intersection crash rate is lower than the mean critical crash rate. No further investigation is necessary.
- The proposed driveway on Pleasant Street will meet stopping sight distance standards.
- The project should improve safety on Ten Eyck Road and Pleasant Street by eliminating two existing driveways (one on each roadway).
- No mitigation is necessary for the existing slip lane and bike lane due to its short length and low turning movements.
- The proposed modification to the City's sidewalk project will improve pedestrian safety but not reduce the width of Ten Eyck Road below 36-feet to allow future installation of a left-turn lane.

RECOMMENDATIONS

The TIA recommendations are summarized below:

- Do not install a right-turn lane for westbound Highway 26 at Ten Eyck Road.
- Make no change to the existing westbound slip lane.
- Collect additional turning movement counts in the future to verify the intersection volumes, especially the eastbound left-turn and southbound traffic volumes, are growing at 2.0% annually. Reevaluate the queuing with the next TSP update.
- The site plan should take care to maintain approximately 200 feet of sight distance in both directions on Pleasant Street.

ANDREW

EXPIRES: 12/31/20

CLOSING

Please feel free to contact me at 360.567.2117 or John.Manix@pbsusa.com with any questions or comments.

Sincerely,

John Manix, PE

Senior Traffic Engineer

Attachments: Figure 1. Vicinity Map

Figure 2. Site Plan

Figure 3. Trip Distribution and Assignment

Figure 4. 2040 With Project Volumes

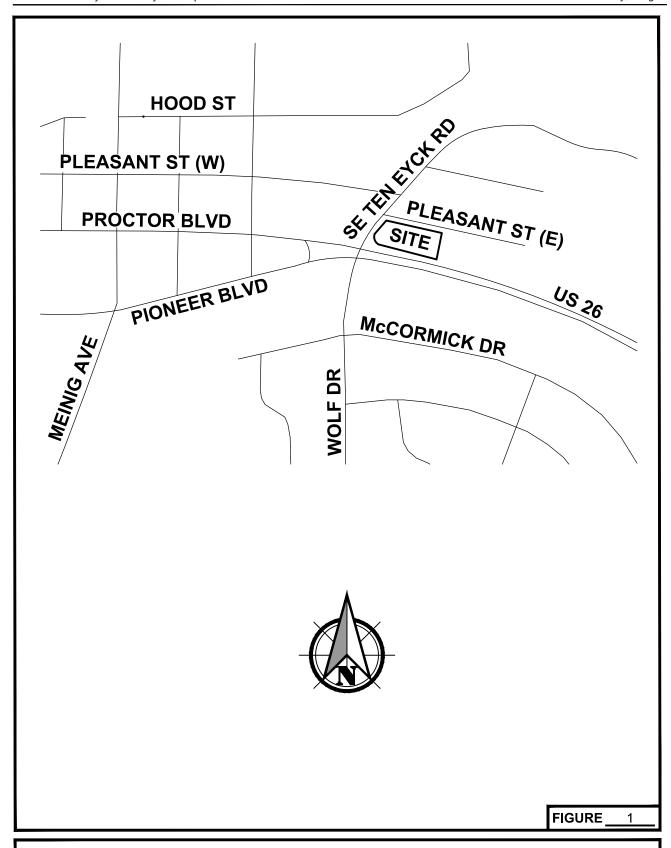
Appendix A. Traffic Counts

Appendix B. Trip Generation Calculations

Appendix C. Level of Service Calculations

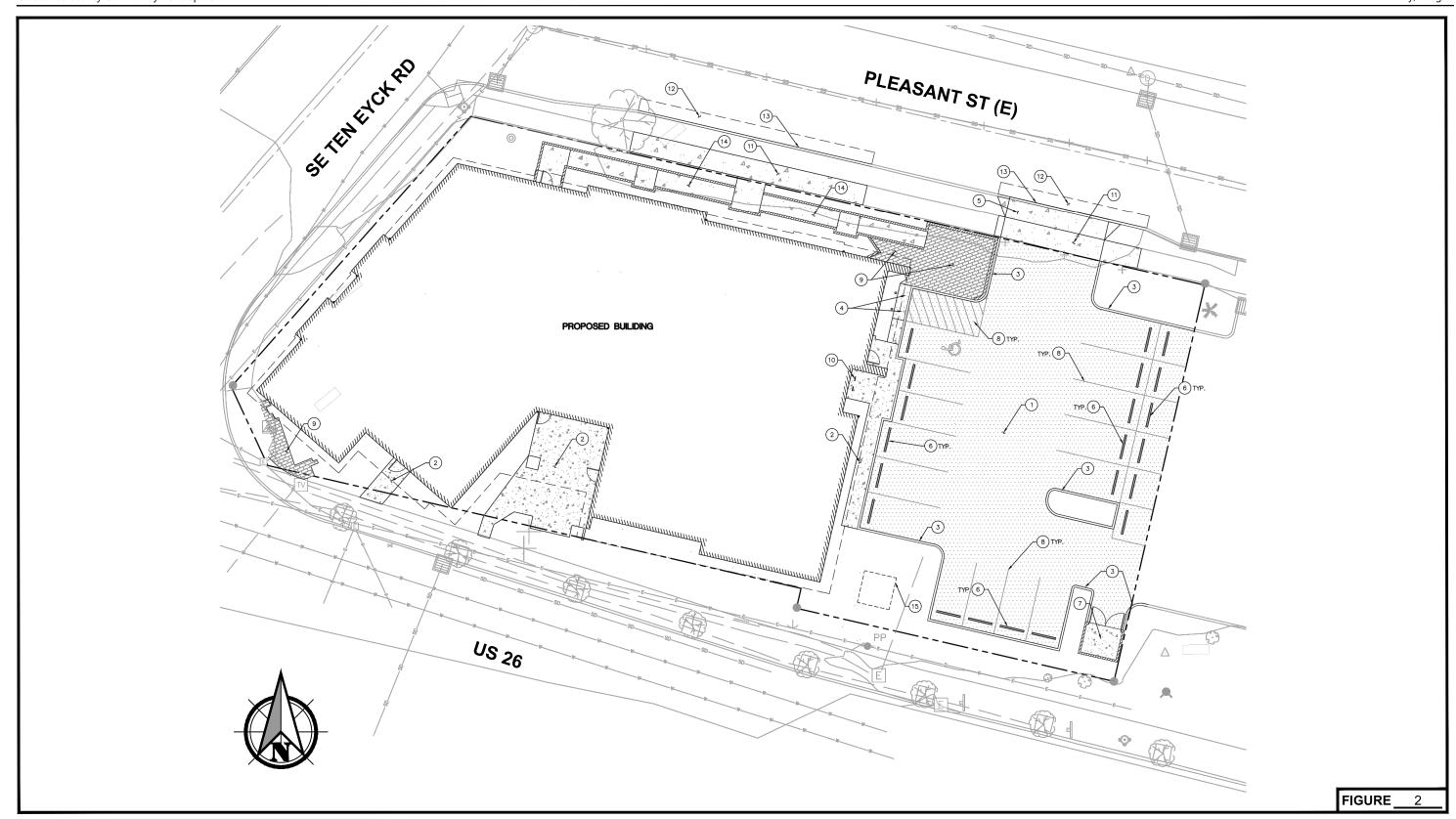
Appendix D. Crash History

BJ:DAH,JAM:mo



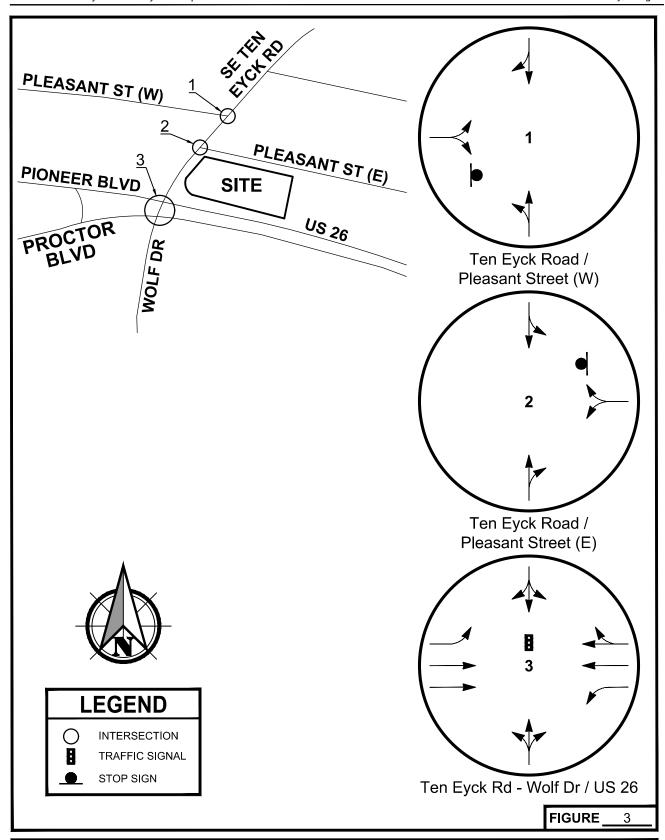
Vicinity Map Sandy Health Clinic





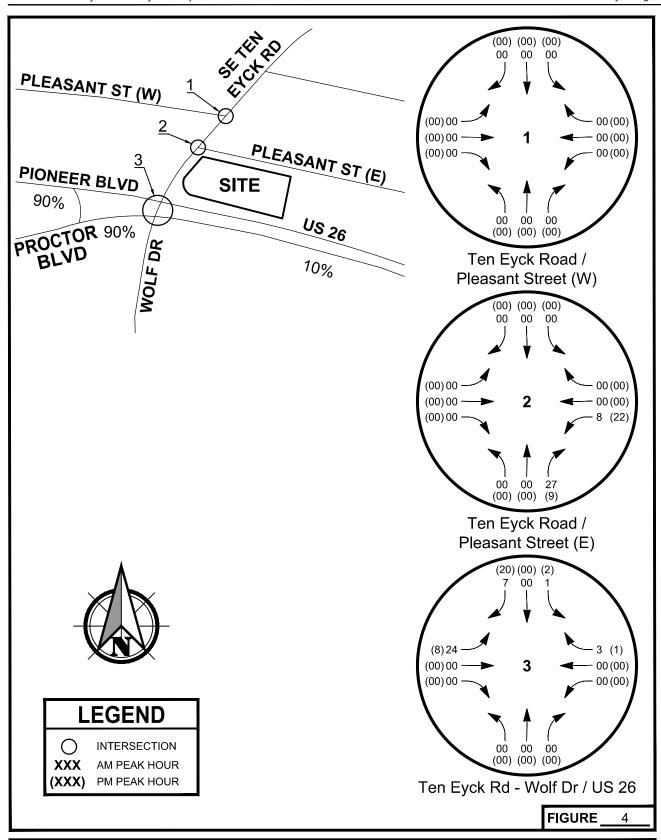
Site Plan
Sandy Health Clinic





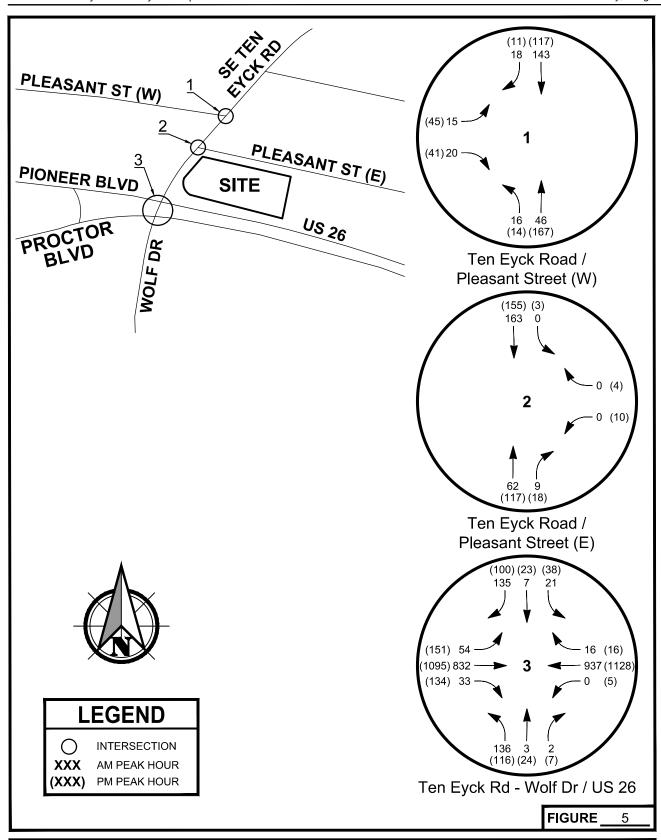
Existing Lane ConfigurationsSandy Health Clinic





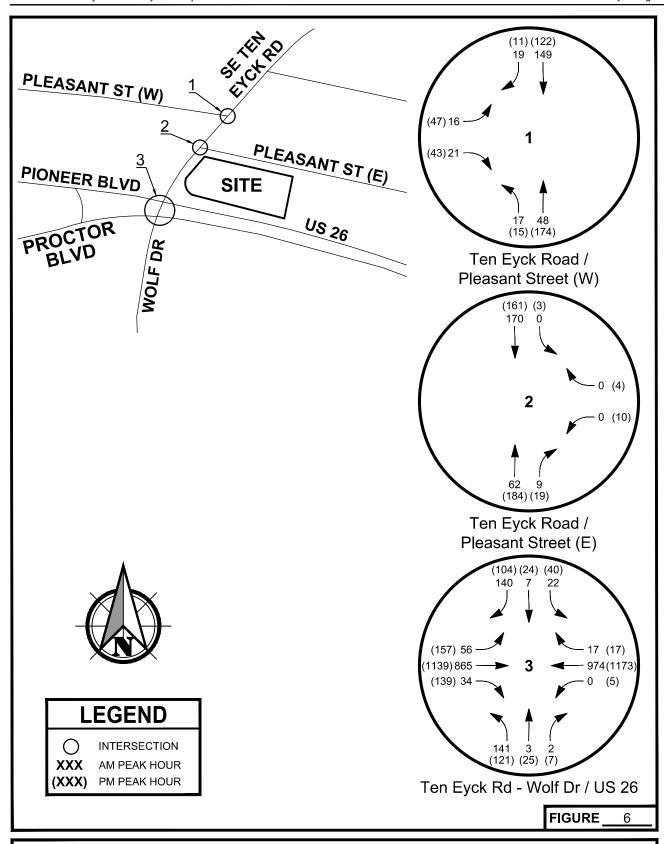
Trip Distribution & Assignment Sandy Health Clinic





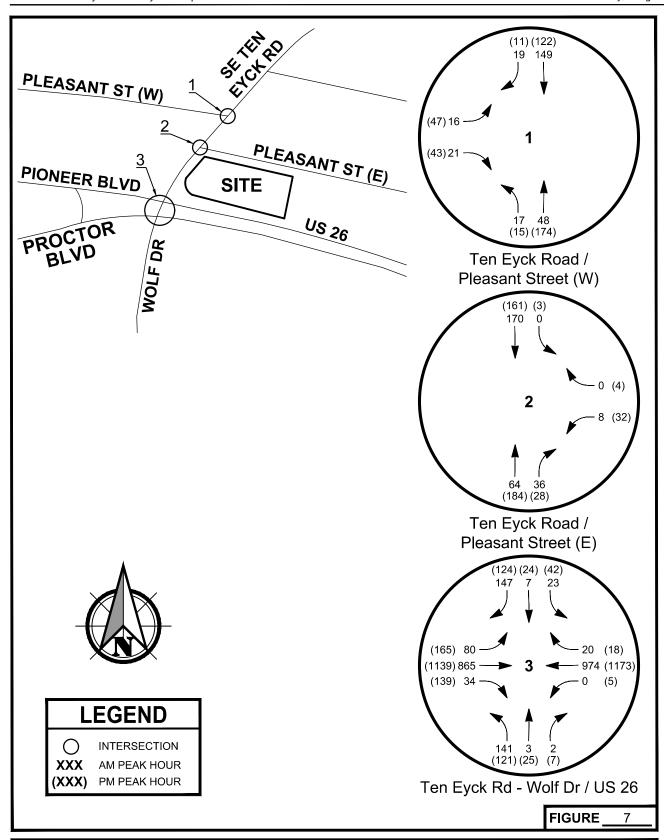
2020 Existing Traffic Volumes Sandy Health Clinic





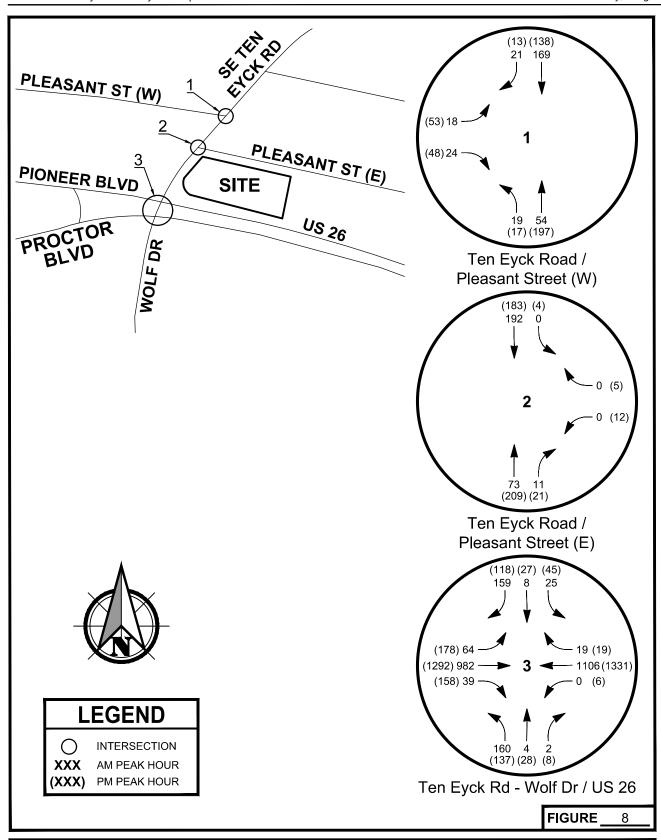
2022 Without Project Traffic Volumes Sandy Health Clinic





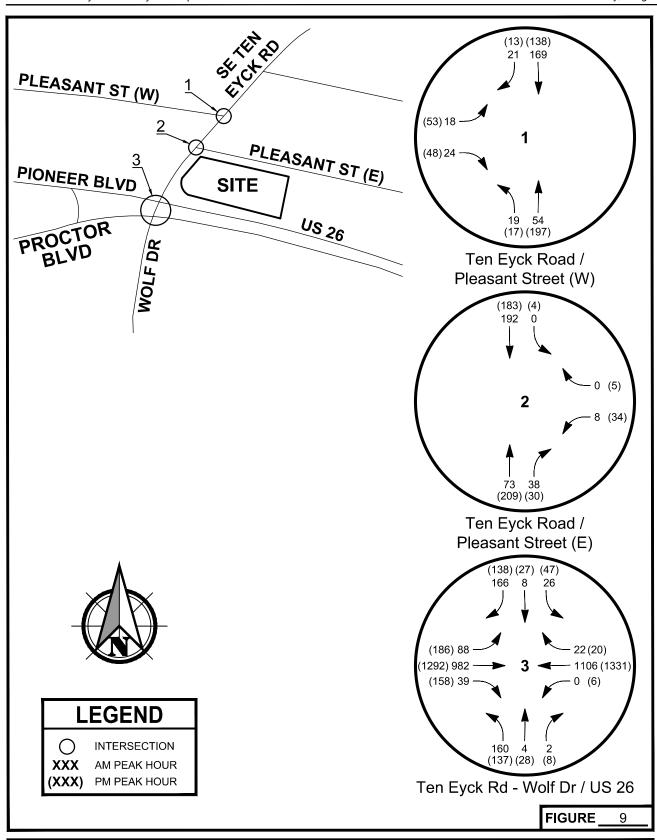
2022 With Project Traffic Volumes Sandy Health Clinic





2029 Without Project Traffic Volumes Sandy Health Clinic





2029 With Project Traffic Volumes Sandy Health Clinic



Appendix A Traffic Counts

Total Vehicle Summary

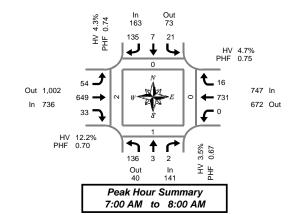


Clay Carney (503) 833-2740

Ten Eyck Rd & Hwy 26

Wednesday, February 19, 2020 7:00 AM to 9:00 AM

5-Minute Interval Summary 7:00 AM to 9:00 AM



Interval		North	bound			South	bound			Eastb	ound			Westk	ound				Pedes	trians	
Start		Ten E	yck Rd			Ten E	yck Rd			Hwy	/ 26			Hwy	/ 26		Interval		Cross		
Time	L	T	R	Bikes	L	T	R	Bikes	L	T	R	Bikes	L	Т	R	Bikes	Total	North	South	East	West
7:00 AM	13	0	0	0	3	0	11	0	2	33	2	0	0	61	1	0	126	0	0	0	0
7:05 AM	16	0	0	0	0	0	15	0	6	39	0	0	0	78	1	0	155	0	1	0	1
7:10 AM	20	0	0	0	3	1	12	0	2	26	2	0	0	83	1	0	150	0	0	0	0
7:15 AM	15	0	0	0	2	0	18	0	2	53	3	0	0	85	1	0	179	0	0	0	0
7:20 AM	16	2	0	0	2	0	17	0	3	39	3	0	0	64	0	0	146	0	0	0	0
7:25 AM	9	0	0	0	1	0	12	0	2	39	4	0	0	74	3	0	144	0	0	0	0
7:30 AM	7	0	0	0	0	1	9	0	4	53	4	0	0	58	3	0	139	0	0	0	0
7:35 AM	12	1	0	0	0	1	13	0	10	57	4	0	0	45	1	0	144	0	0	0	0
7:40 AM	5	0	0	0	3	1	5	0	7	71	2	0	0	55	0	0	149	0	0	0	0
7:45 AM	8	0	0	0	3	1	13	0	4	86	3	0	0	49	3	1	170	0	0	0	1
7:50 AM	5	0	1	0	4	1	4	0	8	79	4	0	0	41	0	0	147	0	0	0	0
7:55 AM	10	0	1	0	0	1	6	0	4	74	2	0	0	38	2	0	138	0	0	0	0
8:00 AM	4	0	0	0	1	0	8	0	1	62	4	0	0	45	1	0	126	0	0	0	0
8:05 AM	12	0	0	0	1	0	9	0	3	55	1	0	0	43	0	0	124	0	0	0	1
8:10 AM	5	0	0	0	0	0	9	0	4	60	2	0	0	46	0	0	126	0	0	0	0
8:15 AM	4	0	0	0	0	0	8	0	4	47	1	0	1	51	0	0	116	0	0	0	0
8:20 AM	7	0	0	0	3	0	12	0	4	62	1	0	0	48	2	0	139	0	0	0	0
8:25 AM	6	2	1	0	1	0	11	0	3	61	4	0	0	40	0	0	129	0	0	0	0
8:30 AM	7	1	0	0	6	0	9	0	7	60	1	0	1	47	1	0	140	0	0	0	1
8:35 AM	12	0	0	0	1	1	7	0	5	53	3	0	0	53	2	0	137	0	0	0	0
8:40 AM	9	1	1	0	2	1	11	0	1	56	2	0	1	53	0	0	138	0	0	0	0
8:45 AM	15	0	0	0	5	0	13	0	10	64	3	0	0	51	1	0	162	0	0	0	0
8:50 AM	4	1	0	0	2	0	14	0	5	60	3	0	0	62	2	0	153	0	0	0	0
8:55 AM	3	0	0	0	3	1	4	0	3	60	2	0	0	45	0	0	121	2	0	0	0
Total Survey	224	8	4	0	46	10	250	0	104	1,349	60	0	3	1,315	25	1	3,398	2	1	0	4

15-Minute Interval Summary

7:00 AM to 9:00 AM

Interval Start			bound yck Rd				bound yck Rd			Eastb Hwy				Westk Hwy			Interval		Pedes		
Time	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	Total	North	South	East	West
7:00 AM	49	0	0	0	6	1	38	0	10	98	4	0	0	222	3	0	431	0	1	0	1
7:15 AM	40	2	0	0	5	0	47	0	7	131	10	0	0	223	4	0	469	0	0	0	0
7:30 AM	24	1	0	0	3	3	27	0	21	181	10	0	0	158	4	0	432	0	0	0	0
7:45 AM	23	0	2	0	7	3	23	0	16	239	9	0	0	128	5	1	455	0	0	0	1
8:00 AM	21	0	0	0	2	0	26	0	8	177	7	0	0	134	1	0	376	0	0	0	1
8:15 AM	17	2	1	0	4	0	31	0	11	170	6	0	1	139	2	0	384	0	0	0	0
8:30 AM	28	2	1	0	9	2	27	0	13	169	6	0	2	153	3	0	415	0	0	0	1
8:45 AM	22	1	0	0	10	1	31	0	18	184	8	0	0	158	3	0	436	2	0	0	0
Total Survey	224	8	4	0	46	10	250	0	104	1,349	60	0	3	1,315	25	1	3,398	2	1	0	4

Peak Hour Summary

7:00 AM to 8:00 AM

ſ	By			bound yck Rd				bound yck Rd			Eastb Hwy	ound / 26			West! Hw	oound y 26		Total
	Approach	In	Out	Total	Bikes	In	Out	Total	Bikes	In	Out	Total	Bikes	In	Out	Total	Bikes	
ı	Volume	141	40	181	0	163	73	236	0	736	1,002	1,738	0	747	672	1,419	1	1,787
	%HV		3.5	5%			4.3	3%			12.	2%			4.7	7%		7.7%
	PHF		0.	67			0.	74			0.	70			0.	75		0.92

	Pedes	trians	
	Cross	swalk	
North	South	East	West
0	1	0	2

By Movement			bound yck Rd				bound yck Rd			Eastb Hwy				Westk Hwy	oound y 26		Total
Movement	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	
Volume	136	3	2	141	21	7	135	163	54	649	33	736	0	731	16	747	1,787
%HV	3.7%	0.0%	0.0%	3.5%	23.8%	0.0%	1.5%	4.3%	5.6%	13.1%	6.1%	12.2%	0.0%	4.8%	0.0%	4.7%	7.7%
PHF	0.67	0.38	0.25	0.67	0.53	0.58	0.72	0.74	0.64	0.68	0.69	0.70	0.00	0.74	0.57	0.75	0.92

Rolling Hour Summary

7:00 AM to 9:00 AM

Interval		North	bound			South	bound			Easth	ound			Westl	bound				Pedes	strians
Start		Ten E	yck Rd			Ten E	yck Rd			Hw	y 26			Hw	y 26		Interval		Cros	swalk
Time	L	Т	R	Bikes	L	T	R	Bikes	L	T	R	Bikes	L	Т	R	Bikes	Total	North	South	Eas
7:00 AM	136	3	2	0	21	7	135	0	54	649	33	0	0	731	16	1	1,787	0	1	0
7:15 AM	108	3	2	0	17	6	123	0	52	728	36	0	0	643	14	1	1,732	0	0	0
7:30 AM	85	3	3	0	16	6	107	0	56	767	32	0	1	559	12	1	1,647	0	0	0
7:45 AM	89	4	4	0	22	5	107	0	48	755	28	0	3	554	11	1	1,630	0	0	0
8:00 AM	88	5	2	0	25	3	115	0	50	700	27	0	3	584	9	0	1,611	2	0	0

		Pedes	trians	
		Cross	swalk	
	North	South	East	West
	0	1	0	2
	0	0	0	2
	0	0	0	2
1	0	0	0	3
	2	0	0	2

Heavy Vehicle Summary



Clay Carney (503) 833-2740

Ten Eyck Rd & Hwy 26

Wednesday, February 19, 2020 7:00 AM to 9:00 AM 2 0 5 85 + 35 2 0 0 0 85 + 35 2 0 0 0 Out In 2 5 Peak Hour Summary 7:00 AM to 8:00 AM

Out 42

In 90

Heavy Vehicle 5-Minute Interval Summary 7:00 AM to 9:00 AM

Interval			bound				bound				ound				oound		
Start		Ten E	yck Rd			Ten E	yck Rd			Hw	y 26			Hw	y 26		Interval
Time	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	Total
7:00 AM	1	0	0	1	0	0	0	0	0	8	1	9	0	5	0	5	15
7:05 AM	1	0	0	1	0	0	0	0	0	13	0	13	0	2	0	2	16
7:10 AM	0	0	0	0	1	0	0	1	0	6	0	6	0	4	0	4	11
7:15 AM	2	0	0	2	0	0	0	0	1	7	0	8	0	3	0	3	13
7:20 AM	0	0	0	0	1	0	0	1	0	5	0	5	0	4	0	4	10
7:25 AM	0	0	0	0	0	0	0	0	0	5	0	5	0	2	0	2	7
7:30 AM	0	0	0	0	0	0	0	0	11	2	0	3	0	0	0	0	3
7:35 AM	0	0	0	0	0	0	0	0	1	3	0	4	0	2	0	2	6
7:40 AM	0	0	0	0	1	0	0	1	0	10	0	10	0	4	0	4	15
7:45 AM	0	0	0	0	1	0	1	2	0	8	0	8	0	4	0	4	14
7:50 AM	0	0	0	0	1	0	1	2	0	9	1	10	0	1	0	1	13
7:55 AM	1	0	0	1	0	0	0	0	0	9	0	9	0	4	0	4	14
8:00 AM	0	0	0	0	0	0	0	0	0	7	0	7	0	4	0	4	11
8:05 AM	0	0	0	0	0	0	1	1	0	5	11	6	0	5	0	5	12
8:10 AM	0	0	0	0	0	0	0	0	0	5	0	5	0	7	0	7	12
8:15 AM	0	0	0	0	0	0	0	0	0	2	0	2	0	5	0	5	7
8:20 AM	1	0	0	1	0	0	0	0	0	2	0	2	0	8	0	8	11
8:25 AM	0	0	1	1	0	0	0	0	0	8	0	8	0	6	0	6	15
8:30 AM	1	0	0	1	1	0	0	1	0	3	0	3	1	11	0	12	17
8:35 AM	1	0	0	1	0	0	1	1	1	3	0	4	0	2	1	3	9
8:40 AM	0	0	0	0	0	0	0	0	0	3	0	3	0	3	0	3	6
8:45 AM	0	0	0	0	0	0	0	0	0	4	0	4	0	3	0	3	7
8:50 AM	0	0	0	0	0	0	2	2	0	6	1	7	0	5	0	5	14
8:55 AM	0	0	0	0	0	0	0	0	0	8	0	8	0	3	0	3	11
Total Survey	8	0	1	9	6	0	6	12	4	141	4	149	1	97	1	99	269

Heavy Vehicle 15-Minute Interval Summary 7:00 AM to 9:00 AM

Interval Start			bound yck Rd				bound yck Rd				oound y 26				oound y 26		Interval
Time	L	Т	R	Total	L	T	R	Total	L	Т	R	Total	L	Т	R	Total	Total
7:00 AM	2	0	0	2	1	0	0	1	0	27	1	28	0	11	0	11	42
7:15 AM	2	0	0	2	1	0	0	1	1	17	0	18	0	9	0	9	30
7:30 AM	0	0	0	0	1	0	0	1	2	15	0	17	0	6	0	6	24
7:45 AM	1	0	0	1	2	0	2	4	0	26	1	27	0	9	0	9	41
8:00 AM	0	0	0	0	0	0	1	1	0	17	1	18	0	16	0	16	35
8:15 AM	1	0	1	2	0	0	0	0	0	12	0	12	0	19	0	19	33
8:30 AM	2	0	0	2	1	0	1	2	1	9	0	10	1	16	1	18	32
8:45 AM	0	0	0	0	0	0	2	2	0	18	1	19	0	11	0	11	32
Total Survey	8	0	1	9	6	0	6	12	4	141	4	149	1	97	1	99	269

Heavy Vehicle Peak Hour Summary 7:00 AM to 8:00 AM

Ву			bound yck Rd			bound yck Rd			ound v 26			oound v 26	Total
Approach	In	Out	Total	In	Out	Total	In	Out	Total	In	Out	Total	
Volume	5	2	7	7	3	10	90	42	132	35	90	125	137
PHF	0.42			0.35			0.80			0.80			0.82

By Movement			bound yck Rd				bound yck Rd			Eastb Hwy	ound / 26			West! Hw	oound / 26		Total
wovernent	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	
Volume	5	0	0	5	5	0	2	7	3	85	2	90	0	35	0	35	137
PHF	0.42	0.00	0.00	0.42	0.42	0.00	0.25	0.35	0.38	0.79	0.50	0.80	0.00	0.80	0.00	0.80	0.82

Heavy Vehicle Rolling Hour Summary 7:00 AM to 9:00 AM

			•••														
Interval		North	bound			South	bound			Eastl	oound			West	oound		
Start		Ten E	yck Rd			Ten E	yck Rd			Hw	y 26			Hw	y 26		Interval
Time	L	Т	R	Total	L	T	R	Total	L	T	R	Total	L	Т	R	Total	Total
7:00 AM	5	0	0	5	5	0	2	7	3	85	2	90	0	35	0	35	137
7:15 AM	3	0	0	3	4	0	3	7	3	75	2	80	0	40	0	40	130
7:30 AM	2	0	1	3	3	0	3	6	2	70	2	74	0	50	0	50	133
7:45 AM	4	0	1	5	3	0	4	7	1	64	2	67	1	60	1	62	141
8:00 AM	3	0	1	4	1	0	4	5	1	56	2	59	1	62	1	64	132

Peak Hour Summary All Traffic Data Clay Carney (503) 833-2740 Ten Eyck Rd & Hwy 26 7:00 AM to 8:00 AM Wednesday, February 19, 2020 Ten Eyck Rd Bikes 0 163 73 135 21 Ľ 4 Peds 0 Hwy 26 Bikes 1 16 1002 731 747 0 ~ Peds 54 672 736 649 33 4 Bikes 0 Hwy 26 Peds 1 **K** 1 7 136 2 Ten Eyck Rd 40 141 Bikes HV% Approach PHF Volume EΒ 0.70 12.2% 736 WB 0.75 4.7% 747 NB 0.67 3.5% 141 SB 0.74 4.3% 163 Intersection 0.92 7.7% 1,787 Count Period: 7:00 AM to 9:00 AM

Total Vehicle Summary

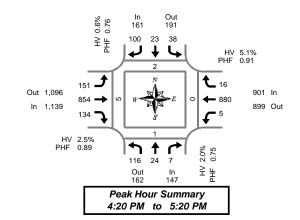


Clay Carney (503) 833-2740

Ten Eyck Rd & Hwy 26

Wednesday, February 19, 2020 4:00 PM to 6:00 PM

5-Minute Interval Summary 4:00 PM to 6:00 PM



Interval		North	bound			South	bound			Eastb	ound			Westb	ound				Pedes	trians	
Start		Ten E	yck Rd			Ten E	yck Rd			Hwy	/ 26			Hwy	/ 26		Interval		Cross	swalk	
Time	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	Total	North	South	East	West
4:00 PM	5	4	0	0	2	2	14	0	11	55	19	0	1	76	2	0	191	0	0	0	1
4:05 PM	10	2	11	0	4	2	6	0	17	78	5	0	0	48	4	0	177	0	0	0	0
4:10 PM	4	3	0	0	0	1	7	0	13	73	12	0	0	68	1	0	182	4	0	0	2
4:15 PM	4	3	0	0	5	0	5	0	9	67	12	0	0	81	3	0	189	1	0	0	0
4:20 PM	6	2	0	0	1	1	5	0	11	73	8	0	0	81	0	0	188	2	0	0	0
4:25 PM	11	0	11	0	4	1	8	0	8	60	11	0	0	72	0	0	176	0	0	0	0
4:30 PM	6	2	0	0	3	0	4	0	9	70	17	0	0	64	2	0	177	.0	0	0	0
4:35 PM	14	2	0	0	2	4	6	0	13	70	6	0	0	83	11	0	201	0	0	0	0
4:40 PM	11	2	0	0	0	6	10	0	19	80	12	0	1	75	11	0	217	0	0	0	0
4:45 PM	10	1	2	0	2	0	4	0	18	85	18	0	1	63	2	0	206	0	0	0	3
4:50 PM	12	6	0	0	3	2	15	0	11	55	12	0	1	61	3	0	181	0	1	0	1
4:55 PM	11	1	2	0	4	2	6	0	9	52	14	0	1	89	3	0	194	0	0	0	0
5:00 PM	12	4	1	0	4	2	9	0	18	60	7	0	1	85	0	0	203	0	0	0	0
5:05 PM	7	2	0	0	4	2	14	0	13	99	7	0	0	67	111	0	216	. 0	0	0	0
5:10 PM	7	1	0	0	6	2	7	0	8	72	13	0	0	71	3	0	190	0	0	0	1
5:15 PM	9	1	1	0	5	1	12	0	14	78	9	0	0	69	0	0	199	0	0	0	0
5:20 PM	8	1	0	0	4	1	4	0	12	59	8	0	1	68	11	0	167	0	0	0	0
5:25 PM	6	2	0	0	5	0	7	0	11	71	7	0	1	73	0	0	183	1	0	0	0
5:30 PM	4	0	0	0	1	3	9	0	14	77	10	0	0	62	2	0	182	0	0	0	0
5:35 PM	8	2	1	0	1	0	6	0	18	80	10	0	0	36	0	0	162	0	1	0	0
5:40 PM	5	1	0	0	4	1	10	0	16	57	4	0	0	48	0	0	146	1	0	0	0
5:45 PM	7	3	1	0	3	0	7	0	12	65	9	0	0	62	11	0	170	0	0	0	11
5:50 PM	12	1	0	0	2	0	8	0	13	72	5	0	0	63	1	0	177	1	0	0	2
5:55 PM	4	2	1	0	3	1	9	0	17	63	14	0	0	48	1	0	163	0	0	0	0
Total Survey	193	48	11	0	72	34	192	0	314	1,671	249	0	8	1,613	32	0	4,437	10	2	0	11

15-Minute Interval Summary 4:00 PM to 6:00 PM

Interval			bound				bound			Eastb	ound				ound				Pedes	trians	
Start		Ten E	yck Rd			Ten E	yck Rd			Hw	/ 26			Hwy	/ 26		Interval		Cross	swalk	
Time	L	T	R	Bikes	L	Т	R	Bikes	L	T	R	Bikes	L	T	R	Bikes	Total	North	South	East	West
4:00 PM	19	9	1	0	6	5	27	0	41	206	36	0	1	192	7	0	550	4	0	0	3
4:15 PM	21	5	1	0	10	2	18	0	28	200	31	0	0	234	3	0	553	3	0	0	0
4:30 PM	31	6	0	0	5	10	20	0	41	220	35	0	1	222	4	0	595	0	0	0	0
4:45 PM	33	8	4	0	9	4	25	0	38	192	44	0	3	213	8	0	581	0	1	0	4
5:00 PM	26	7	1	0	14	6	30	0	39	231	27	0	1	223	4	0	609	0	0	0	1
5:15 PM	23	4	1	0	14	2	23	0	37	208	24	0	2	210	1	0	549	1	0	0	0
5:30 PM	17	3	1	0	6	4	25	0	48	214	24	0	0	146	2	0	490	1	1	0	0
5:45 PM	23	6	2	0	8	1	24	0	42	200	28	0	0	173	3	0	510	1	0	0	3
Total Survey	193	48	11	0	72	34	192	0	314	1,671	249	0	8	1,613	32	0	4,437	10	2	0	11

Peak Hour Summary 4:20 PM to 5:20 PM

I	Bv		North	bound			South	bound			Eastb	ound			West	ound		
	Approach		Ten E	yck Rd			Ten E	yck Rd			Hwy	y 26			Hw	/ 26		Total
	Apploacii	In	Out	Total	Bikes	In	Out	Total	Bikes	In	Out	Total	Bikes	In	Out	Total	Bikes	
ſ	Volume	147	162	309	0	161	191	352	0	1,139	1,096	2,235	0	901	899	1,800	0	2,348
I	%HV		2.0)%			0.0	5%			2.5	5%			5.1	1%		3.4%
	PHF		0.	75			0.	76			0.	89			0.	91		0.94

	Pedes	trians	
	Cross	swalk	
North	South	East	West
2	1	0	5

By Movement			bound yck Rd				bound yck Rd				ound / 26			Westk Hwy	oound / 26		Total
wovernent	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	
Volume	116	24	7	147	38	23	100	161	151	854	134	1,139	5	880	16	901	2,348
%HV	0.9%	8.3%	0.0%	2.0%	0.0%	0.0%	1.0%	0.6%	0.7%	3.3%	0.0%	2.5%	0.0%	5.2%	0.0%	5.1%	3.4%
PHF	0.83	0.55	0.44	0.75	0.63	0.58	0.76	0.76	0.76	0.86	0.76	0.89	0.42	0.91	0.50	0.91	0.94

Rolling Hour Summary 4:00 PM to 6:00 PM

Interval	Northbound Southbound								Eastb	ound			Westk	oound				Pedestrians			
Start		Ten E	yck Rd		Ten Eyck Rd				Hwy 26					Hwy	y 26		Interval	Crosswalk			
Time	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	Total	North	South	East	West
4:00 PM	104	28	6	0	30	21	90	0	148	818	146	0	5	861	22	0	2,279	7	1	0	7
4:15 PM	111	26	6	0	38	22	93	0	146	843	137	0	5	892	19	0	2,338	3	1	0	5
4:30 PM	113	25	6	0	42	22	98	0	155	851	130	0	7	868	17	0	2,334	1	1	0	5
4:45 PM	99	22	7	0	43	16	103	0	162	845	119	0	6	792	15	0	2,229	2	2	0	5
5:00 PM	89	20	5	0	42	13	102	0	166	853	103	0	3	752	10	0	2,158	3	1	0	4

Heavy Vehicle Summary



Clay Carney (503) 833-2740

Ten Eyck Rd & Hwy 26

Wednesday, February 19, 2020 4:00 PM to 6:00 PM 1 2 0
Out In
0 3

Peak Hour Summary
4:20 PM to 5:20 PM

Out 48

In 29

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46

Heavy Vehicle 5-Minute Interval Summary 4:00 PM to 6:00 PM

Interval			bound				bound				oound						
Start		Ten E	yck Rd			Ten E	yck Rd			Hw	y 26			Hw	y 26		Interval
Time	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	Total
4:00 PM	1	0	0	1	0	0	2	2	0	3	0	3	0	4	1	5	11
4:05 PM	0	0	0	0	0	0	0	0	0	8	0	8	0	4	0	4	12
4:10 PM	0	0	0	0	0	0	0	0	0	2	0	2	0	5	0	5	7
4:15 PM	0	0	0	0	0	0	0	0	0	3	0	3	0	6	1	7	10
4:20 PM	0	0	0	0	0	0	0	0	0	8	0	8	0	6	0	6	14
4:25 PM	0	0	0	0	0	0	0	0	0	4	0	4	0	5	0	5	9
4:30 PM	1	2	0	3	0	0	0	0	0	2	0	2	0	3	0	3	8
4:35 PM	0	0	0	0	0	0	0	0	0	2	0	2	0	4	0	4	6
4:40 PM	0	0	0	0	0	0	0	0	0	2	0	2	0	3	0	3	5
4:45 PM	0	0	0	0	0	0	0	0	0	2	0	2	0	4	0	4	6
4:50 PM	0	0	0	0	0	0	0	0	0	1	0	1	0	3	0	3	4
4:55 PM	0	0	0	0	0	0	0	0	0	1	0	1	0	7	0	7	8
5:00 PM	0	0	0	0	0	0	0	0	0	4	0	4	0	3	0	3	7
5:05 PM	0	0	0	0	0	0	0	0	1	0	0	1	0	5	0	5	6
5:10 PM	0	0	0	0	0	0	1	1	0	2	0	2	0	2	0	2	5
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	11	11
5:20 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0	3	3
5:25 PM	0	0	0	0	0	0	0	0	0	11	0	1	0	2	0	2	3
5:30 PM	0	0	0	0	0	0	0	0	0	2	0	2	0	2	0	2	4
5:35 PM	0	0	0	0	0	0	0	0	0	1	0	1	0	2	0	2	3
5:40 PM	1	0	0	11	0	0	0	0	0	1	0	1	0	0	0	0	2
5:45 PM	0	0	0	0	0	0	0	0	11	11	0	2	0	2	0	2	4
5:50 PM	0	0	0	0	0	0	0	0	0	4	0	4	0	3	0	3	7
5:55 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	2	2
Total Survey	3	2	0	5	0	0	3	3	2	54	0	56	0	81	2	83	147

Heavy Vehicle 15-Minute Interval Summary 4:00 PM to 6:00 PM

Interval Start		North Ten E	bound yck Rd		Southbound Ten Eyck Rd						ound / 26			Interval			
Time	L	Т	R	Total	L	T	R	Total	L	Т	R	Total	L	Т	R	Total	Total
4:00 PM	1	0	0	1	0	0	2	2	0	13	0	13	0	13	1	14	30
4:15 PM	0	0	0	0	0	0	0	0	0	15	0	15	0	17	1	18	33
4:30 PM	1	2	0	3	0	0	0	0	0	6	0	6	0	10	0	10	19
4:45 PM	0	0	0	0	0	0	0	0	0	4	0	4	0	14	0	14	18
5:00 PM	0	0	0	0	0	0	1	1	1	6	0	7	0	10	0	10	18
5:15 PM	0	0	0	0	0	0	0	0	0	1	0	1	0	6	0	6	7
5:30 PM	1	0	0	1	0	0	0	0	0	4	0	4	0	4	0	4	9
5:45 PM	0	0	0	0	0	0	0	0	1	5	0	6	0	7	0	7	13
Total Survey	3	2	0	5	0	0	3	3	2	54	0	56	0	81	2	83	147

Heavy Vehicle Peak Hour Summary 4:20 PM to 5:20 PM

By		North Ten E	bound yck Rd			bound yck Rd			oound y 26		Total		
Approach	In	Out	Total	ln	Out	Total	In	Out	Total	In	Out	Total	
Volume	3	0	3	1	3	4	29	48	77	46	28	74	79
PHF	0.25			0.25			0.52			0.77			0.64

By Movement			bound yck Rd		Southbound Ten Eyck Rd				Eastbound Hwy 26				Westbound Hwy 26				Total
Wovernerit	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	1
Volume	1	2	0	3	0	0	1	1	1	28	0	29	0	46	0	46	79
PHF	0.25	0.25	0.00	0.25	0.00	0.00	0.25	0.25	0.25	0.50	0.00	0.52	0.00	0.77	0.00	0.77	0.64

Heavy Vehicle Rolling Hour Summary 4:00 PM to 6:00 PM

Interval		North	bound			South	bound			Eastk	ound						
Start		Ten E	yck Rd		Ten Eyck Rd					Hw	y 26			Interval			
Time	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	Total
4:00 PM	2	2	0	4	0	0	2	2	0	38	0	38	0	54	2	56	100
4:15 PM	1	2	0	3	0	0	1	1	1	31	0	32	0	51	1	52	88
4:30 PM	1	2	0	3	0	0	1	1	1	17	0	18	0	40	0	40	62
4:45 PM	1	0	0	1	0	0	1	1	1	15	0	16	0	34	0	34	52
5:00 PM	1	0	0	1	0	0	1	1	2	16	0	18	0	27	0	27	47

Peak Hour Summary All Traffic Data Clay Carney (503) 833-2740 Ten Eyck Rd & Hwy 26 4:20 PM to 5:20 PM Wednesday, February 19, 2020 Ten Eyck Rd Bikes 0 161 191 100 23 38 Ľ 4 Peds 2 Hwy 26 Bikes 0 16 1096 880 901 5 2 Peds 151 7 1139 854 899 134 4 Bikes 0 Hwy 26 Peds 1 **K** 1 7 7 116 Ten Eyck Rd 162 147 Bikes HV% Approach PHF Volume EΒ 0.89 2.5% 1,139 WB 0.91 5.1% 901 NB 0.75 2.0% 147 SB 0.76 0.6% 161 Intersection 0.94 3.4% 2,348 Count Period: 4:00 PM to 6:00 PM

Total Vehicle Summary

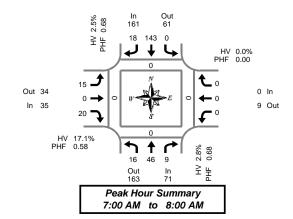


Clay Carney (503) 833-2740

Ten Eyck Rd & Pleasant St

Wednesday, February 19, 2020 7:00 AM to 9:00 AM

5-Minute Interval Summary 7:00 AM to 9:00 AM



Interval			bound			South					ound				oound					strians	
Start		Ten E	yck Rd	,		Ten Ey	/ck Rd				ant St	.,		Pleas	ant St	,	Interval			swalk	
Time	L	T	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	Total	North	South	East	West
7:00 AM	1	5	2	0	0	11	0	0	0	0	1	0	0	0	0	0	20	0	0	0	0
7:05 AM	1	2	0	0	0	15	1	0	0	0	1	0	0	0	0	0	20	0	0	0	0
7:10 AM	1	0	0	0	0	18	1	0	0	0	1	0	0	0	0	0	21	0	0	0	0
7:15 AM	2	3	1	0	0	19	4	0	0	0	2	0	0	0	0	0	31	0	0	0	0
7:20 AM	3	1	1	0	0	16	1	0	0	0	1	0	0	0	0	0	23	0	0	0	0
7:25 AM	3	4	0	0	0	11	1	0	4	0	2	0	0	0	0	0	25	0	0	0	0
7:30 AM	1	6	2	0	0	9	3	0	0	0	2	0	0	0	0	0	23	0	0	0	0
7:35 AM	1	4	0	0	0	9	2	0	4	0	3	0	0	0	0	0	23	0	0	0	0
7:40 AM	0	11	11	0	0	10	0	0	2	0	111	0	0	0	0	0	25	0	0	0	0
7:45 AM	1	3	0	0	0	13	2	0	3	0	1	0	0	0	0	0	23	0	0	0	0
7:50 AM	1	4	1	0	0	4	1	0	1	0	5	0	0	0	0	0	17	0	0	0	0
7:55 AM	1	3	11	0	0	8	2	0	11	0	0	0	0	0	0	0	16	0	0	0	0
8:00 AM	0	1	2	0	0	6	1	0	3	0	1	0	0	0	0	0	14	0	0	0	0
8:05 AM	0	2	11	0	0	6	11	0	0	0	1	0	1	0	0	0	12	0	0	0	0
8:10 AM	0	3	0	0	0	13	0	0	111	0	0	0	0	0	0	0	17	0	0	0	0
8:15 AM	0	5	1	0	0	12	2	0	1	0	2	0	0	1	0	0	24	0	0	0	0
8:20 AM	0	6	0	0	0	8	1	0	0	0	11	0	0	0	0	0	16	0	0	0	0
8:25 AM	2	3	1	0	0	13	1	0	111	0	0	0	0	0	0	0	21	0	0	0	0
8:30 AM	0	5	2	0	0	13	0	0	2	0	3	0	0	0	0	0	25	0	0	0	0
8:35 AM	0	4	0	0	0	8	0	0	0	0	0	0	1	0	0	0	13	0	0	0	0
8:40 AM	1	4	11	0	11	15	2	0	0	1	4	0	0	0	11	0	30	0	0	0	0
8:45 AM	0	6	11	0	0	11	2	0	0	0	3	0	0	0	0	0	23	0	0	0	0
8:50 AM	0	6	1	0	0	10	0	0	0	1	2	0	2	0	0	0	22	0	0	0	0
8:55 AM	0	3	0	0	0	10	0	0	0	1	1	0	0	0	0	0	15	0	0	0	0
Total Survey	19	94	19	0	1	268	28	0	23	3	38	0	4	1	1	0	499	0	0	0	0

15-Minute Interval Summary 7:00 AM to 9:00 AM

Interval Start			bound yck Rd			South Ten Ey	bound yck Rd				oound ant St				oound ant St		Interval			strians swalk	
Time	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	Total	North	South	East	West
7:00 AM	3	7	2	0	0	44	2	0	0	0	3	0	0	0	0	0	61	0	0	0	0
7:15 AM	8	8	2	0	0	46	6	0	4	0	5	0	0	0	0	0	79	0	0	0	0
7:30 AM	2	21	3	0	0	28	5	0	6	0	6	0	0	0	0	0	71	0	0	0	0
7:45 AM	3	10	2	0	0	25	5	0	5	0	6	0	0	0	0	0	56	0	0	0	0
8:00 AM	0	6	3	0	0	25	2	0	4	0	2	0	1	0	0	0	43	0	0	0	0
8:15 AM	2	14	2	0	0	33	4	0	2	0	3	0	0	1	0	0	61	0	0	0	0
8:30 AM	1	13	3	0	1	36	2	0	2	1	7	0	1	0	1	0	68	0	0	0	0
8:45 AM	0	15	2	0	0	31	2	0	0	2	6	0	2	0	0	0	60	0	0	0	0
Total Survey	19	94	19	0	1	268	28	0	23	3	38	0	4	1	1	0	499	0	0	0	0

Peak Hour Summary 7:00 AM to 8:00 AM

	By			bound yck Rd				bound yck Rd				ound ant St				oound ant St		Total
Appi	roach	In	Out	Total	Bikes	In	Out	Total	Bikes	In	Out	Total	Bikes	ln	Out	Total	Bikes	
Vol	lume	71	163	234	0	161	61	222	0	35	34	69	0	0	9	9	0	267
%	6HV		2.8	3%			2.	5%			17.	1%			0.0	0%		4.5%
P	PHF		0.	68			0.	68			0.	58			0.	00		0.84

	Pedes	trians											
Crosswalk													
North	South	East	West										
0	0	0	0										

By Movement		Northi Ten Ey	oound ck Rd				bound yck Rd				oound ant St			Westb Pleas			Total
Movement	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	
Volume	16	46	9	71	0	143	18	161	15	0	20	35	0	0	0	0	267
%HV	6.3%	2.2%	0.0%	2.8%	0.0%	1.4%	11.1%	2.5%	6.7%	0.0%	25.0%	17.1%	0.0%	0.0%	0.0%	0.0%	4.5%
PHF	0.50	0.55	0.75	0.68	0.00	0.67	0.75	0.68	0.42	0.00	0.71	0.58	0.00	0.00	0.00	0.00	0.84

Rolling Hour Summary

7:00 AM to 9:00 AM

	Interval		North	bound			South	bound			East	bound			West	oound				Pedes	trians
	Start		Ten E	yck Rd			Ten Ey	yck Rd			Pleas	sant St			Pleas	ant St		Interval		Cross	swalk
	Time	L	Т	R	Bikes	L	Т	R	Bikes	L	T	R	Bikes	L	Т	R	Bikes	Total	North	South	East
	7:00 AM	16	46	9	0	0	143	18	0	15	0	20	0	0	0	0	0	267	0	0	0
Γ.	7:15 AM	13	45	10	0	0	124	18	0	19	0	19	0	1	0	0	0	249	0	0	0
	7:30 AM	7	51	10	0	0	111	16	0	17	0	17	0	1	1	0	0	231	0	0	0
Γ.	7:45 AM	6	43	10	0	1	119	13	0	13	1	18	0	2	1	1	0	228	0	0	0
	8:00 AM	3	48	10	0	1	125	10	0	8	3	18	0	4	1	1	0	232	0	0	0

Heavy Vehicle Summary



Clay Carney (503) 833-2740

Ten Eyck Rd & Pleasant St

Wednesday, February 19, 2020 7:00 AM to 9:00 AM Out 3

In 6

Peak Hour Summary 7:00 AM to 8:00 AM

Heavy Vehicle 5-Minute Interval Summary 7:00 AM to 9:00 AM

Interval		North	bound			South	bound			Eastl	oound			Westl	oound		
Start		Ten E	yck Rd			Ten E	yck Rd			Pleas	ant St			Pleas	ant St		Interval
Time	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	L	T	R	Total	Total
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:05 AM	0	0	0	0	0	0	0	0	0	0	1	1	0	0	0	0	1
7:10 AM	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1
7:15 AM	0	0	0	0	0	0	0	0	0	0	1	1	0	0	0	0	1
7:20 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:25 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	1	0	1	0	0	1	1	0	0	0	0	0	0	0	0	2
7:35 AM	0	0	0	0	0	1	1	2	1	0	1	2	0	0	0	0	4
7:40 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	1	0	1	0	0	1	1	0	0	0	0	2
7:50 AM	0	0	0	0	0	0	0	0	0	0	1	1	0	0	0	0	1
7:55 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	1	0	1	1	0	0	1	0	0	0	0	2
8:05 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:10 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	2	2	1	0	0	1	0	0	0	0	3
8:20 AM	0	1	0	11	0	0	0	0	0	0	0	0	0	0	0	0	1
8:25 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	1	0	1	0	1	0	1	0	0	1	1	0	0	0	0	3
8:35 AM	0	1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1
8:40 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:50 AM	0	0	0	0	0	2	0	2	0	0	0	0	0	0	0	0	2
8:55 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total Survey	1	4	0	5	0	6	4	10	3	0	6	9	0	0	0	0	24

Heavy Vehicle 15-Minute Interval Summary 7:00 AM to 9:00 AM

Interval			bound				bound				ound				oound		
Start		Ten E	yck Rd			Ten E	yck Rd			Pleas	ant St			Pleas	ant St		Interval
Time	L	T	R	Total	∟	T	R	Total	LI.	T	R	Total	١	T	R	Total	Total
7:00 AM	1	0	0	1	0	0	0	0	0	0	1	1	0	0	0	0	2
7:15 AM	0	0	0	0	0	0	0	0	0	0	1	1	0	0	0	0	1
7:30 AM	0	1	0	1	0	1	2	3	1	0	1	2	0	0	0	0	6
7:45 AM	0	0	0	0	0	1	0	1	0	0	2	2	0	0	0	0	3
8:00 AM	0	0	0	0	0	1	0	1	1	0	0	1	0	0	0	0	2
8:15 AM	0	1	0	1	0	0	2	2	1	0	0	1	0	0	0	0	4
8:30 AM	0	2	0	2	0	1	0	1	0	0	1	1	0	0	0	0	4
8:45 AM	0	0	0	0	0	2	0	2	0	0	0	0	0	0	0	0	2
Total Survey	1	4	0	5	0	6	4	10	3	0	6	9	0	0	0	0	24

Heavy Vehicle Peak Hour Summary 7:00 AM to 8:00 AM

By			bound yck Rd			bound yck Rd			oound ant St			bound sant St	Total
Approach	In	Out	Total	In	Out	Total	In	Out	Total	ln	Out	Total	
Volume	2	7	9	4	2	6	6	3	9	0	0	0	12
PHF	0.50			0.33			0.50			0.00			0.50

By Movement			bound yck Rd				bound yck Rd				oound ant St			Westl Pleas			Total
Wovement	L	Т	R	Total	∟	T	R	Total	١	T	R	Total	L	Т	R	Total	
Volume	1	1	0	2	0	2	2	4	1	0	5	6	0	0	0	0	12
PHF	0.25	0.25	0.00	0.50	0.00	0.25	0.25	0.33	0.25	0.00	0.63	0.50	0.00	0.00	0.00	0.00	0.50

Heavy Vehicle Rolling Hour Summary 7:00 AM to 9:00 AM

Interval Start		North Ten E	bound yck Rd				bound yck Rd				oound ant St			Westl Pleas	oound ant St		Interval
Time	L	Т	R	Total	L	T	R	Total	L	Т	R	Total	L	Т	R	Total	Total
7:00 AM	1	1	0	2	0	2	2	4	1	0	5	6	0	0	0	0	12
7:15 AM	0	1	0	1	0	3	2	5	2	0	4	6	0	0	0	0	12
7:30 AM	0	2	0	2	0	3	4	7	3	0	3	6	0	0	0	0	15
7:45 AM	0	3	0	3	0	3	2	5	2	0	3	5	0	0	0	0	13
8:00 AM	0	3	0	3	0	4	2	6	2	0	1	3	0	0	0	0	12

Peak Hour Summary All Traffic Data Clay Carney (503) 833-2740 Ten Eyck Rd & Pleasant St 7:00 AM to 8:00 AM Wednesday, February 19, 2020 Ten Eyck Rd **Bikes** 0 161 61 18 143 0 Ľ Peds 0 Pleasant St Bikes 0 0 34 0 0 0 0 15 0 9 20 4 Bikes 0 Pleasant St Peds 0 **K** 1 7 16 46 9 Ten Eyck Rd 163 71 Bikes HV% Approach PHF Volume EΒ 0.58 17.1% WB 0.00 0.0% 0 71 NB 0.68 2.8% SB 0.68 2.5% 161 Intersection 0.84 4.5% 267 Count Period: 7:00 AM to 9:00 AM

Total Vehicle Summary

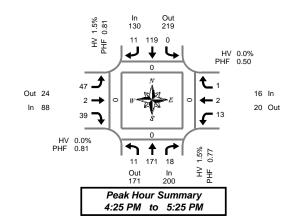


Clay Carney (503) 833-2740

Ten Eyck Rd & Pleasant St

Wednesday, February 19, 2020 4:00 PM to 6:00 PM

5-Minute Interval Summary 4:00 PM to 6:00 PM



Interval		Northi					bound			Eastl	ound			West	oound				Pedes	trians	
Start		Ten Ey	yck Rd			Ten E	yck Rd			Pleas	ant St			Pleas	ant St		Interval		Cross	swalk	
Time	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	Total	North	South	East	West
4:00 PM	0	9	1	0	0	9	1	0	2	0	4	0	2	0	0	0	28	0	0	0	0
4:05 PM	1	20	2	0	0	5	2	0	1	0	2	0	0	2	2	0	37	0	0	0	0
4:10 PM	1	10	2	0	0	7	2	0	5	0	3	0	1	0	1	0	32	0	0	0	0
4:15 PM	2	11	1	0	0	8	0	0	4	11	11	0	0	2	0	0	30	0	0	0	0
4:20 PM	1	9	2	0	0	7	0	0	2	1	1	0	0	1	0	0	24	0	0	0	0
4:25 PM	0	11	0	0	0	8	0	0	7	0	4	0	1	0	0	0	31	0	0	0	0
4:30 PM	1	14	1	0	0	7	0	0	5	0	3	0	0	0	0	0	31	0	0	0	0
4:35 PM	1	16	3	0	0	12	0	0	4	0	11	0	0	0	0	0	37	0	0	0	0
4:40 PM	0	22	1	0	0	6	4	0	11	0	2	0	1	0	0	0	37	0	0	0	0
4:45 PM	4	17	1	0	0	9	0	0	5	0	11	0	2	0	1	0	40	0	0	0	0
4:50 PM	1	12	2	0	0	18	0	0	3	0	6	0	2	2	0	0	46	0	0	0	0
4:55 PM	0	11	0	0	0	10	2	0	3	0	5	0	0	0	0	0	31	0	0	0	0
5:00 PM	0	19	1	0	0	10	0	0	4	1	5	0	1	0	0	0	41	0	0	0	0
5:05 PM	1	12	4	0	0	14	2	0	5	0	4	0	0	0	0	0	42	0	0	0	0
5:10 PM	0	14	2	0	0	10	3	0	3	0	3	0	3	0	0	0	38	0	0	0	0
5:15 PM	2	9	1	0	0	6	0	0	3	1	3	0	0	0	0	0	25	0	0	0	0
5:20 PM	1	14	2	0	0	9	0	0	4	0	2	0	3	0	0	0	35	0	0	0	0
5:25 PM	0	14	0	0	0	7	1	0	11	0	2	0	0	0	0	0	25	0	0	0	0
5:30 PM	0	17	1	0	0	12	0	0	2	0	11	0	0	0	0	0	33	0	0	0	0
5:35 PM	0	14	2	0	0	4	0	0	3	0	2	0	2	0	0	0	27	0	0	0	0
5:40 PM	1	16	2	0	1	10	0	0	11	0	4	0	1	0	0	0	36	0	0	0	0
5:45 PM	0	12	1	0	0	8	1	0	2	0	1	0	0	0	0	0	25	0	0	0	0
5:50 PM	0	12	2	0	0	8	1	0	1	0	4	0	1	1	1	0	31	0	0	0	0
5:55 PM	0	13	2	0	0	7	1	0	3	0	4	0	1	0	0	0	31	0	0	0	0
Total Survey	17	328	36	0	1	211	20	0	74	4	68	0	21	8	5	0	793	0	0	0	0

15-Minute Interval Summary 4:00 PM to 6:00 PM

Interval Start			bound yck Rd				bound yck Rd				oound ant St				bound ant St		Interval			strians swalk	
Time	L	Т	R	Bikes	L	Т	R	Bikes	L	T	R	Bikes	L	Т	R	Bikes	Total	North	South	East	West
4:00 PM	2	39	5	0	0	21	5	0	8	0	9	0	3	2	3	0	97	0	0	0	0
4:15 PM	3	31	3	0	0	23	0	0	13	2	6	0	1	3	0	0	85	0	0	0	0
4:30 PM	2	52	5	0	0	25	4	0	10	0	6	0	1	0	0	0	105	0	0	0	0
4:45 PM	5	40	3	0	0	37	2	0	11	0	12	0	4	2	1	0	117	0	0	0	0
5:00 PM	1	45	7	0	0	34	5	0	12	1	12	0	4	0	0	0	121	0	0	0	0
5:15 PM	3	37	3	0	0	22	1	0	8	1	7	0	3	0	0	0	85	0	0	0	0
5:30 PM	1	47	5	0	1	26	0	0	6	0	7	0	3	0	0	0	96	0	0	0	0
5:45 PM	0	37	5	0	0	23	3	0	6	0	9	0	2	1	1	0	87	0	0	0	0
Total Survey	17	328	36	0	1	211	20	0	74	4	68	0	21	8	5	0	793	0	0	0	0

Peak Hour Summary 4:25 PM to 5:25 PM

Ву		North Ten E	oound ck Rd				bound yck Rd				ound ant St				oound ant St		Total
Approach	In	Out	Total	Bikes	In	Out	Total	Bikes	In	Out	Total	Bikes	In	Out	Total	Bikes	
Volume	200	171	371	0	130	219	349	0	88	24	112	0	16	20	36	0	434
%HV		200 171 371 0 1.5%				1.5	5%			0.0)%			0.0	0%		1.2%
PHF						0.	81			0.	31			0.	50		0.88

	reues	ulalis	
	Cross	swalk	
North	South	East	West
0	0	0	0

By Movement		Northi Ten Ey	bound yck Rd				bound yck Rd			Eastb Pleas	ound ant St			Westl Pleas	oound ant St		Total
Movement	١	Т	R	Total	∟	T	R	Total	L	T	R	Total	L	T	R	Total	
Volume	11	171	18	200	0	119	11	130	47	2	39	88	13	2	1	16	434
%HV	0.0%	1.8%	0.0%	1.5%	0.0%	0.8%	9.1%	1.5%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	1.2%
PHF	0.55	0.78	0.64	0.77	0.00	0.78	0.55	0.81	0.73	0.50	0.61	0.81	0.54	0.25	0.25	0.50	0.88

Rolling Hour Summary 4:00 PM to 6:00 PM

Interval		North	oound			South	bound			Eastl	ound			Westl	bound				Pedes	trians	
Start		Ten Ey	ck Rd			Ten E	yck Rd			Pleas	ant St			Pleas	ant St		Interval		Cross	swalk	
Time	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	L	Т	R	Bikes	Total	North	South	East	West
4:00 PM	12	162	16	0	0	106	11	0	42	2	33	0	9	7	4	0	404	0	0	0	0
4:15 PM	11	168	18	0	0	119	11	0	46	3	36	0	10	5	1	0	428	0	0	0	0
4:30 PM	11	174	18	0	0	118	12	0	41	2	37	0	12	2	1	0	428	0	0	0	0
4:45 PM	10	169	18	0	1	119	8	0	37	2	38	0	14	2	1	0	419	0	0	0	0
5:00 PM	5	166	20	0	1	105	9	0	32	2	35	0	12	1	1	0	389	0	0	0	0

Heavy Vehicle Summary



Clay Carney (503) 833-2740

Ten Eyck Rd & Pleasant St

Wednesday, February 19, 2020 4:00 PM to 6:00 PM

Peak Hour Summary 4:25 PM to 5:25 PM

Out

Out 1

In 0

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Heavy Vehicle 5-Minute Interval Summary 4:00 PM to 6:00 PM

Interval			bound				bound				ound				bound		
Start			yck Rd	,			yck Rd	,			ant St	,			ant St	,	Interval
Time	L	Т	R	Total	Total												
4:00 PM	0	1	0	1	0	3	0	3	0	0	0	0	0	0	0	0	4
4:05 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:10 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	1	0	1	0	0	0	0	0	0	0	0	1
4:20 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:25 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	2	0	2	0	0	0	0	0	0	0	0	0	0	0	0	2
4:35 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:40 PM	0	0	0	0	0	0	1	11	0	0	0	0	0	0	0	0	11
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:50 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:55 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1
5:05 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:10 PM	0	0	0	0	0	1	0	1	0	0	0	0	0	0	0	0	11
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:20 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:25 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:35 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:40 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1
5:50 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:55 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total Survey	0	5	0	5	0	5	1	6	0	0	0	0	0	0	0	0	11

Heavy Vehicle 15-Minute Interval Summary 4:00 PM to 6:00 PM

Interval			bound				bound				ound				oound		
Start		Ten E	yck Rd			Ten E	yck Rd			Pleas	ant St			Pleas	ant St		Interval
Time	L	T	R	Total	∟	T	R	Total	LI.	Т	R	Total	١	T	R	Total	Total
4:00 PM	0	1	0	1	0	3	0	3	0	0	0	0	0	0	0	0	4
4:15 PM	0	0	0	0	0	1	0	1	0	0	0	0	0	0	0	0	1
4:30 PM	0	2	0	2	0	0	1	1	0	0	0	0	0	0	0	0	3
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	1	0	1	0	1	0	1	0	0	0	0	0	0	0	0	2
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1
Total Survey	0	5	0	5	0	5	1	6	0	0	0	0	0	0	0	0	11

Heavy Vehicle Peak Hour Summary 4:25 PM to 5:25 PM

By			bound yck Rd			bound yck Rd			oound ant St			bound ant St	Total
Approach	In	Out	Total	In	Out	Total	In	Out	Total	In	Out	Total	
Volume	3	1	4	2	3	5	0	1	1	0	0	0	5
PHF	0.38			0.50			0.00			0.00			0.42

By Movement			bound yck Rd				bound yck Rd				ound ant St			West! Pleas	oound ant St		Total
Movement	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	L	Т	R	Total	
Volume	0	3	0	3	0	1	. 1	2	0	0	0	0	0	0	0	0	5
PHF	0.00	0.38	0.00	0.38	0.00	0.25	0.25	0.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.42

Heavy Vehicle Rolling Hour Summary 4:00 PM to 6:00 PM

4.00 i iii			•														
Interval		North	bound			South	bound			Eastl	ound			West	bound		
Start		Ten E	yck Rd			Ten E	yck Rd			Pleas	ant St			Pleas	ant St		Interval
Time	L	Т	R	Total	L	T	R	Total	L	Т	R	Total	L	Т	R	Total	Total
4:00 PM	0	3	0	3	0	4	1	5	0	0	0	0	0	0	0	0	8
4:15 PM	0	3	0	3	0	2	1	3	0	0	0	0	0	0	0	0	6
4:30 PM	0	3	0	3	0	1	1	2	0	0	0	0	0	0	0	0	5
4:45 PM	0	1	0	1	0	1	0	1	0	0	0	0	0	0	0	0	2
5:00 PM	0	2	0	2	0	1	0	1	0	0	0	0	0	0	0	0	3

Peak Hour Summary All Traffic Data Clay Carney (503) 833-2740 Ten Eyck Rd & Pleasant St 4:25 PM to 5:25 PM Wednesday, February 19, 2020 Ten Eyck Rd **Bikes** 0 130 219 11 119 0 Ľ Peds 0 Pleasant St Bikes 0 1 24 2 16 13 0 47 2 20 39 4 Bikes 0 Pleasant St Peds 0 **K** 1 7 11 171 18 Ten Eyck Rd 171 200 Bikes HV% Approach PHF Volume EΒ 0.81 0.0% WB 0.50 0.0% 16 200 NB 0.77 1.5% SB 0.81 1.5% 130 Intersection 1.2% 434 Count Period: 4:00 PM to 6:00 PM

Mt. H	ood Highway No. 26 (US 26)				ODOT TV	/T Data		
MP	Location		2013	2014	2015	2016	2017	2018
24.5	59 EB, just west of Ten Eyck Rd		12,500	12,600	11,200	11,500	11,400	12,500
24.6	61 WB, just west of Ten Eyck Rd		11,600	11,700	11,700	12,100	12,000	12,600
25.1	10 EB+WB, just west of Langensa	nd Rd	16,900	17,100	18,000	18,500	18,400	20,700
		Totals	41,000	41,400	40,900	42,100	41,800	45,800
	Annual Growth from 2013	r	n/a	1.0%	-0.1%	0.9%	0.5%	2.3%

SEASONAL TREND TABLE (Upo	lated: 6/26/	19)		Sacanal Trans
TREND	1-Feb	15-Feb	1-Mar	Seasonal Trend Peak Period Factor
COMMUTER	1.08	1.06	1.04	0.94
RECREATIONAL SUMMER WINTER	1.02	1.04	1.05	0.70
SUMMER	1.24	1.21	1.15	0.83

^{*}Seasonal Trend Table factors are based on previous year ATR data. The table is updated yearly. *Grey shading indicates months were seasonal factor is greater than 30%.

Commuter, Recreational Summer-Winter, & Summer	1.11 1.34	0.83	<< Over 30%, so too high to be used
Commuter & Summer	1.14 1.28	0.89	<< This is an approved blend of trends, so this one is used.
Recreational Summer-Winter only	1.04 1.49	0.70	<< Over 30%, so too high to be used
Commuter & Recreational Summer-Winter	1.05 1.28	0.82	<< This is not an approved blend of trends, but it validates the number used above.

Appendix BTrip Generation Calculations

Detailed Land Use Data

For 9.6 1000 Sq. Ft. GFA of CLINIC 1 (630) Clinic

Project: Sandy Medical Clinic

Open Date: 3/3/2020 Analysis Date: 3/3/2020

Day / Period	Total Trips	Pass-By Trips	Avg Rate	Min Rate	Max Rate	Std Dev	Avg Size	% Enter	% Exit	Use Eq.	Equation	
Weekday Average Daily Trips Source: Trip Generation Manual 10th Edition	366	0	38.16	25.25	86.21	30.18	21	50	50	False		
Weekday AM Peak Hour of Adjacent Street Traffic Source: Trip Generation Manual 10th Edition	35	0	3.69	2.27	9.36	2.82	21	78	22	False		
Weekday PM Peak Hour of Adjacent Street Traffic Source: Trip Generation Manual 10th Edition	31	0	3.28	1.93	7	1.84	18	29	71	False	Ln(T) = 0.72 Ln(X) + 1.97	0.7

Detailed Land Use Data

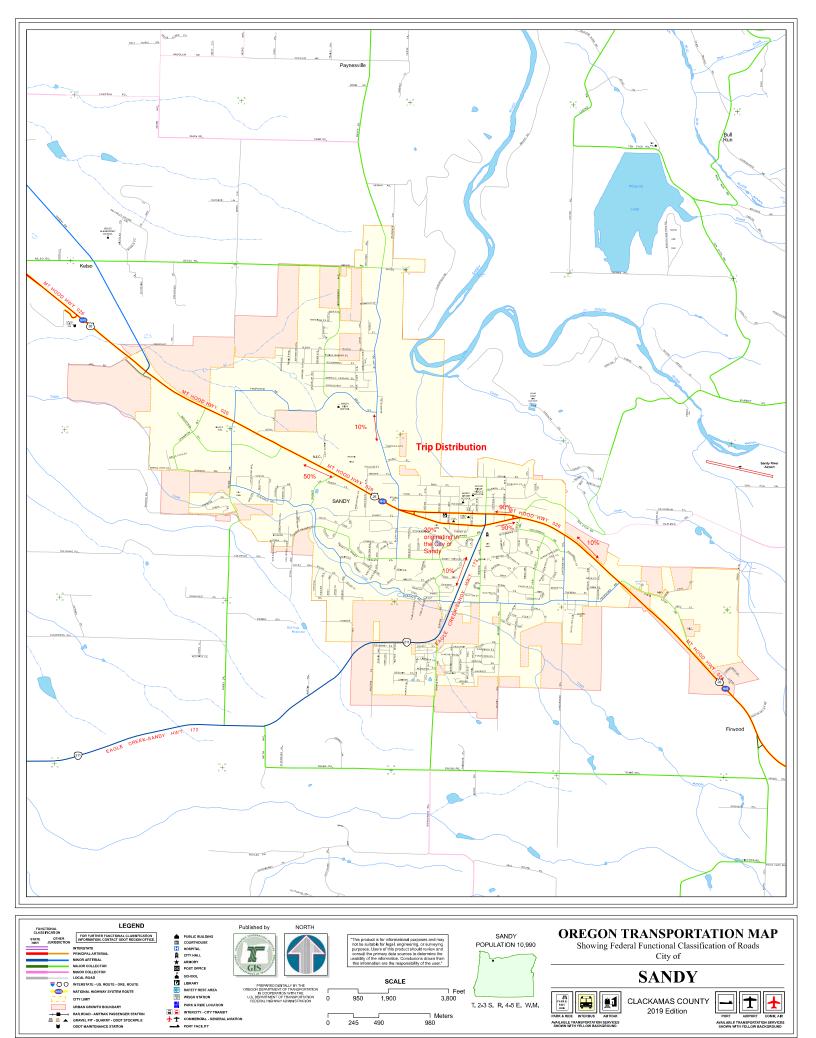
For 6.3 1000 Sq. Ft. GFA of WAREHOUSE 1 (150) Warehousing

Project: Sandy Medical Clinic

Open Date: 3/3/2020

Analysis Date: 3/3/2020

Day / Period	Total Trips	Pass-By Trips	Avg Rate	Min Rate	Max Rate	Std Dev	Avg Size	% Enter	% Exit	Use Eq.	Equation	R2
Weekday Average Daily Trips Source: Trip Generation Manual 10th Edition	11	0	1.74	0.15	16.93	1.55	285	50	50	False	T = 1.58(X) + 45.54	0.93
Weekday AM Peak Hour of Adjacent Street Traffic	1	0	0.17	0.02	1.93	0.2	451	77	23	False	T = 0.12(X) + 25.32	0.69
Source: Trip Generation Manual 10th Edition Weekday PM Peak Hour of Adjacent Street Traffic	1	0	0.19	0.01	1.8	0.18	400	27	73	False	T = 0.12(X) + 27.82	0.65
Source: Trip Generation Manual 10th Edition												



John A. Manix

From: Wilson, James <jwilson2@clackamas.us>
Sent: Tuesday, February 18, 2020 3:18 PM

To: John A. Manix

Cc: Cockrell, Deborah; Kelly, Steve

Subject: RE: PBS Engineers - Traffic Study Question(s)

Hi John

Here are estimates for staff members:

25% trips originate from within the City limits of Sandy 50% trips originate from the west of Sandy 8% trips originate from the north of Sandy 8% trips originate from the east of Sandy 9% trips originate from the south of Sandy

James

From: John A. Manix < Manix@pbsusa.com>
Sent: Tuesday, February 18, 2020 10:52 AM
To: Wilson, James < jwilson2@clackamas.us>

Cc: Cockrell, Deborah <DCockrell@clackamas.us>; Kelly, Steve <SteveKel@clackamas.us>

Subject: RE: PBS Engineers - Traffic Study Question(s)

James: This is good. Thank you

I will assume that the origin of staff trips will be about the same. If you have anything similar for staff trips that will be helpful.

John Manix, PE | Senior Traffic Engineer | PBS Vancouver | 360.607.1854 (cell)

From: Wilson, James < <u>iwilson2@clackamas.us</u>>
Sent: Tuesday, February 18, 2020 10:36 AM
To: John A. Manix < <u>Manix@pbsusa.com</u>>

Cc: Cockrell, Deborah < DCockrell@clackamas.us >; Kelly, Steve < SteveKel@clackamas.us >

Subject: RE: PBS Engineers - Traffic Study Question(s)

Hi John

Here are estimates of where patients and clients of the new clinic will originate.

These are based on current patient demographics, information from the Health Resources and Services Administration (HRSA), and information from Medicaid / Oregon Health Plan insurance networks.

If you need anything more, please let me know.

45% trips originate from within the City limits of Sandy 8% trips originate from the west of Sandy (Kelso, Boring)

5% trips originate from the north of Sandy

12% trips originate from the east of Sandy (Mt Hood Village, and Mountain Communities)

30% trips originate from the south of Sandy (Estacada / Eagle Creek)

Have a great morning

James

JAMES WILSON CHIEF OPERATIONS OFFICER CLACKAMAS HEALTH CENTERS 503-655-8697

EXCEPTIONAL CARE FOR THE WHOLE PERSON DELIVERED WITH DIGNITY AND RESPECT FOR ALL.

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From: Cockrell, Deborah < DCockrell@clackamas.us>

Sent: Tuesday, February 18, 2020 9:30 AM **To:** Wilson, James <jwilson2@clackamas.us>

Subject: FW: PBS Engineers - Traffic Study Question(s)

FYI data needed

From: John A. Manix [mailto:Manix@pbsusa.com]
Sent: Tuesday, February 18, 2020 8:39 AM
To: Cockrell, Deborah < DCockrell@clackamas.us>
Subject: RE: PBS Engineers - Traffic Study Question(s)

Deborah: I understand the data will not be easy to produce. If you or the staff can give me a rough estimate of the origin of patrons and/or staff, I would appreciate the effort. It would be best to revise my estimate below in the February 13, 2020 email.

John Manix, PE | Senior Traffic Engineer | PBS Vancouver | 360.607.1854 (cell)

From: Cockrell, Deborah < DCockrell@clackamas.us>

Sent: Monday, February 17, 2020 12:42 PM
To: John A. Manix < Manix@pbsusa.com>

Cc: Kelly, Steve < SteveKel@clackamas.us; Wilson, James < jwilson2@clackamas.us;

Subject: RE: PBS Engineers - Traffic Study Question(s)

Unfortunately this data will not be easy to produce. We will have to survey staff. JAMES: Can you pull this data for us? Also, dental is the only new traffic. BH and PC already have a presence in Sandy

From: John A. Mani]

Sent: Thursday, February 13, 2020 8:59 AM
To: Cockrell, Deborah < DCockrell@clackamas.us>
Cc: Kelly, Steve < SteveKel@clackamas.us>

Subject: RE: PBS Engineers - Traffic Study Question(s)

Deborah: Thank you. This is good information but more important is the were in the community do the trips to your clinic come from. Please edit my estimate below based on your experience.

For example do most patients and staff live in the Sandy or do they live north, east, west or south of town. This is not an exact process but based on residential density and my experience with the community, here is my estimate:

50% trips originate from within the City limits of Sandy,

10% trips originate from the west of Sandy

10% trips originate from the north of Sandy

20% trips originate from the east of Sandy

10% trips originate from the south of Sandy

For the proposed clinic at Hwy 26 and Ten Eyke Road, I need to know which direction the staff and patience approach the clinic. Feel free to call if you have questions.

Thanks

John Manix, PE

Senior Traffic Engineer

PBS

415 W 6th St., Suite 601, Vancouver, WA 98660 office: 360.695.3488 | direct: 360.567.2117 | cell: 360.607.1854 john.manix@pbsusa.com pbsusa.com



From: Kelly, Steve < Sent: Wednesday, February 12, 2020 1:20 PM To: John A. Manix < Manix@pbsusa.com>

Subject: FW: PBS Engineers - Traffic Study Question(s)

John,

Here is what I got from the Director of all of County Health Clinics. See below, sir.

Steve Kelly, Project Coordinator Clackamas County Community Development 2051 Kaen Road, Suite 245 Oregon City, OR 97045

503 . 650 . 5665 stevekel@clackamas.us

From: Cockrell, Deborah < <u>DCockrell@clackamas.us</u>>

Sent: Tuesday, February 11, 2020 1:08 PM To: Kelly, Steve < SteveKel@clackamas.us>

Subject: RE: PBS Engineers - Traffic Study Question(s)

MD will see 18 people per day, 4 days a week. DMD will see 14 people per day, 4 days a week. Probably 40 people per day for the therapists.

From: Kelly, Steve

Sent: Tuesday, February 11, 2020 11:33 AM

To: Cockrell, Deborah < DCockrell@clackamas.us Subject: PBS Engineers - Traffic Study Question(s)

Importance: High

John Manix of PBS.

Wants to know if we have information of any kind that determines visitors (patients) that are driven to the sites in Sandy. He would need them if they are available for counts for vehicular usage to both clinic sites presently (high school and other location). I am assuming someone else has these numbers or data.
He is getting me a letter with a price today he said. I will provide him our Professional Services Contract and use his letter as an Exhibit A.
Thanks.
Steve Kelly, Project Coordinator Clackamas County Community Development 2051 Kaen Road, Suite 245 Oregon City, OR 97045
503 . 650 . 5665

stevekel@clackamas.us

NOTE: This message was trained as non-spam. If this is wrong, please correct the training as soon as possible.

Appendix CLevel of Service Calculations

Critical Intersection Volume-to-Capacity Ratio							
Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)							
2020 Existing Conditions	Weekday AM Peak Hour						

	EB		WB		NB	SB
Lane Group	EBL	EBT	WBL	WBTR	NBLTR	SBLTR
Adj Flow Rate (veh/h)	59	904	0	1034	152	69
Sat Flow (veh/h)	1589	2988	1667	3269	1469	1618
Critical Flow Ratios	0.04	1 0.30	0.00	0.32	0.10	0.04
	critical			critical	critical	

Cycle Length
Lost Time per Phase
Total Lost Time

64.4 seconds
4 seconds
12 seconds

Critical Intersection V/C Ratio: 0.56

Method follows ODOT Analysis Procedures Manual, Version 2, Chapter 13.4.4.

Critical Intersection Volume-to-Capacity Ratio							
Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)							
2022 Without Project	Weekday AM Peak Hour						

	EB			WB			NB	SB
Lane Group	EBL	EBT		WBL		WBTR	NBLTR	SBLTR
Adj Flow Rate (veh/h)		61	940		0	1076	157	70
Sat Flow (veh/h)		1589	2988		1641	3269	1444	1593
Critical Flow Ratios		0.04	0.31		0.00	0.33	0.11	0.04
	critica	l				critical	critical	

Sum of Critical Flow Ratios 0.48

Cycle Length 69.3 seconds
Lost Time per Phase 4 seconds
Total Lost Time 12 seconds

Critical Intersection V/C Ratio: 0.58

Critical Intersection Volume-	to-Capacity Ratio
Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)	
2022 With Project Trips	Weekday AM Peak Hour

	EB			WB			NB	SB
Lane Group	EBL	EBT		WBL		WBTR	NBLTR	SBLTR
Adj Flow Rate (veh/h)		87	940		0	1080	157	73
Sat Flow (veh/h)	15	89	2988		1641	3267	1447	1595
Critical Flow Ratios	0	.05	0.31		0.00	0.33	0.11	0.05
	critical					critical	critical	

Cycle Length 71.7 seconds
Lost Time per Phase 4 seconds
Total Lost Time 12 seconds

Critical Intersection V/C Ratio: 0.59

Method follows ODOT Analysis Procedures Manual, Version 2, Chapter 13.4.4.

Critical Intersection Volume-to-Capacity Ratio							
Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)							
2029 Without Project	Weekday AM Peak Hour						

	EB		V	VB		NB	SB
Lane Group	EBL	EBT	V	VBL	WBTR	NBLTR	SBLTR
Adj Flow Rate (veh/h)		70	1067	0	1222	179	75
Sat Flow (veh/h)		1589	2988	1641	3268	1438	1604
Critical Flow Ratios		0.04	0.36	0.00	0.37	0.12	0.05
	critica	1			critical	critical	

Sum of Critical Flow Ratios 0.54

Cycle Length 76.8 seconds
Lost Time per Phase 4 seconds
Total Lost Time 12 seconds

Critical Intersection V/C Ratio: 0.64

Critical Intersection Volume-to-Capacity Ratio					
Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)					
2029 With Project Trips	Weekday AM Peak Hour				

	EB			WB			NB	SB
Lane Group	EBL	EBT		WBL	,	WBTR	NBLTR	SBLTR
Adj Flow Rate (veh/h)		96	1067		0	1225	179	76
Sat Flow (veh/h)	1	589	2988		1641	3266	1439	1606
Critical Flow Ratios		0.06	0.36		0.00	0.38	0.12	0.05
	critical					critical	critical	

Cycle Length 78.3 seconds
Lost Time per Phase 4 seconds
Total Lost Time 12 seconds

Critical Intersection V/C Ratio: 0.66

Method follows ODOT Analysis Procedures Manual, Version 2, Chapter 13.4.4.

Critical Intersection Volume-to-Capacity Ratio				
Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)				
2029 With Project Trips with WB Right-Turn Lane	Weekday AM Peak Hour			

	EB		WB		NB	SB
Lane Group	EBL	EBT	WBL	WBT	NBLTR	SBLTR
Adj Flow Rate (veh/h)	90	5 1067	7 (1202	179	78
Sat Flow (veh/h)	1589	9 2988	1641	3195	1440	1604
Critical Flow Ratios	0.0	5 0.36	0.00	0.38	0.12	0.05
	critical			critical	critical	

Sum of Critical Flow Ratios 0.56

Cycle Length 77.3 seconds
Lost Time per Phase 4 seconds
Total Lost Time 12 seconds

Critical Intersection V/C Ratio: 0.66

Critical Intersection Volume-to-Capacity Ratio					
Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)					
2020 Existing Conditions	Weekday PM Peak Hour				

	EB		WB		NB	SB
Lane Group	EBL	EBT	WBL	WBTR	NBLTR	SBLTR
Adj Flow Rate (veh/h)	161	1165	5	1216	154	114
Sat Flow (veh/h)	1654	3247	1667	3272	1219	1587
Critical Flow Ratios	0.10	0.36	0.00	0.37	0.13	0.07
	critical			critical	critical	

Cycle Length 110 seconds
Lost Time per Phase 4 seconds
Total Lost Time 12 seconds

Critical Intersection V/C Ratio: 0.67

Method follows ODOT Analysis Procedures Manual, Version 2, Chapter 13.4.4.

Critical Intersection Volume-to-Capacity Ratio					
Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)					
2022 Without Project	Weekday PM Peak Hour				

	EB		WB		NB	SB
Lane Group	EBL	EBT	WBL	WBTR	NBLTR	SBLTR
Adj Flow Rate (veh/h)	167	1212	5	1265	161	127
Sat Flow (veh/h)	1641	3247	1641	3271	1174	1575
Critical Flow Ratios	0.10	0.37	0.00	0.39	0.14	0.08
	critical			critical	critical	

Sum of Critical Flow Ratios 0.63

Cycle Length 110 seconds
Lost Time per Phase 4 seconds
Total Lost Time 12 seconds

Critical Intersection V/C Ratio: 0.70

Critical Intersection Volume-to-Capacity Ratio					
Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)					
2022 With Project Trips	Weekday PM Peak Hour				

	EB		WB			NB	SB
Lane Group	EBL	EBT	WBL	WBT	R	NBLTR	SBLTR
Adj Flow Rate (veh/h)	17	6 12	12	5	1266	161	143
Sat Flow (veh/h)	164	.1 32	47	1641	3270	1121	1577
Critical Flow Ratios	0.1	1 0.	37	0.00	0.39	0.14	0.09
	critical			critic	al	critical	

Cycle Length 110 seconds
Lost Time per Phase 4 seconds
Total Lost Time 12 seconds

Critical Intersection V/C Ratio: 0.72

Method follows ODOT Analysis Procedures Manual, Version 2, Chapter 13.4.4.

Critical Intersection Volume-to-Capacity Ratio				
Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)				
2029 Without Project	Weekday PM Peak Hour			

	EB			WB			NB	SB
Lane Group	EBL	EBT		WBL		WBTR	NBLTR	SBLTR
Adj Flow Rate (veh/h)	18	9	1374		6	1435	183	149
Sat Flow (veh/h)	164	1	3247		1641	3271	1119	1578
Critical Flow Ratios	0.1	2	0.42		0.00	0.44	0.16	0.09
	critical					critical	critical	

Sum of Critical Flow Ratios 0.72

Cycle Length 110 seconds
Lost Time per Phase 4 seconds
Total Lost Time 12 seconds

Critical Intersection V/C Ratio: 0.81

Critical Intersection Volume-	to-Capacity Ratio
Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)	
2029 With Project Trips	Weekday PM Peak Hour

	EB		WB			NB	SB
Lane Group	EBL	EBT	WBL	,	WBTR	NBLTR	SBLTR
Adj Flow Rate (veh/h)	19	8 1	1374	6	1436	183	163
Sat Flow (veh/h)	163	0 3	3228	1630	3160	1065	1587
Critical Flow Ratios	0.1	2	0.43	0.00	0.45	0.17	0.10
	critical				critical	critical	

Cycle Length 110 seconds
Lost Time per Phase 4 seconds
Total Lost Time 12 seconds

Critical Intersection V/C Ratio: 0.84

Method follows ODOT Analysis Procedures Manual, Version 2, Chapter 13.4.4.

Critical Intersection Volume-	to-Capacity Ratio
Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)	
2029 With Project Trips with WB Right-Turn Lane	Weekday PM Peak Hour

	EB	WB	3	Ν	В	SB
Lane Group	EBL E	EBT WB	BL WBT	N	BLTR	SBLTR
Adj Flow Rate (veh/h)	198	1374	6	1416	183	163
Sat Flow (veh/h)	1641	3247	1641	3195	1065	1587
Critical Flow Ratios	0.12	0.42	0.00	0.44	0.17	0.10
	critical		critico	al cr	ritical	

Sum of Critical Flow Ratios 0.74

Cycle Length 110 seconds
Lost Time per Phase 4 seconds
Total Lost Time 12 seconds

Critical Intersection V/C Ratio: 0.83

	ၨ	→	•	•	←	•	•	†	/	>	ţ	1
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	ň	∱ }			4			4	
Traffic Volume (vph)	54	832	33	0	937	16	136	3	2	21	7	135
Future Volume (vph)	54	832	33	0	937	16	136	3	2	21	7	135
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Storage Length (ft)	115		100	105		0	0		0	0		0
Storage Lanes	1		1	1		0	0		0	0		0
Taper Length (ft)	100			100			100			100		
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor			0.98		1.00			1.00			0.99	
Frt			0.850		0.998			0.998			0.889	
Flt Protected	0.950							0.954			0.994	
Satd. Flow (prot)	1568	2942	1403	1750	3162	0	0	1604	0	0	1458	0
Flt Permitted	0.950							0.592			0.953	
Satd. Flow (perm)	1568	2942	1372	1750	3162	0	0	994	0	0	1398	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)			77		2			1			147	
Link Speed (mph)		25			25			25			25	
Link Distance (ft)		468			302			365			210	
Travel Time (s)		12.8			8.2			10.0			5.7	
Confl. Peds. (#/hr)			1	1			2					2
Confl. Bikes (#/hr)						1						
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	13%	6%	0%	5%	0%	4%	0%	0%	24%	0%	2%
Adj. Flow (vph)	59	904	36	0	1018	17	148	3	2	23	8	147
Shared Lane Traffic (%)												
Lane Group Flow (vph)	59	904	36	0	1035	0	0	153	0	0	178	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA
Median Width(ft)		12			12			0			0	
Link Offset(ft)		-12			0			0			4	
Crosswalk Width(ft)		72			42			32			30	
Two way Left Turn Lane												
Headway Factor	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
Number of Detectors	2	1	1	2	1		2	2		2	2	
Detector Template	Left	Det25	Right	Left	Det25		Left	Side St		Left	Side St	
Leading Detector (ft)	78	153	153	78	153		78	78		78	78	
Trailing Detector (ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Position(ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Size(ft)	16	16	16	16	16		16	16		16	16	
Detector 1 Type	CI+Ex	Cl+Ex	Cl+Ex	CI+Ex	CI+Ex		CI+Ex	Cl+Ex		Cl+Ex	CI+Ex	
Detector 1 Channel												
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 2 Position(ft)	72	0.0	0.0	72	0.0		72	72		72	72	
Detector 2 Size(ft)	6			6			6	6		6	6	
Detector 2 Type	CI+Ex			CI+Ex			Cl+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 2 Channel	JI. LX			JI LA			JI- LA	Ο1 · ΕΛ		31 · LA	Ο1 · LΛ	
Detector 2 Extend (s)	0.0			0.0			0.0	0.0		0.0	0.0	
Esterio (3)	0.0			0.0			0.0	0.0		0.0	0.0	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Detector Phase	5	2	2	1	6		8	8		4	4	
Switch Phase												
Minimum Initial (s)	4.0	10.0	10.0	4.0	10.0		6.0	6.0		6.0	6.0	
Minimum Split (s)	8.5	26.0	26.0	8.5	30.0		11.5	11.5		23.5	23.5	
Total Split (s)	29.5	54.0	54.0	19.5	44.0		25.5	25.5		25.5	25.5	
Total Split (%)	29.8%	54.5%	54.5%	19.7%	44.4%		25.8%	25.8%		25.8%	25.8%	
Maximum Green (s)	25.0	50.0	50.0	15.0	40.0		20.0	20.0		20.0	20.0	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5		4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	0.5	0.5	1.0	0.5		1.5	1.5		1.5	1.5	
Lost Time Adjust (s)	-0.5	0.0	0.0	-0.5	0.0			-1.5			-1.5	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lead/Lag	Lag	Lag	Lag	Lead	Lead							
Lead-Lag Optimize?												
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8		2.5	2.5		2.5	2.5	
Minimum Gap (s)	0.5	3.8	3.8	0.5	3.8		2.0	2.0		2.0	2.0	
Time Before Reduce (s)	8.0	10.0	10.0	8.0	10.0		5.0	5.0		5.0	5.0	
Time To Reduce (s)	3.0	10.0	10.0	3.0	10.0		5.0	5.0		5.0	5.0	
Recall Mode	None	Min	Min	None	Min		None	None		None	None	
Walk Time (s)		7.0	7.0		7.0					7.0	7.0	
Flash Dont Walk (s)		15.0	15.0		19.0					11.0	11.0	
Pedestrian Calls (#/hr)		0	0		0					0	0	
Act Effct Green (s)	8.3	35.2	35.2		28.3			20.5			20.5	
Actuated g/C Ratio	0.13	0.55	0.55		0.44			0.32			0.32	
v/c Ratio	0.29	0.56	0.05		0.74			0.48			0.33	
Control Delay	34.6	10.3	0.4		19.9			29.4			8.8	
Queue Delay	0.0	0.0	0.0		0.0			0.0			0.0	
Total Delay	34.6	10.3	0.4		19.9			29.4			8.8	
LOS	С	В	Α		В			С			Α	
Approach Delay		11.4			19.9			29.4			8.8	
Approach LOS		В			В			С			Α	
Intersection Summary												

Intersection Summary

Area Type: Other

Cycle Length: 99

Actuated Cycle Length: 64.4)

Natural Cycle: 65

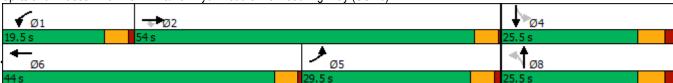
Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.74

Intersection Signal Delay: 16.1 Intersection LOS: B
Intersection Capacity Utilization 65.0% ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)



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Lane Group	EBL	EBT	EBR	WBT	NBT	SBT
Lane Group Flow (vph)	59	904	36	1035	153	178
v/c Ratio	0.29	0.56	0.05	0.74	0.48	0.33
Control Delay	34.6	10.3	0.4	19.9	29.4	8.8
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	34.6	10.3	0.4	19.9	29.4	8.8
Queue Length 50th (ft)	24	112	0	200	54	10
Queue Length 95th (ft)	65	151	2	290	#142	64
Internal Link Dist (ft)		388		222	285	130
Turn Bay Length (ft)	115		100			
Base Capacity (vph)	675	2332	1103	2100	361	601
Starvation Cap Reductn	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0
Reduced v/c Ratio	0.09	0.39	0.03	0.49	0.42	0.30
Intersection Summary						

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	^	7	*	∱ }			4			4	
Traffic Volume (vph)	54	832	33	0	937	16	136	3	2	21	7	135
Future Volume (vph)	54	832	33	0	937	16	136	3	2	21	7	135
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)	4.0	4.0	4.0		4.0			4.0			4.0	
Lane Util. Factor	1.00	0.95	1.00		0.95			1.00			1.00	
Frpb, ped/bikes	1.00	1.00	0.98		1.00			1.00			0.99	
Flpb, ped/bikes	1.00	1.00	1.00		1.00			1.00			1.00	
Frt	1.00	1.00	0.85		1.00			1.00			0.89	
Flt Protected	0.95	1.00	1.00		1.00			0.95			0.99	
Satd. Flow (prot)	1568	2942	1373		3160			1602			1458	
FIt Permitted	0.95	1.00	1.00		1.00			0.59			0.95	
Satd. Flow (perm)	1568	2942	1373		3160			994			1398	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	59	904	36	0	1018	17	148	3	2	23	8	147
RTOR Reduction (vph)	0	0	16	0	1	0	0	1	0	0	101	0
Lane Group Flow (vph)	59	904	20	0	1034	0	0	152	0	0	77	0
Confl. Peds. (#/hr)			1	1			2					2
Confl. Bikes (#/hr)						1						
Heavy Vehicles (%)	6%	13%	6%	0%	5%	0%	4%	0%	0%	24%	0%	2%
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases		_	2	•			8			4	•	
Actuated Green, G (s)	4.6	37.4	37.4		28.3			18.9			18.9	
Effective Green, g (s)	5.1	37.4	37.4		28.3			20.4			20.4	
Actuated g/C Ratio	0.08	0.57	0.57		0.43			0.31			0.31	
Clearance Time (s)	4.5	4.0	4.0		4.0			5.5			5.5	
Vehicle Extension (s)	2.3	5.8	5.8		5.8			2.5			2.5	
Lane Grp Cap (vph)	121	1672	780		1359			308			433	
v/s Ratio Prot	0.04	c0.31	700		c0.33			000			400	
v/s Ratio Perm	0.04	00.01	0.01		00.00			c0.15			0.05	
v/c Ratio	0.49	0.54	0.03		0.76			0.49			0.18	
Uniform Delay, d1	29.1	8.8	6.2		15.9			18.5			16.6	
Progression Factor	1.00	1.00	1.00		1.00			1.00			1.00	
Incremental Delay, d2	1.8	0.8	0.0		3.3			0.9			0.1	
Delay (s)	30.9	9.6	6.3		19.1			19.4			16.7	
Level of Service	C	3.0 A	Α		В			В			В	
Approach Delay (s)	0	10.8			19.1			19.4			16.7	
Approach LOS		В			В			В			В	
Intersection Summary												
HCM 2000 Control Delay			15.4	H	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capacit	v ratio		0.66	,.								
Actuated Cycle Length (s)	,		65.8	Sı	um of lost	time (s)			12.0			
Intersection Capacity Utilization	on		65.0%		U Level c				С			
Analysis Period (min)			15			2.7.00						
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	ሻ	∱ ∱			4			4	
Traffic Volume (veh/h)	54	832	33	0	937	16	136	3	2	21	7	135
Future Volume (veh/h)	54	832	33	0	937	16	136	3	2	21	7	135
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		0.98	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1668	1573	1668	1750	1682	1682	1750	1750	1750	1750	1750	1750
Adj Flow Rate, veh/h	59	904	0	0	1018	16	148	3	1	23	8	38
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	6	13	6	0	5	5	0	0	0	0	0	0
Cap, veh/h	86	2069	979	3	1853	29	350	5	2	140	59	139
Arrive On Green	0.05	0.69	0.00	0.00	0.58	0.58	0.13	0.16	0.13	0.13	0.16	0.13
Sat Flow, veh/h	1589	2988	1414	1667	3218	51	1430	29	10	349	378	891
Grp Volume(v), veh/h	59	904	0	0	505	529	152	0	0	69	0	0
Grp Sat Flow(s),veh/h/ln	1589	1494	1414	1667	1598	1671	1469	0	0	1618	0	0
Q Serve(g_s), s	2.0	7.5	0.0	0.0	11.0	11.0	3.3	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(g_c), s	2.0	7.5	0.0	0.0	11.0	11.0	5.5	0.0	0.0	2.2	0.0	0.0
Prop In Lane	1.00		1.00	1.00		0.03	0.97		0.01	0.33		0.55
Lane Grp Cap(c), veh/h	86	2069	979	3	920	963	316	0	0	294	0	0
V/C Ratio(X)	0.69	0.44	0.00	0.00	0.55	0.55	0.48	0.00	0.00	0.23	0.00	0.00
Avail Cap(c_a), veh/h	725	2673	1265	462	1144	1196	633	0	0	635	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	26.0	3.8	0.0	0.0	7.4	7.4	22.8	0.0	0.0	21.4	0.0	0.0
Incr Delay (d2), s/veh	5.9	0.5	0.0	0.0	1.7	1.6	0.8	0.0	0.0	0.3	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	0.9	1.5	0.0	0.0	3.3	3.5	2.0	0.0	0.0	0.8	0.0	0.0
Unsig. Movement Delay, s/veh			0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0
LnGrp Delay(d),s/veh	31.9	4.3	0.0	0.0	9.0	8.9	23.7	0.0	0.0	21.7	0.0	0.0
LnGrp LOS	С	A	A	A	A	A	C	A	A	C	A	A
Approach Vol, veh/h		963			1034			152			69	
Approach Delay, s/veh		6.0			9.0			23.7			21.7	
Approach LOS		Α			Α			C			C C	
											U	
Timer - Assigned Phs	1	2		4	5	6		8				
Phs Duration (G+Y+Rc), s	0.0	43.2		12.7	7.0	36.2		12.7				
Change Period (Y+Rc), s	4.5	* 4.5		5.5	4.5	4.0		5.5				
Max Green Setting (Gmax), s	15.0	* 50		20.0	25.0	40.0		20.0				
Max Q Clear Time (g_c+I1), s	0.0	9.5		4.2	4.0	13.0		7.5				
Green Ext Time (p_c), s	0.0	23.0		0.2	0.1	19.2		0.4				
Intersection Summary												
HCM 6th Ctrl Delay			9.1									
HCM 6th LOS			Α									
Notos												

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	^	7	ሻ	∱ }			4			4	
Traffic Volume (vph)	151	1095	134	5	1128	16	116	24	7	38	23	100
Future Volume (vph)	151	1095	134	5	1128	16	116	24	7	38	23	100
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Storage Length (ft)	115		100	105		0	0		0	0		0
Storage Lanes	1		1	1		0	0		0	0		0
Taper Length (ft)	100			100			100			100		
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	1.00		0.98	1.00	1.00			1.00			0.99	
Frt			0.850		0.998			0.994			0.916	
Flt Protected	0.950			0.950				0.962			0.988	
Satd. Flow (prot)	1646	3228	1488	1662	3161	0	0	1639	0	0	1553	0
Flt Permitted	0.950			0.950				0.548			0.910	
Satd. Flow (perm)	1645	3228	1454	1662	3161	0	0	930	0	0	1431	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)			95		2			2			67	
Link Speed (mph)		25			25			25			25	
Link Distance (ft)		468			302			365			210	
Travel Time (s)		12.8			8.2			10.0			5.7	
Confl. Peds. (#/hr)	2		1	1		2	5					5
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Heavy Vehicles (%)	1%	3%	0%	0%	5%	0%	1%	8%	0%	0%	0%	1%
Adj. Flow (vph)	161	1165	143	5	1200	17	123	26	7	40	24	106
Shared Lane Traffic (%)												
Lane Group Flow (vph)	161	1165	143	5	1217	0	0	156	0	0	170	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA
Median Width(ft)		12			12			0			0	
Link Offset(ft)		-12			0			0			4	
Crosswalk Width(ft)		72			42			32			30	
Two way Left Turn Lane												
Headway Factor	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
Number of Detectors	2	1	1	2	1		2	2		2	2	
Detector Template	Left	Det25	Right	Left	Det25		Left	Side St		Left	Side St	
Leading Detector (ft)	78	153	153	78	153		78	78		78	78	
Trailing Detector (ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Position(ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Size(ft)	16	16	16	16	16		16	16		16	16	
Detector 1 Type	CI+Ex	Cl+Ex	CI+Ex	CI+Ex	CI+Ex		CI+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 1 Channel												
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 2 Position(ft)	72	0.0	0.0	72	0.0		72	72		72	72	
Detector 2 Size(ft)	6			6			6	6		6	6	
Detector 2 Type	CI+Ex			CI+Ex			Cl+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 2 Channel	OI. LX			OI LX			OI. LX	OI? LX		OI. LX	OI. LX	
Detector 2 Extend (s)	0.0			0.0			0.0	0.0		0.0	0.0	
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Tulli Type	FIUL	INA	ı Cilli	FIUL	INA		i Cilli	INA		ı CIIII	INA	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Detector Phase	5	2	2	1	6		8	8		4	4	
Switch Phase												
Minimum Initial (s)	4.0	10.0	10.0	4.0	10.0		6.0	6.0		6.0	6.0	
Minimum Split (s)	8.5	26.0	26.0	8.5	30.0		11.5	11.5		23.5	23.5	
Total Split (s)	20.0	70.0	70.0	15.0	65.0		25.0	25.0		25.0	25.0	
Total Split (%)	18.2%	63.6%	63.6%	13.6%	59.1%		22.7%	22.7%		22.7%	22.7%	
Maximum Green (s)	15.5	66.0	66.0	10.5	61.0		19.5	19.5		19.5	19.5	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5		4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	0.5	0.5	1.0	0.5		1.5	1.5		1.5	1.5	
Lost Time Adjust (s)	-0.5	0.0	0.0	-0.5	0.0			-1.5			-1.5	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lead/Lag	Lag	Lag	Lag	Lead	Lead							
Lead-Lag Optimize?												
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8		2.5	2.5		2.5	2.5	
Minimum Gap (s)	0.5	3.8	3.8	0.5	3.8		2.0	2.0		2.0	2.0	
Time Before Reduce (s)	8.0	10.0	10.0	8.0	10.0		5.0	5.0		5.0	5.0	
Time To Reduce (s)	3.0	10.0	10.0	3.0	10.0		5.0	5.0		5.0	5.0	
Recall Mode	None	C-Min	C-Min	None	C-Min		None	None		None	None	
Walk Time (s)		7.0	7.0		7.0					7.0	7.0	
Flash Dont Walk (s)		15.0	15.0		19.0					11.0	11.0	
Pedestrian Calls (#/hr)		0	0		0					0	0	
Act Effct Green (s)	15.0	76.5	76.5	5.8	59.7			23.3			23.3	
Actuated g/C Ratio	0.14	0.70	0.70	0.05	0.54			0.21			0.21	
v/c Ratio	0.72	0.52	0.14	0.06	0.71			0.78			0.48	
Control Delay	63.6	9.5	2.8	50.6	22.2			68.1			27.7	
Queue Delay	0.0	0.0	0.0	0.0	0.0			0.0			0.0	
Total Delay	63.6	9.5	2.8	50.6	22.2			68.1			27.7	
LOS	Е	Α	Α	D	С			Е			С	
Approach Delay		14.8			22.3			68.1			27.7	
Approach LOS		В			С			Е			С	

Intersection Summary

Area Type: Other

Cycle Length: 110

Actuated Cycle Length: 110

Offset: 0 (0%), Referenced to phase 2:EBT and 6:WBT, Start of Green, Master Intersection

Natural Cycle: 70

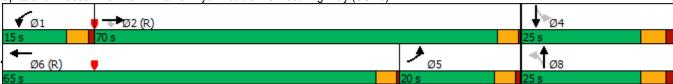
Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.78

Intersection Signal Delay: 21.3 Intersection LOS: C
Intersection Capacity Utilization 76.9% ICU Level of Service D

Analysis Period (min) 15

Splits and Phases: 3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)



	۶	→	•	•	←	†	↓
Lane Group	EBL	EBT	EBR	WBL	WBT	NBT	SBT
Lane Group Flow (vph)	161	1165	143	5	1217	156	170
v/c Ratio	0.72	0.52	0.14	0.06	0.71	0.78	0.48
Control Delay	63.6	9.5	2.8	50.6	22.2	68.1	27.7
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	63.6	9.5	2.8	50.6	22.2	68.1	27.7
Queue Length 50th (ft)	109	205	11	3	366	97	58
Queue Length 95th (ft)	#182	280	35	16	396	#233	136
Internal Link Dist (ft)		388			222	285	130
Turn Bay Length (ft)	115		100	105			
Base Capacity (vph)	248	2246	1040	166	1799	202	361
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.65	0.52	0.14	0.03	0.68	0.77	0.47
Intersection Summary							

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

	۶	→	*	•	—	•	1	†	~	/	ţ	✓
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	^	7	ሻ	∱ }			4			4	
Traffic Volume (vph)	151	1095	134	5	1128	16	116	24	7	38	23	100
Future Volume (vph)	151	1095	134	5	1128	16	116	24	7	38	23	100
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95			1.00			1.00	
Frpb, ped/bikes	1.00	1.00	0.98	1.00	1.00			1.00			0.99	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00			1.00			1.00	
Frt	1.00	1.00	0.85	1.00	1.00			0.99			0.92	
Flt Protected	0.95	1.00	1.00	0.95	1.00			0.96			0.99	
Satd. Flow (prot)	1646	3228	1454	1662	3161			1632			1554	
FIt Permitted	0.95	1.00	1.00	0.95	1.00			0.55			0.91	
Satd. Flow (perm)	1646	3228	1454	1662	3161			930			1430	
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	161	1165	143	5	1200	17	123	26	7	40	24	106
RTOR Reduction (vph)	0	0	32	0	1	0	0	2	0	0	53	0
Lane Group Flow (vph)	161	1165	111	5	1216	0	0	154	0	0	117	0
Confl. Peds. (#/hr)	2		1	1		2	5					5
Heavy Vehicles (%)	1%	3%	0%	0%	5%	0%	1%	8%	0%	0%	0%	1%
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Actuated Green, G (s)	18.0	73.0	73.0	1.2	56.2			21.8			21.8	
Effective Green, g (s)	18.5	73.0	73.0	1.7	56.2			23.3			23.3	
Actuated g/C Ratio	0.17	0.66	0.66	0.02	0.51			0.21			0.21	
Clearance Time (s)	4.5	4.0	4.0	4.5	4.0			5.5			5.5	
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8			2.5			2.5	
Lane Grp Cap (vph)	276	2142	964	25	1614			196			302	
v/s Ratio Prot	0.10	c0.36		0.00	c0.38							
v/s Ratio Perm			0.08					c0.17			0.08	
v/c Ratio	0.58	0.54	0.12	0.20	0.75			0.79			0.39	
Uniform Delay, d1	42.2	9.7	6.7	53.5	21.4			41.0			37.2	
Progression Factor	1.00	1.00	1.00	1.00	1.00			1.00			1.00	
Incremental Delay, d2	2.4	1.0	0.2	2.3	3.3			18.0			0.6	
Delay (s)	44.6	10.7	7.0	55.8	24.7			59.0			37.8	
Level of Service	D	В	Α	Е	С			E			D	
Approach Delay (s)		14.1			24.8			59.0			37.8	
Approach LOS		В			С			Е			D	
Intersection Summary												
HCM 2000 Control Delay			22.1	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capacity ratio			0.73									
Actuated Cycle Length (s)			110.0		um of lost				12.0			
Intersection Capacity Utilization	on		76.9%	IC	CU Level c	of Service			D			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	ň	∱ }			4			44	
Traffic Volume (veh/h)	151	1095	134	5	1128	16	116	24	7	38	23	100
Future Volume (veh/h)	151	1095	134	5	1128	16	116	24	7	38	23	100
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	0.99		0.99	0.99		0.99
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1736	1709	1750	1750	1682	1682	1641	1641	1641	1750	1750	1750
Adj Flow Rate, veh/h	161	1165	112	5	1200	16	123	26	5	40	24	50
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Percent Heavy Veh, %	1	3	0	0	5	5	8	8	8	0	0	0
Cap, veh/h	375	2335	1065	16	1636	22	210	35	6	112	73	110
Arrive On Green	0.23	0.72	0.72	0.01	0.51	0.51	0.14	0.16	0.14	0.14	0.16	0.14
Sat Flow, veh/h	1654	3247	1481	1667	3229	43	958	221	40	432	464	700
Grp Volume(v), veh/h	161	1165	112	5	594	622	154	0	0	114	0	0
Grp Sat Flow(s),veh/h/ln	1654	1624	1481	1667	1598	1674	1219	0	0	1596	0	0
Q Serve(g_s), s	9.2	17.3	2.5	0.3	32.1	32.1	6.6	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(g_c), s	9.2	17.3	2.5	0.3	32.1	32.1	13.8	0.0	0.0	7.2	0.0	0.0
Prop In Lane	1.00		1.00	1.00		0.03	0.80		0.03	0.35		0.44
Lane Grp Cap(c), veh/h	375	2335	1065	16	810	848	234	0	0	274	0	0
V/C Ratio(X)	0.43	0.50	0.11	0.31	0.73	0.73	0.66	0.00	0.00	0.42	0.00	0.00
Avail Cap(c_a), veh/h	375	2335	1065	167	886	928	278	0	0	324	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	36.5	6.8	4.7	54.1	21.3	21.3	45.7	0.0	0.0	42.6	0.0	0.0
Incr Delay (d2), s/veh	0.5	0.8	0.2	6.4	5.8	5.6	3.6	0.0	0.0	0.7	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	3.8	5.6	0.8	0.2	13.0	13.6	4.4	0.0	0.0	3.0	0.0	0.0
Unsig. Movement Delay, s/veh												
LnGrp Delay(d),s/veh	36.9	7.5	4.9	60.5	27.1	26.9	49.3	0.0	0.0	43.3	0.0	0.0
LnGrp LOS	D	Α	Α	Е	С	С	D	Α	Α	D	Α	Α
Approach Vol, veh/h		1438			1221			154			114	
Approach Delay, s/veh		10.6			27.1			49.3			43.3	
Approach LOS		В			С			D			D	
Timer - Assigned Phs	1	2		4	5	6		8				
Phs Duration (G+Y+Rc), s	5.1	83.6		21.3	28.9	59.8		21.3				
Change Period (Y+Rc), s	4.5	* 4.5		5.5	4.5	4.0		5.5				
Max Green Setting (Gmax), s	10.5	* 66		19.5	15.5	61.0		19.5				
Max Q Clear Time (g_c+I1), s	2.3	19.3		9.2	11.2	34.1		15.8				
Green Ext Time (p_c), s	0.0	34.8		0.3	0.2	21.7		0.2				
. ,	0.0	04.0		0.0	0.2	21.1		0.2				
Intersection Summary												
HCM 6th Ctrl Delay			20.8									
HCM 6th LOS			C									
Notos												

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

Lane Group EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT Lane Configurations ↑ <	140 140 1750 0 0
Traffic Volume (vph) 56 865 34 0 974 17 141 3 2 22 7 Future Volume (vph) 56 865 34 0 974 17 141 3 2 22 7 Ideal Flow (vphpl) 1750 </th <th>140 1750 0 0</th>	140 1750 0 0
Traffic Volume (vph) 56 865 34 0 974 17 141 3 2 22 7 Future Volume (vph) 56 865 34 0 974 17 141 3 2 22 7 Ideal Flow (vphpl) 1750 </td <td>140 1750 0 0</td>	140 1750 0 0
Future Volume (vph) 56 865 34 0 974 17 141 3 2 22 7 Ideal Flow (vphpl) 1750	1750 0 0
Ideal Flow (vphpl) 1750 <td>1750 0 0</td>	1750 0 0
Storage Length (ft) 115 100 105 0 0 0 0 Storage Lanes 1 1 1 0 0 0 0	0
Storage Lanes 1 1 1 0 0 0	0
0	
Tabol Consultin 100 100 100 100	1.00
Lane Util. Factor 1.00 0.95 1.00 1.00 0.95 0.95 1.00 1.00 1.00 1.00 1.00	
Ped Bike Factor 0.98 1.00 1.00 0.99	
Frt 0.850 0.997 0.998 0.888	
Flt Protected 0.950 0.954 0.994	
Satd. Flow (prot) 1568 2942 1403 1716 3158 0 0 1603 0 0 1454	0
Flt Permitted 0.950 0.572 0.951	
Satd. Flow (perm) 1568 2942 1372 1716 3158 0 0 959 0 0 1391	0
Right Turn on Red Yes Yes Yes	Yes
Satd. Flow (RTOR) 77 2 1 152	. 00
Link Speed (mph) 25 25 25 25	
Link Distance (ft) 468 302 365 210	
Travel Time (s) 12.8 8.2 10.0 5.7	
Confl. Peds. (#/hr) 1 1 2	2
Confl. Bikes (#/hr)	_
Peak Hour Factor 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92	0.92
Heavy Vehicles (%) 6% 13% 6% 2% 5% 2% 4% 2% 2% 24% 2%	2%
Adj. Flow (vph) 61 940 37 0 1059 18 153 3 2 24 8	152
Shared Lane Traffic (%)	
Lane Group Flow (vph) 61 940 37 0 1077 0 0 158 0 0 184	0
Enter Blocked Intersection No	No
Lane Alignment L NA R NA R NA L NA R NA L NA R NA R NA	R NA
Median Width(ft) 12 12 0 0	
Link Offset(ft) -12 0 0 4	
Crosswalk Width(ft) 72 42 32 30	
Two way Left Turn Lane	
Headway Factor 1.11 1.11 1.11 1.11 1.11 1.11 1.11 1.	1.11
Number of Detectors 2 1 1 2 1 2 2 2 2	
Detector Template Left Det25 Right Left Det25 Left Side St Left Side St	
Leading Detector (ft) 78 153 153 78 153 78 78 78 78	
Trailing Detector (ft) 2 137 137 2 137 2 2 2 2	
Detector 1 Position(ft) 2 137 137 2 137 2 2 2 2	
Detector 1 Size(ft) 16 16 16 16 16 16 16 16 16	
Detector 1 Type CI+Ex CI+Ex CI+Ex CI+Ex CI+Ex CI+Ex CI+Ex CI+Ex CI+Ex	
Detector 1 Channel	
Detector 1 Extend (s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	
Detector 1 Queue (s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	
Detector 1 Delay (s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	
Detector 2 Position(ft) 72 72 72 72 72 72 72	
Detector 2 Size(ft) 6 6 6 6 6	
Detector 2 Type CI+Ex CI+Ex CI+Ex CI+Ex CI+Ex	
Detector 2 Channel	
Detector 2 Extend (s) 0.0 0.0 0.0 0.0 0.0 0.0	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Detector Phase	5	2	2	1	6		8	8		4	4	
Switch Phase												
Minimum Initial (s)	4.0	10.0	10.0	4.0	10.0		6.0	6.0		6.0	6.0	
Minimum Split (s)	8.5	26.0	26.0	8.5	30.0		11.5	11.5		23.5	23.5	
Total Split (s)	29.5	54.0	54.0	19.5	44.0		25.5	25.5		25.5	25.5	
Total Split (%)	29.8%	54.5%	54.5%	19.7%	44.4%		25.8%	25.8%		25.8%	25.8%	
Maximum Green (s)	25.0	50.0	50.0	15.0	40.0		20.0	20.0		20.0	20.0	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5		4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	0.5	0.5	1.0	0.5		1.5	1.5		1.5	1.5	
Lost Time Adjust (s)	-0.5	0.0	0.0	-0.5	0.0			-1.5			-1.5	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lead/Lag	Lag	Lag	Lag	Lead	Lead							
Lead-Lag Optimize?												
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8		2.5	2.5		2.5	2.5	
Minimum Gap (s)	0.5	3.8	3.8	0.5	3.8		2.0	2.0		2.0	2.0	
Time Before Reduce (s)	8.0	10.0	10.0	8.0	10.0		5.0	5.0		5.0	5.0	
Time To Reduce (s)	3.0	10.0	10.0	3.0	10.0		5.0	5.0		5.0	5.0	
Recall Mode	None	Min	Min	None	Min		None	None		None	None	
Walk Time (s)		7.0	7.0		7.0					7.0	7.0	
Flash Dont Walk (s)		15.0	15.0		19.0					11.0	11.0	
Pedestrian Calls (#/hr)		0	0		0					0	0	
Act Effct Green (s)	8.3	39.6	39.6		30.0			21.2			21.2	
Actuated g/C Ratio	0.12	0.57	0.57		0.43			0.31			0.31	
v/c Ratio	0.32	0.56	0.05		0.79			0.54			0.35	
Control Delay	36.8	10.1	0.4		22.3			33.3			9.1	
Queue Delay	0.0	0.0	0.0		0.0			0.0			0.0	
Total Delay	36.8	10.1	0.4		22.3			33.3			9.1	
LOS	D	В	Α		С			С			Α	
Approach Delay		11.3			22.3			33.3			9.1	
Approach LOS		В			С			С			Α	
Intersection Summary												

Intersection Summary

Area Type: Other

Cycle Length: 99

Actuated Cycle Length: 69.3)

Natural Cycle: 65

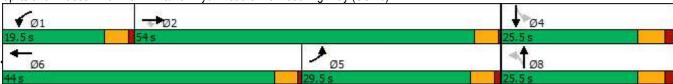
Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.79

Intersection Signal Delay: 17.4 Intersection LOS: B
Intersection Capacity Utilization 66.8% ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)



	•	→	\rightarrow	←	†	ļ
Lane Group	EBL	EBT	EBR	WBT	NBT	SBT
Lane Group Flow (vph)	61	940	37	1077	158	184
v/c Ratio	0.32	0.56	0.05	0.79	0.54	0.35
Control Delay	36.8	10.1	0.4	22.3	33.3	9.1
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	36.8	10.1	0.4	22.3	33.3	9.1
Queue Length 50th (ft)	26	118	0	213	59	10
Queue Length 95th (ft)	67	160	2	309	#160	65
Internal Link Dist (ft)		388		222	285	130
Turn Bay Length (ft)	115		100			
Base Capacity (vph)	613	2189	1040	1940	317	560
Starvation Cap Reductn	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0
Reduced v/c Ratio	0.10	0.43	0.04	0.56	0.50	0.33
Intersection Summary						

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

	۶	→	•	•	←	•	•	†	<i>></i>	/	+	-√
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	^	7	*	↑ ↑			4			4	
Traffic Volume (vph)	56	865	34	0	974	17	141	3	2	22	7	140
Future Volume (vph)	56	865	34	0	974	17	141	3	2	22	7	140
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)	4.0	4.0	4.0		4.0			4.0			4.0	
Lane Util. Factor	1.00	0.95	1.00		0.95			1.00			1.00	
Frpb, ped/bikes	1.00	1.00	0.98		1.00			1.00			0.99	
Flpb, ped/bikes	1.00	1.00	1.00		1.00			1.00			1.00	
Frt	1.00	1.00	0.85		1.00			1.00			0.89	
Flt Protected	0.95	1.00	1.00		1.00			0.95			0.99	
Satd. Flow (prot)	1568	2942	1373		3159			1601			1456	
FIt Permitted	0.95	1.00	1.00		1.00			0.57			0.95	
Satd. Flow (perm)	1568	2942	1373		3159			960			1394	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	61	940	37	0	1059	18	153	3	2	24	8	152
RTOR Reduction (vph)	0	0	15	0	1	0	0	1	0	0	106	0
Lane Group Flow (vph)	61	940	22	0	1076	0	0	157	0	0	78	0
Confl. Peds. (#/hr)			1	1			2					2
Confl. Bikes (#/hr)						1						
Heavy Vehicles (%)	6%	13%	6%	2%	5%	2%	4%	2%	2%	24%	2%	2%
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases		_	2	•			8			4	•	
Actuated Green, G (s)	6.2	40.7	40.7		30.0			19.6			19.6	
Effective Green, g (s)	6.7	40.7	40.7		30.0			21.1			21.1	
Actuated g/C Ratio	0.10	0.58	0.58		0.43			0.30			0.30	
Clearance Time (s)	4.5	4.0	4.0		4.0			5.5			5.5	
Vehicle Extension (s)	2.3	5.8	5.8		5.8			2.5			2.5	
Lane Grp Cap (vph)	150	1715	800		1357			290			421	
v/s Ratio Prot	0.04	c0.32	000		c0.34			200			721	
v/s Ratio Perm	0.04	00.02	0.02		<mark>С</mark> 0.0 т			c 0.16			0.06	
v/c Ratio	0.41	0.55	0.02		0.79			0.54			0.19	
Uniform Delay, d1	29.7	8.9	6.2		17.2			20.3			18.0	
Progression Factor	1.00	1.00	1.00		1.00			1.00			1.00	
Incremental Delay, d2	1.00	0.8	0.0		3.9			1.6			0.2	
Delay (s)	30.7	9.7	6.2		21.1			22.0			18.2	
Level of Service	C	Α	Α.2		C			ZZ.0			В	
Approach Delay (s)	J	10.8			21.1			22.0			18.2	
Approach LOS		В			C			C			В	
Intersection Summary												
HCM 2000 Control Delay			16.6	H	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capacit	ty ratio		0.70	,.								
Actuated Cycle Length (s)	,		69.8	Sı	um of lost	time (s)			12.0			
Intersection Capacity Utilization	on		66.8%		U Level o				C			
Analysis Period (min)			15			2.7.00						
c Critical Lane Group												

	•	→	•	•	←	•	4	†	~	>	ļ	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	ሻ	ħβ			4			4	
Traffic Volume (veh/h)	56	865	34	0	974	17	141	3	2	22	7	140
Future Volume (veh/h)	56	865	34	0	974	17	141	3	2	22	7	140
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		0.98	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1668	1573	1668	1723	1682	1682	1723	1723	1723	1723	1723	1723
Adj Flow Rate, veh/h	61	940	1	0	1059	17	153	3	1	24	8	38
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	6	13	6	2	5	5	2	2	2	2	2	2
Cap, veh/h	88	2069	978	3	1854	30	349	4	1	140	61	139
Arrive On Green	0.06	0.69	0.69	0.00	0.58	0.58	0.13	0.16	0.13	0.13	0.16	0.13
Sat Flow, veh/h	1589	2988	1413	1641	3217	52	1407	28	9	350	378	865
Grp Volume(v), veh/h	61	940	1	0	526	550	157	0	0	70	0	0
Grp Sat Flow(s),veh/h/ln	1589	1494	1413	1641	1598	1671	1444	0	0	1594	0	0
Q Serve(g_s), s	2.2	8.1	0.0	0.0	12.0	12.0	3.6	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(g_c), s	2.2	8.1	0.0	0.0	12.0	12.0	6.0	0.0	0.0	2.3	0.0	0.0
Prop In Lane	1.00	.	1.00	1.00		0.03	0.97	0.0	0.01	0.34	0.0	0.54
Lane Grp Cap(c), veh/h	88	2069	978	3	921	963	317	0	0	298	0	0
V/C Ratio(X)	0.69	0.45	0.00	0.00	0.57	0.57	0.50	0.00	0.00	0.24	0.00	0.00
Avail Cap(c_a), veh/h	702	2590	1225	441	1108	1159	606	0	0	609	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	0.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	26.8	4.0	2.7	0.0	7.7	7.7	23.4	0.0	0.0	21.9	0.0	0.0
Incr Delay (d2), s/veh	5.8	0.5	0.0	0.0	1.8	1.7	0.9	0.0	0.0	0.3	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	0.9	1.7	0.0	0.0	3.7	3.9	2.1	0.0	0.0	0.9	0.0	0.0
Unsig. Movement Delay, s/veh		1.7	0.0	0.0	0.7	0.0	2.1	0.0	0.0	0.0	0.0	0.0
LnGrp Delay(d),s/veh	32.6	4.5	2.7	0.0	9.5	9.4	24.3	0.0	0.0	22.2	0.0	0.0
LnGrp LOS	C	4.0 A	Α	Α	Α	Α	C C	Α	Α	C	Α	Α
Approach Vol, veh/h		1002			1076			157			70	
Approach Delay, s/veh		6.2			9.5			24.3			22.2	
Approach LOS		Α			9.5 A			24.3 C			C C	
Apploach EOS											C	
Timer - Assigned Phs	1	2		4	5	6		8				
Phs Duration (G+Y+Rc), s	0.0	44.4		13.2	7.2	37.2		13.2				
Change Period (Y+Rc), s	4.5	* 4.5		5.5	4.5	4.0		5.5				
Max Green Setting (Gmax), s	15.0	* 50		20.0	25.0	40.0		20.0				
Max Q Clear Time (g_c+I1), s	0.0	10.1		4.3	4.2	14.0		8.0				
Green Ext Time (p_c), s	0.0	23.7		0.2	0.2	19.3		0.4				
Intersection Summary												
HCM 6th Ctrl Delay			9.5									
HCM 6th LOS			A									
Notos												

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

	•	→	•	•	+	•	•	†	/	/	+	4
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	^	7	ሻ	↑ ↑			4			4	
Traffic Volume (vph)	157	1139	139	5	1173	17	121	25	7	40	24	104
Future Volume (vph)	157	1139	139	5	1173	17	121	25	7	40	24	104
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Storage Length (ft)	115		100	105		0	0		0	0		0
Storage Lanes	1		1	1		0	0		0	0		0
Taper Length (ft)	100		•	100		•	100		•	100		
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	1.00	0.00	0.98	1.00	1.00	0.00	1.00	1.00	1.00	1.00	0.99	1.00
Frt	1.00		0.850	1.00	0.998			0.994			0.917	
Flt Protected	0.950		0.000	0.950	0.000			0.962			0.988	
Satd. Flow (prot)	1630	3228	1458	1630	3161	0	0	1625	0	0	1534	0
Flt Permitted	0.950	OLLO	1 100	0.950	0101	V	•	0.549	· ·		0.906	J
Satd. Flow (perm)	1629	3228	1426	1629	3161	0	0	924	0	0	1407	0
Right Turn on Red	1020	OLLO	Yes	1020	0101	Yes	•	021	Yes		1101	Yes
Satd. Flow (RTOR)			95		2	100		2			65)	. 00
Link Speed (mph)		25			25			25			25	
Link Distance (ft)		468			302			365			210	
Travel Time (s)		12.8			8.2			10.0			5.7	
Confl. Peds. (#/hr)	2		1	1	V. <u> </u>	2	5				• • • • • • • • • • • • • • • • • • • •	5
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Heavy Vehicles (%)	2%	3%	2%	2%	5%	2%	2%	8%	2%	2%	2%	2%
Adj. Flow (vph)	167	1212	148	5	1248	18	129	27	7	43	26	111
Shared Lane Traffic (%)							0					
Lane Group Flow (vph)	167	1212	148	5	1266	0	0	163	0	0	180	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA
Median Width(ft)		12			12			0			0	
Link Offset(ft)		-12			0			0			4	
Crosswalk Width(ft)		72			42			32			30	
Two way Left Turn Lane												
Headway Factor	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
Number of Detectors	2	1	1	2	1		2	2		2	2	
Detector Template	Left	Det25	Right	Left	Det25		Left	Side St		Left	Side St	
Leading Detector (ft)	78	153	153	78	153		78	78		78	78	
Trailing Detector (ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Position(ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Size(ft)	16	16	16	16	16		16	16		16	16	
Detector 1 Type	CI+Ex	CI+Ex	CI+Ex	CI+Ex	Cl+Ex		CI+Ex	Cl+Ex		Cl+Ex	CI+Ex	
Detector 1 Channel												
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 2 Position(ft)	72			72			72	72		72	72	
Detector 2 Size(ft)	6			6			6	6		6	6	
Detector 2 Type	CI+Ex			CI+Ex			CI+Ex	Cl+Ex		CI+Ex	Cl+Ex	
Detector 2 Channel												
Detector 2 Extend (s)	0.0			0.0			0.0	0.0		0.0	0.0	
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	

	•	→	•	•	←	•	4	†	<i>></i>	>	ļ	4
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Detector Phase	5	2	2	1	6		8	8		4	4	
Switch Phase												
Minimum Initial (s)	4.0	10.0	10.0	4.0	10.0		6.0	6.0		6.0	6.0	
Minimum Split (s)	8.5	26.0	26.0	8.5	30.0		11.5	11.5		23.5	23.5	
Total Split (s)	20.0	70.0	70.0	15.0	65.0		25.0	25.0		25.0	25.0	
Total Split (%)	18.2%	63.6%	63.6%	13.6%	59.1%		22.7%	22.7%		22.7%	22.7%	
Maximum Green (s)	15.5	66.0	66.0	10.5	61.0		19.5	19.5		19.5	19.5	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5		4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	0.5	0.5	1.0	0.5		1.5	1.5		1.5	1.5	
Lost Time Adjust (s)	-0.5	0.0	0.0	-0.5	0.0			-1.5			-1.5	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lead/Lag	Lag	Lag	Lag	Lead	Lead							
Lead-Lag Optimize?												
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8		2.5	2.5		2.5	2.5	
Minimum Gap (s)	0.5	3.8	3.8	0.5	3.8		2.0	2.0		2.0	2.0	
Time Before Reduce (s)	8.0	10.0	10.0	8.0	10.0		5.0	5.0		5.0	5.0	
Time To Reduce (s)	3.0	10.0	10.0	3.0	10.0		5.0	5.0		5.0	5.0	
Recall Mode	None	C-Min	C-Min	None	C-Min		None	None		None	None	
Walk Time (s)		7.0	7.0		7.0					7.0	7.0	
Flash Dont Walk (s)		15.0	15.0		19.0					11.0	11.0	
Pedestrian Calls (#/hr)		0	0		0					0	0	
Act Effct Green (s)	15.2	74.6	74.6	5.8	57.5			25.3			25.3	
Actuated g/C Ratio	0.14	0.68	0.68	0.05	0.52			0.23			0.23	
v/c Ratio	0.74	0.55	0.15	0.06	0.77			0.76			0.48	
Control Delay	65.3	10.5	2.9	50.6	24.8			64.2			28.9	
Queue Delay	0.0	0.0	0.0	0.0	0.0			0.0			0.0	
Total Delay	65.3	10.5	2.9	50.6	24.8			64.2			28.9	
LOS	Е	В	Α	D	С			Е			С	
Approach Delay		15.8			24.9			64.2			28.9	
Approach LOS		В			С			Е			С	
Intone 1' O												

Intersection Summary

Area Type: Other

Cycle Length: 110
Actuated Cycle Length: 110

Offset: 0 (0%), Referenced to phase 2:EBT and 6:WBT, Start of Green, Master Intersection

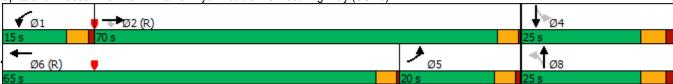
Natural Cycle: 75

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.77

Intersection Signal Delay: 22.7 Intersection LOS: C
Intersection Capacity Utilization 79.4% ICU Level of Service D

Analysis Period (min) 15



	۶	→	•	•	←	†	ļ
Lane Group	EBL	EBT	EBR	WBL	WBT	NBT	SBT
Lane Group Flow (vph)	167	1212	148	5	1266	163	180
v/c Ratio	0.74	0.55	0.15	0.06	0.77	0.76	0.48
Control Delay	65.3	10.5	2.9	50.6	24.8	64.2	28.9
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	65.3	10.5	2.9	50.6	24.8	64.2	28.9
Queue Length 50th (ft)	113	218	12	3	397	102	66
Queue Length 95th (ft)	#207	297	37	16	416	#245	147
Internal Link Dist (ft)		388			222	285	130
Turn Bay Length (ft)	115		100	105			
Base Capacity (vph)	247	2189	997	163	1758	214	373
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.68	0.55	0.15	0.03	0.72	0.76	0.48
Intersection Summary							

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

	۶	→	*	•	←	•	1	†	~	/	ţ	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	, j	† †	7	7	↑ ↑			4			4	
Traffic Volume (vph)	157	1139	139	5	1173	17	121	25	7	40	24	104
Future Volume (vph)	157	1139	139	5	1173	17	121	25	7	40	24	104
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95			1.00			1.00	
Frpb, ped/bikes	1.00	1.00	0.98	1.00	1.00			1.00			0.99	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00			1.00			1.00	
Frt	1.00	1.00	0.85	1.00	1.00			0.99			0.92	
Flt Protected	0.95	1.00	1.00	0.95	1.00			0.96			0.99	
Satd. Flow (prot)	1630	3228	1426	1630	3160			1618			1534	
FIt Permitted	0.95	1.00	1.00	0.95	1.00			0.55			0.91	
Satd. Flow (perm)	1630	3228	1426	1630	3160			924			1406	
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	167	1212	148	5	1248	18	129	27	7	43	26	111
RTOR Reduction (vph)	0	0	34	0	1	0	0	2	0	0	50	0
Lane Group Flow (vph)	167	1212	114	5	1265	0	0	161	0	0	130	0
Confl. Peds. (#/hr)	2	1212	1	1	1200	2	5	101			100	5
Heavy Vehicles (%)	2%	3%	2%	2%	5%	2%	2%	8%	2%	2%	2%	2%
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA	270	Perm	NA	
Protected Phases	5	2	1 Cilli	1	6		1 Cilli	8		1 Cilli	4	
Permitted Phases	<u> </u>		2	'	- U		8	- U		4		
Actuated Green, G (s)	18.3	71.0	71.0	1.2	53.9		U	23.8		7	23.8	
Effective Green, g (s)	18.8	71.0	71.0	1.7	53.9			25.3			25.3	
Actuated g/C Ratio	0.17	0.65	0.65	0.02	0.49			0.23			0.23	
Clearance Time (s)	4.5	4.0	4.0	4.5	4.0			5.5			5.5	
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8			2.5			2.5	
Lane Grp Cap (vph)	278	2083	920	25	1548			212			323	
v/s Ratio Prot	0.10	c0.38	920	0.00	c0.40			212			323	
v/s Ratio Perm	0.10	60.36	0.08	0.00	C 0.40			c 0.17			0.09	
v/c Ratio	0.60	0.58	0.00	0.20	0.82			0.76			0.09	
Uniform Delay, d1	42.1	11.1	7.5	53.5	23.9			39.5			35.9	
• •	1.00	1.00	1.00	1.00	1.00			1.00			1.00	
Progression Factor	2.8	1.00	0.3	2.3	4.9			14.3			0.6	
Incremental Delay, d2		12.3						53.8			36.5	
Delay (s)	45.0		7.8	55.8	28.8							
Level of Service	D	B	Α	Е	C			D D			D	
Approach Delay (s) Approach LOS		15.4 B			28.9 C			53.8 D			36.5 D	
Intersection Summary												
HCM 2000 Control Delay			24.1	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capacit	tv ratio		0.77	-								
Actuated Cycle Length (s)	.,		110.0	S	um of lost	time (s)			12.0			
Intersection Capacity Utilization	on		79.4%		CU Level o				D			
Analysis Period (min)	· ·		15		, = 3.070	2230						
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	7	ħβ			4			4	
Traffic Volume (veh/h)	157	1139	139	5	1173	17	121	25	7	40	24	104
Future Volume (veh/h)	157	1139	139	5	1173	17	121	25	7	40	24	104
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	0.99		0.99	0.99		0.99
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1723	1709	1723	1723	1682	1682	1641	1641	1641	1723	1723	1723
Adj Flow Rate, veh/h	167	1212	116	5	1248	17	129	27	5	43	26	58
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Percent Heavy Veh, %	2	3	2	2	5	5	8	8	8	2	2	2
Cap, veh/h	339	2299	1032	16	1665	23	215	36	6	114	74	121
Arrive On Green	0.21	0.71	0.71	0.01	0.52	0.52	0.15	0.17	0.15	0.15	0.17	0.15
Sat Flow, veh/h	1641	3247	1458	1641	3227	44	924	214	36	414	442	719
Grp Volume(v), veh/h	167	1212	116	5	618	647	161	0	0	127	0	0
Grp Sat Flow(s),veh/h/ln	1641	1624	1458	1641	1598	1674	1174	0	0	1574	0	0
Q Serve(g_s), s	9.9	19.1	2.8	0.3	33.6	33.6	7.0	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(g_c), s	9.9	19.1	2.8	0.3	33.6	33.6	15.0	0.0	0.0	8.1	0.0	0.0
Prop In Lane	1.00		1.00	1.00		0.03	0.80		0.03	0.34		0.46
Lane Grp Cap(c), veh/h	339	2299	1032	16	824	864	241	0	0	288	0	0
V/C Ratio(X)	0.49	0.53	0.11	0.31	0.75	0.75	0.67	0.00	0.00	0.44	0.00	0.00
Avail Cap(c_a), veh/h	339	2299	1032	164	886	928	270	0	0	320	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	38.6	7.5	5.1	54.1	21.0	21.0	45.3	0.0	0.0	41.9	0.0	0.0
Incr Delay (d2), s/veh	0.7	0.9	0.2	6.7	6.2	5.9	4.7	0.0	0.0	0.8	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	4.1	6.3	0.9	0.2	13.6	14.2	4.7	0.0	0.0	3.3	0.0	0.0
Unsig. Movement Delay, s/veh		0.0	0.0	0.2	10.0	11.2		0.0	0.0	0.0	0.0	0.0
LnGrp Delay(d),s/veh	39.2	8.3	5.3	60.8	27.2	26.9	50.0	0.0	0.0	42.7	0.0	0.0
LnGrp LOS	D	A	A	E	C	C	D	A	A	D	A	A
Approach Vol, veh/h		1495			1270			161	, <u>, , , , , , , , , , , , , , , , , , </u>		127	
Approach Delay, s/veh		11.6			27.2			50.0			42.7	
Approach LOS		В			C C			50.0 D			42.7 D	
											U	
Timer - Assigned Phs	1	2		4	5	6		8				
Phs Duration (G+Y+Rc), s	5.1	82.4		22.5	26.7	60.8		22.5				
Change Period (Y+Rc), s	4.5	* 4.5		5.5	4.5	4.0		5.5				
Max Green Setting (Gmax), s	10.5	* 66		19.5	15.5	61.0		19.5				
Max Q Clear Time (g_c+l1), s	2.3	21.1		10.1	11.9	35.6		17.0				
Green Ext Time (p_c), s	0.0	34.9		0.3	0.2	21.2		0.1				
Intersection Summary												
HCM 6th Ctrl Delay			21.4									
HCM 6th LOS			C									
Notes												

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ች	^	7	ሻ	† }			4			4	
Traffic Volume (vph)	80	865	34	0	974	20	141	3	2	23	7	147
Future Volume (vph)	80	865	34	0	974	20	141	3	2	23	7	147
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Storage Length (ft)	115		100	105		0	0		0	0		0
Storage Lanes	1		1	1		0	0		0	0		0
Taper Length (ft)	100			100			100			100		
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor			0.98		1.00			1.00			0.99	
Frt			0.850		0.997			0.998			0.888	
Flt Protected	0.950							0.954			0.994	
Satd. Flow (prot)	1568	2942	1403	1716	3158	0	0	1603	0	0	1455	0
FIt Permitted	0.950							0.555			0.951	
Satd. Flow (perm)	1568	2942	1372	1716	3158	0	0	931	0	0	1392	0
Right Turn on Red			Yes			Yes			Yes	-		Yes
Satd. Flow (RTOR)			77		2			1			160	
Link Speed (mph)		25			25			25			25	
Link Distance (ft)		468			302			365			210	
Travel Time (s)		12.8			8.2			10.0			5.7	
Confl. Peds. (#/hr)			1	1			2				• • • • • • • • • • • • • • • • • • • •	2
Confl. Bikes (#/hr)			•	•		1	_					_
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	13%	6%	2%	5%	2%	4%	2%	2%	24%	2%	2%
Adj. Flow (vph)	87	940	37	0	1059	22	153	3	2	25	8	160
Shared Lane Traffic (%)	•	0.0	•	•					_			
Lane Group Flow (vph)	87	940	37	0	1081	0	0	158	0	0	193	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA
Median Width(ft)		12			12			0			0	
Link Offset(ft)		-12			0			0			4	
Crosswalk Width(ft)		72			42			32			30	
Two way Left Turn Lane		. –						<u> </u>				
Headway Factor	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
Number of Detectors	2	1	1	2	1		2	2		2	2	
Detector Template	Left	Det25	Right	Left	Det25			Side St			Side St	
Leading Detector (ft)	78	153	153	78	153		78	78		78	78	
Trailing Detector (ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Position(ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Size(ft)	16	16	16	16	16		16	16		16	16	
Detector 1 Type	CI+Ex	CI+Ex	CI+Ex	CI+Ex	CI+Ex		Cl+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 1 Channel	OI · LX	OI · LX	OILX	OI · LX	OI · LX		OI · LX	OI. LX		OI LX	OI · LX	
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 2 Position(ft)	72	0.0	0.0	72	0.0		72	72		72	72	
Detector 2 Size(ft)	6			6			6	6		6	6	
	Cl+Ex			Cl+Ex			Cl+Ex	Cl+Ex		CI+Ex	Cl+Ex	
Detector 2 Type	UI+EX			OI+EX			OI+EX	UI+EX		OI+EX	UI+EX	
Detector 2 Channel	0.0			0.0			0.0	0.0		0.0	0.0	
Detector 2 Extend (s)	0.0			0.0			0.0	0.0		0.0	0.0	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Detector Phase	5	2	2	1	6		8	8		4	4	
Switch Phase												
Minimum Initial (s)	4.0	10.0	10.0	4.0	10.0		6.0	6.0		6.0	6.0	
Minimum Split (s)	8.5	26.0	26.0	8.5	30.0		11.5	11.5		23.5	23.5	
Total Split (s)	29.5	54.0	54.0	19.5	44.0		25.5	25.5		25.5	25.5	
Total Split (%)	29.8%	54.5%	54.5%	19.7%	44.4%		25.8%	25.8%		25.8%	25.8%	
Maximum Green (s)	25.0	50.0	50.0	15.0	40.0		20.0	20.0		20.0	20.0	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5		4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	0.5	0.5	1.0	0.5		1.5	1.5		1.5	1.5	
Lost Time Adjust (s)	-0.5	0.0	0.0	-0.5	0.0			-1.5			-1.5	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lead/Lag	Lag	Lag	Lag	Lead	Lead							
Lead-Lag Optimize?												
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8		2.5	2.5		2.5	2.5	
Minimum Gap (s)	0.5	3.8	3.8	0.5	3.8		2.0	2.0		2.0	2.0	
Time Before Reduce (s)	8.0	10.0	10.0	8.0	10.0		5.0	5.0		5.0	5.0	
Time To Reduce (s)	3.0	10.0	10.0	3.0	10.0		5.0	5.0		5.0	5.0	
Recall Mode	None	Min	Min	None	Min		None	None		None	None	
Walk Time (s)		7.0	7.0		7.0					7.0	7.0	
Flash Dont Walk (s)		15.0	15.0		19.0					11.0	11.0	
Pedestrian Calls (#/hr)		0	0		0					0	0	
Act Effct Green (s)	9.6	41.4	41.4		30.6			21.9			21.9	
Actuated g/C Ratio	0.13	0.58	0.58		0.43			0.31			0.31	
v/c Ratio	0.42	0.55	0.04		0.80			0.55			0.36	
Control Delay	38.3	10.0	0.4		23.7			35.6			9.2	
Queue Delay	0.0	0.0	0.0		0.0			0.0			0.0	
Total Delay	38.3	10.0	0.4		23.7			35.6			9.2	
LOS	D	Α	Α		С			D			Α	
Approach Delay		11.9			23.7			35.6			9.2	
Approach LOS		В			С			D			Α	
Intersection Summary												

Intersection Summary

Area Type: Other

Cycle Length: 99

Actuated Cycle Length: 71.7

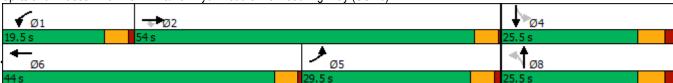
Natural Cycle: 65

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.80

Intersection Signal Delay: 18.3 Intersection LOS: B
Intersection Capacity Utilization 68.9% ICU Level of Service C

Analysis Period (min) 15



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Lane Group	EBL	EBT	EBR	WBT	NBT	SBT
Lane Group Flow (vph)	87	940	37	1081	158	193
v/c Ratio	0.42	0.55	0.04	0.80	0.55	0.36
Control Delay	38.3	10.0	0.4	23.7	35.6	9.2
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	38.3	10.0	0.4	23.7	35.6	9.2
Queue Length 50th (ft)	38	118	0	223	63	11
Queue Length 95th (ft)	88	160	2	327	#171	69
Internal Link Dist (ft)		388		222	285	130
Turn Bay Length (ft)	115		100			
Base Capacity (vph)	587	2179	1036	1858	295	549
Starvation Cap Reductn	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0
Reduced v/c Ratio	0.15	0.43	0.04	0.58	0.54	0.35
Intersection Summary						

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	*	^	7	ሻ	∱ 1≽			4			4	
Traffic Volume (vph)	80	865	34	0	974	20	141	3	2	23	7	147
Future Volume (vph)	80	865	34	0	974	20	141	3	2	23	7	147
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)	4.0	4.0	4.0		4.0			4.0			4.0	
Lane Util. Factor	1.00	0.95	1.00		0.95			1.00			1.00	
Frpb, ped/bikes	1.00	1.00	0.98		1.00			1.00			0.99	
Flpb, ped/bikes	1.00	1.00	1.00		1.00			1.00			1.00	
Frt	1.00	1.00	0.85		1.00			1.00			0.89	
Flt Protected	0.95	1.00	1.00		1.00			0.95			0.99	
Satd. Flow (prot)	1568	2942	1373		3157			1601			1455	
Flt Permitted	0.95	1.00	1.00		1.00			0.55			0.95	
Satd. Flow (perm)	1568	2942	1373		3157			931			1393	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	87	940	37	0	1059	22	153	3	2	25	8	160
RTOR Reduction (vph)	0	0	15	0	1	0	0	1	0	0	112	0
Lane Group Flow (vph)	87	940	22	0	1080	0	0	157	0	0	81	0
Confl. Peds. (#/hr)			1	1			2					2
Confl. Bikes (#/hr)						1						
Heavy Vehicles (%)	6%	13%	6%	2%	5%	2%	4%	2%	2%	24%	2%	2%
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Actuated Green, G (s)	7.4	42.5	42.5		30.6			20.3			20.3	
Effective Green, g (s)	7.9	42.5	42.5		30.6			21.8			21.8	
Actuated g/C Ratio	0.11	0.59	0.59		0.42			0.30			0.30	
Clearance Time (s)	4.5	4.0	4.0		4.0			5.5			5.5	
Vehicle Extension (s)	2.3	5.8	5.8		5.8			2.5			2.5	
Lane Grp Cap (vph)	171	1729	807		1336			280			420	
v/s Ratio Prot	0.06	c0.32	00.		c0.34			200			120	
v/s Ratio Perm	0.00	00.02	0.02		C 0.0.			c0.17			0.06	
v/c Ratio	0.51	0.54	0.03		0.81			0.56			0.19	
Uniform Delay, d1	30.4	9.0	6.2		18.3			21.2			18.7	
Progression Factor	1.00	1.00	1.00		1.00			1.00			1.00	
Incremental Delay, d2	1.4	0.8	0.0		4.4			2.1			0.2	
Delay (s)	31.8	9.8	6.3		22.7			23.3			18.9	
Level of Service	С	A	A		C			C			В	
Approach Delay (s)		11.5			22.7			23.3			18.9	
Approach LOS		В			С			С			В	
Intersection Summary												
HCM 2000 Control Delay			17.6	H	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capac	ity ratio		0.71									
Actuated Cycle Length (s)			72.3	Sı	um of lost	time (s)			12.0			
Intersection Capacity Utilizat	ion		68.9%	IC	CU Level of	of Service			С			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	ሻ	∱ ∱			4			4	
Traffic Volume (veh/h)	80	865	34	0	974	20	141	3	2	23	7	147
Future Volume (veh/h)	80	865	34	0	974	20	141	3	2	23	7	147
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		0.98	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1668	1573	1668	1723	1682	1682	1723	1723	1723	1723	1723	1723
Adj Flow Rate, veh/h	87	940	2	0	1059	21	153	3	1	25	8	40
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	6	13	6	2	5	5	2	2	2	2	2	2
Cap, veh/h	124	2090	988	3	1803	36	342	4	1	137	58	139
Arrive On Green	0.08	0.70	0.70	0.00	0.56	0.56	0.13	0.16	0.13	0.13	0.16	0.13
Sat Flow, veh/h	1589	2988	1413	1641	3203	64	1410	28	9	354	367	874
Grp Volume(v), veh/h	87	940	2	0	528	552	157	0	0	73	0	0
Grp Sat Flow(s),veh/h/ln	1589	1494	1413	1641	1598	1669	1447	0	0	1594	0	0
Q Serve(g_s), s	3.2	8.3	0.0	0.0	12.9	12.9	3.7	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(g_c), s	3.2	8.3	0.0	0.0	12.9	12.9	6.2	0.0	0.0	2.5	0.0	0.0
Prop In Lane	1.00	0.0	1.00	1.00		0.04	0.97	0.0	0.01	0.34	0.0	0.55
Lane Grp Cap(c), veh/h	124	2090	988	3	900	939	312	0	0	294	0	0
V/C Ratio(X)	0.70	0.45	0.00	0.00	0.59	0.59	0.50	0.00	0.00	0.25	0.00	0.00
Avail Cap(c_a), veh/h	677	2497	1181	425	1068	1116	585	0	0	587	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	0.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	26.9	3.9	2.7	0.0	8.5	8.5	24.3	0.0	0.0	22.8	0.0	0.0
Incr Delay (d2), s/veh	4.4	0.5	0.0	0.0	2.0	1.9	0.9	0.0	0.0	0.3	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.3	1.7	0.0	0.0	4.1	4.3	2.2	0.0	0.0	0.9	0.0	0.0
Unsig. Movement Delay, s/veh		1.7	0.0	0.0	•••	1.0		0.0	0.0	0.0	0.0	0.0
LnGrp Delay(d),s/veh	31.3	4.4	2.7	0.0	10.5	10.4	25.3	0.0	0.0	23.2	0.0	0.0
LnGrp LOS	C	A	Α	Α	В	В	C	Α	Α	C	Α	Α
Approach Vol, veh/h		1029			1080			157			73	
Approach Delay, s/veh		6.7			10.5			25.3			23.2	
Approach LOS		Α			В			23.3 C			23.2 C	
Apploach EOS					Ь						C	
Timer - Assigned Phs	1	2		4	5	6		8				
Phs Duration (G+Y+Rc), s	0.0	46.3		13.5	8.7	37.7		13.5				
Change Period (Y+Rc), s	4.5	* 4.5		5.5	4.5	4.0		5.5				
Max Green Setting (Gmax), s	15.0	* 50		20.0	25.0	40.0		20.0				
Max Q Clear Time (g_c+I1), s	0.0	10.3		4.5	5.2	14.9		8.2				
Green Ext Time (p_c), s	0.0	23.7		0.2	0.2	18.8		0.4				
Intersection Summary												
HCM 6th Ctrl Delay			10.2									
HCM 6th LOS			В									
Notos												

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	† †	7	ሻ	↑ ↑			4			4	
Traffic Volume (vph)	165	1139	139	5	1173	18	121	25	7	42	24	124
Future Volume (vph)	165	1139	139	5	1173	18	121	25	7	42	24	124
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Storage Length (ft)	115		100	105		0	0		0	0		0
Storage Lanes	1		1	1		0	0		0	0		0
Taper Length (ft)	100			100			100			100		
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	1.00		0.98	1.00	1.00			1.00			0.99	
Frt			0.850		0.998			0.994			0.912	
Flt Protected	0.950			0.950				0.962			0.989	
Satd. Flow (prot)	1630	3228	1458	1630	3161	0	0	1625	0	0	1526	0
Flt Permitted	0.950	0220		0.950		•	•	0.529		•	0.910	
Satd. Flow (perm)	1629	3228	1426	1629	3161	0	0	890	0	0	1404	0
Right Turn on Red			Yes			Yes			Yes	-		Yes
Satd. Flow (RTOR)			95		2			2			75	
Link Speed (mph)		25			25			25			25	
Link Distance (ft)		468			302			365			210	
Travel Time (s)		12.8			8.2			10.0			5.7	
Confl. Peds. (#/hr)	2	12.0	1	1	0.2	2	5	10.0			0.7	5
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Heavy Vehicles (%)	2%	3%	2%	2%	5%	2%	2%	8%	2%	2%	2%	2%
Adj. Flow (vph)	176	1212	148	5	1248	19	129	27	7	45	26	132
Shared Lane Traffic (%)	110	1212	1.0		1210	10	120	_,	<u>'</u>	10	20	102
Lane Group Flow (vph)	176	1212	148	5	1267	0	0	163	0	0	203	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA
Median Width(ft)	L 14/ \	12	11171	L 14/ (12	1 1 1 1 1 1	L 14/ (0	141474	L 14/ (0	1 (1 () (
Link Offset(ft)		-12			0			0			4	
Crosswalk Width(ft)		72			42			32			30	
Two way Left Turn Lane		12			72			02			00	
Headway Factor	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
Number of Detectors	2	1.11	1.11	2	1	1.11	2	2	1.11	2	2	1.11
Detector Template	Left	Det25	Right	Left	Det25		Left				Side St	
Leading Detector (ft)	78	153	153	78	153		78	78		78	78	
Trailing Detector (ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Position(ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Size(ft)	16	16	16	16	16		16	16		16	16	
Detector 1 Type	CI+Ex	Cl+Ex	Cl+Ex	Cl+Ex	CI+Ex		Cl+Ex	Cl+Ex		CI+Ex	Cl+Ex	
Detector 1 Channel	CITLX	CITLX	CITLX	CITLX	CITLX		CITLX	CITLX		CITLX	CITLX	
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
• , ,	72	0.0	0.0	72	0.0		72	72		72		
Detector 2 Position(ft)											72 6	
Detector 2 Size(ft)	6			6 CL Ev			6	6		6		
Detector 2 Type	CI+Ex			CI+Ex			CI+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 2 Channel	0.0			0.0			0.0	0.0		0.0	0.0	
Detector 2 Extend (s)	0.0	N I A	D	0.0	N I A		0.0	0.0		0.0	0.0	
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	

Protected Phases 5 2 1 6 8 4 Permitted Phases 2 2 1 6 8 4 Detector Phase 5 2 2 1 6 8 8 4 4 Switch Phase Minimum Initial (s) 4.0 10.0 10.0 4.0 10.0 6.0 6.0 6.0 6.0 6.0 Minimum Split (s) 8.5 26.0 26.0 8.5 30.0 11.5 11.5 23.5 23.5 Total Split (s) 20.0 70.0 70.0 15.0 65.0 25.0 25.0 25.0 25.0 Total Split (%) 18.2% 63.6% 63.6% 13.6% 59.1% 22.7% 22.7% 22.7% 22.7% Maximum Green (s) 15.5 66.0 66.0 10.5 61.0 19.5 19.5 19.5 Yellow Time (s) 3.5 3.5 3.5 3.5 3.5 3.5 4.0 4.0 4.0 4.0 4.0 All-Red Time (s) 1.0 0.5 0.5 1.0 0.5 1.5 1.5 1.5 1.5 Lost Time Adjust (s) -0.5 0.0 0.0 -0.5 0.0 -1.5 Total Lost Time (s) 4.0 4.0 4.0 4.0 4.0 4.0 4.0 Lead/Lag Lag Lag Lag Lead Lead Lead-Lag Optimize? Vehicle Extension (s) 2.3 5.8 5.8 2.3 5.8 2.5 2.5 2.5 2.5 2.5		۶	→	•	•	←	•	4	†	/	-	ļ	4
Permitted Phases 2 2 1 6 8 4 4 4 Switch Phase 5 2 2 1 1 6 8 8 8 4 4 4 4 Switch Phase Minimum Initial (s) 4.0 10.0 10.0 4.0 10.0 6.0 6.0 6.0 6.0 6.0 Minimum Split (s) 8.5 26.0 26.0 8.5 30.0 11.5 11.5 23.5 23.5 Total Split (s) 20.0 70.0 70.0 15.0 65.0 25.0 25.0 25.0 25.0 25.0 Total Split (%) 18.2% 63.6% 63.6% 13.6% 59.1% 22.7% 22.7% 22.7% 22.7% 22.7% Maximum Green (s) 15.5 66.0 66.0 10.5 61.0 19.5 19.5 19.5 19.5 Yellow Time (s) 3.5 3.5 3.5 3.5 3.5 3.5 3.5 4.0 4.0 4.0 4.0 4.0 All-Red Time (s) 1.0 0.5 0.5 1.0 0.5 1.5 1.5 1.5 1.5 Lost Time Adjust (s) -0.5 0.0 0.0 -0.5 0.0 -1.5 -1.5 Total Lost Time (s) 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 Lead/Lag Lag Lag Lag Lag Lead Lead Lead Lead-Lag Optimize? Vehicle Extension (s) 2.3 5.8 5.8 2.3 5.8 2.5 2.5 2.5 2.5 2.5	Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Detector Phase 5 2 2 1 6 8 8 4 4 Switch Phase Minimum Initial (s) 4.0 10.0 10.0 4.0 10.0 6.0 6.0 6.0 6.0 Minimum Split (s) 8.5 26.0 26.0 8.5 30.0 11.5 11.5 23.5 23.5 Total Split (s) 20.0 70.0 70.0 15.0 65.0 25.0	Protected Phases	5	2		1	6			8			4	
Switch Phase Minimum Initial (s) 4.0 10.0 10.0 4.0 10.0 6.0 6.0 6.0 6.0 6.0 Minimum Split (s) 8.5 26.0 26.0 8.5 30.0 11.5 11.5 23.5 23.5 Total Split (s) 20.0 70.0 70.0 15.0 65.0 25.0 25.0 25.0 25.0 Total Split (%) 18.2% 63.6% 63.6% 13.6% 59.1% 22.7%	Permitted Phases							-					
Minimum Initial (s) 4.0 10.0 10.0 4.0 10.0 6.0 6.0 6.0 6.0 Minimum Split (s) 8.5 26.0 26.0 8.5 30.0 11.5 11.5 23.5 23.5 Total Split (s) 20.0 70.0 70.0 15.0 65.0 25.0 </td <td>Detector Phase</td> <td>5</td> <td>2</td> <td>2</td> <td>1</td> <td>6</td> <td></td> <td>8</td> <td>8</td> <td></td> <td>4</td> <td>4</td> <td></td>	Detector Phase	5	2	2	1	6		8	8		4	4	
Minimum Split (s) 8.5 26.0 26.0 8.5 30.0 11.5 11.5 23.5 23.5 Total Split (s) 20.0 70.0 70.0 15.0 65.0 25	Switch Phase												
Total Split (s) 20.0 70.0 70.0 15.0 65.0 25.0 25.0 25.0 25.0 Total Split (%) 18.2% 63.6% 63.6% 13.6% 59.1% 22.7% 22.7% 22.7% 22.7% Maximum Green (s) 15.5 66.0 66.0 10.5 61.0 19.5 19.5 19.5 Yellow Time (s) 3.5 3.5 3.5 3.5 4.0 4.0 4.0 4.0 All-Red Time (s) 1.0 0.5 0.5 1.0 0.5 1.5 1.5 1.5 1.5 Lost Time Adjust (s) -0.5 0.0 0.0 -0.5 0.0 -1.5 -1.5 Total Lost Time (s) 4.0 4.0 4.0 4.0 4.0 4.0 Lead/Lag Lag Lag Lead Lead Lead Lead-Lag Optimize? Vehicle Extension (s) 2.3 5.8 5.8 2.3 5.8 2.5 2.5 2.5 2.5													
Total Split (%) 18.2% 63.6% 63.6% 13.6% 59.1% 22.7% 22.7% 22.7% 22.7% Maximum Green (s) 15.5 66.0 66.0 10.5 61.0 19.5 19.5 19.5 Yellow Time (s) 3.5 3.5 3.5 3.5 4.0 4.0 4.0 4.0 All-Red Time (s) 1.0 0.5 0.5 1.0 0.5 1.5 1.5 1.5 1.5 Lost Time Adjust (s) -0.5 0.0 0.0 -0.5 0.0 -1.5 -1.5 Total Lost Time (s) 4.0 4.0 4.0 4.0 4.0 4.0 Lead/Lag Lag Lag Lead Lead Lead Lead-Lag Optimize? Vehicle Extension (s) 2.3 5.8 5.8 2.3 5.8 2.5 2.5 2.5 2.5													
Maximum Green (s) 15.5 66.0 66.0 10.5 61.0 19.5 19.5 19.5 19.5 Yellow Time (s) 3.5 3.5 3.5 3.5 4.0 4.0 4.0 4.0 All-Red Time (s) 1.0 0.5 0.5 1.0 0.5 1.5 1.5 1.5 1.5 Lost Time Adjust (s) -0.5 0.0 0.0 -0.5 0.0 -1.5 -1.5 -1.5 Total Lost Time (s) 4.0	Total Split (s)					65.0						25.0	
Yellow Time (s) 3.5 3.5 3.5 3.5 3.5 4.0 4.0 4.0 4.0 All-Red Time (s) 1.0 0.5 0.5 1.0 0.5 1.5	Total Split (%)					59.1%							
All-Red Time (s) 1.0 0.5 0.5 1.0 0.5 1.5 1.5 1.5 1.5 Lost Time Adjust (s) -0.5 0.0 0.0 -0.5 0.0 -1.5 -1.5 -1.5 Total Lost Time (s) 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 Lead/Lag Lag Lag Lag Lead Lead Lead Lead-Lag Optimize? Vehicle Extension (s) 2.3 5.8 5.8 2.3 5.8 2.5 2.5 2.5 2.5	Maximum Green (s)		66.0		10.5			19.5	19.5		19.5	19.5	
Lost Time Adjust (s) -0.5 0.0 0.0 -0.5 0.0 -1.5 -1.5 Total Lost Time (s) 4.0 4.0 4.0 4.0 4.0 4.0 4.0 Lead/Lag Lag Lag Lag Lead Lead Lead-Lag Optimize? Vehicle Extension (s) 2.3 5.8 5.8 2.3 5.8 2.5 2.5 2.5 2.5	Yellow Time (s)		3.5										
Total Lost Time (s) 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 Lead/Lag Lag Lag Lead Lead Lead-Lag Optimize? Vehicle Extension (s) 2.3 5.8 5.8 2.3 5.8 2.5 2.5 2.5 2.5	All-Red Time (s)	1.0	0.5	0.5	1.0	0.5		1.5	1.5		1.5	1.5	
Lead/Lag Lag Lag Lead Lead Lead-Lag Optimize? Vehicle Extension (s) 2.3 5.8 5.8 2.3 5.8 2.5 2.5 2.5 2.5	Lost Time Adjust (s)	-0.5	0.0	0.0	-0.5	0.0			-1.5			-1.5	
Lead-Lag Optimize? Vehicle Extension (s) 2.3 5.8 5.8 2.3 5.8 2.5 2.5 2.5	Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Vehicle Extension (s) 2.3 5.8 5.8 2.3 5.8 2.5 2.5 2.5	Lead/Lag	Lag	Lag	Lag	Lead	Lead							
\setminus /	Lead-Lag Optimize?												
	Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8		2.5	2.5		2.5	2.5	
Minimum Gap (s) 0.5 3.8 3.8 0.5 3.8 2.0 2.0 2.0 2.0	Minimum Gap (s)	0.5	3.8	3.8	0.5	3.8		2.0	2.0		2.0	2.0	
Time Before Reduce (s) 8.0 10.0 10.0 8.0 10.0 5.0 5.0 5.0	Time Before Reduce (s)	8.0	10.0	10.0	8.0	10.0		5.0	5.0		5.0	5.0	
Time To Reduce (s) 3.0 10.0 10.0 3.0 10.0 5.0 5.0 5.0	Time To Reduce (s)	3.0	10.0	10.0	3.0	10.0		5.0	5.0		5.0	5.0	
Recall Mode None C-Min C-Min None C-Min None None None None	Recall Mode	None	C-Min	C-Min	None	C-Min		None	None		None	None	
Walk Time (s) 7.0 7.0 7.0 7.0	Walk Time (s)		7.0	7.0		7.0					7.0	7.0	
Flash Dont Walk (s) 15.0 15.0 19.0 11.0	Flash Dont Walk (s)		15.0	15.0		19.0					11.0	11.0	
Pedestrian Calls (#/hr) 0 0 0 0	Pedestrian Calls (#/hr)		0	0		0					0	0	
Act Effct Green (s) 15.7 72.6 72.6 5.8 55.0 27.3 27.3	Act Effct Green (s)	15.7	72.6	72.6	5.8	55.0			27.3			27.3	
Actuated g/C Ratio 0.14 0.66 0.66 0.05 0.50 0.25 0.25	Actuated g/C Ratio	0.14	0.66	0.66	0.05	0.50			0.25			0.25	
v/c Ratio 0.76 0.57 0.15 0.06 0.80 0.73 0.50	v/c Ratio	0.76	0.57	0.15	0.06	0.80			0.73			0.50	
Control Delay 66.2 11.4 2.9 50.6 27.1 61.0 28.8	Control Delay	66.2	11.4	2.9	50.6	27.1			61.0			28.8	
Queue Delay 0.0 0.0 0.0 0.0 0.0 0.0 0.0	Queue Delay	0.0	0.0	0.0	0.0	0.0			0.0			0.0	
Total Delay 66.2 11.4 2.9 50.6 27.1 61.0 28.8	Total Delay	66.2	11.4	2.9	50.6	27.1			61.0			28.8	
LOS E B A D C E C		Е	В	Α	D	С			E			С	
Approach Delay 16.9 27.2 61.0 28.8	Approach Delay		16.9			27.2			61.0			28.8	
Approach LOS B C E C			В			С			Е			С	

Intersection Summary

Area Type: Other

Cycle Length: 110
Actuated Cycle Length: 110

Offset: 0 (0%), Referenced to phase 2:EBT and 6:WBT, Start of Green, Master Intersection

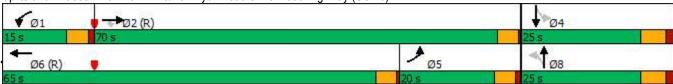
Natural Cycle: 80

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.80

Intersection Signal Delay: 24.0 Intersection LOS: C
Intersection Capacity Utilization 81.2% ICU Level of Service D

Analysis Period (min) 15



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Lane Group	EBL	EBT	EBR	WBL	WBT	NBT	SBT
Lane Group Flow (vph)	176	1212	148	5	1267	163	203
v/c Ratio	0.76	0.57	0.15	0.06	0.80	0.73	0.50
Control Delay	66.2	11.4	2.9	50.6	27.1	61.0	28.8
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	66.2	11.4	2.9	50.6	27.1	61.0	28.8
Queue Length 50th (ft)	118	195	11	3	378	107	78
Queue Length 95th (ft)	#224	297	37	16	417	#250	164
Internal Link Dist (ft)		388			222	285	130
Turn Bay Length (ft)	115		100	105			
Base Capacity (vph)	250	2130	973	163	1753	222	404
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.70	0.57	0.15	0.03	0.72	0.73	0.50
Intersection Summary							

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^↑	7	ሻ	∱ ∱			4			4	
Traffic Volume (vph)	165	1139	139	5	1173	18	121	25	7	42	24	124
Future Volume (vph)	165	1139	139	5	1173	18	121	25	7	42	24	124
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95			1.00			1.00	
Frpb, ped/bikes	1.00	1.00	0.98	1.00	1.00			1.00			0.99	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00			1.00			1.00	
Frt	1.00	1.00	0.85	1.00	1.00			0.99			0.91	
Flt Protected	0.95	1.00	1.00	0.95	1.00			0.96			0.99	
Satd. Flow (prot)	1630	3228	1426	1630	3160			1619			1527	
Flt Permitted	0.95	1.00	1.00	0.95	1.00			0.53			0.91	
Satd. Flow (perm)	1630	3228	1426	1630	3160			890			1405	
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	176	1212	148	5	1248	19	129	27	7	45	26	132
RTOR Reduction (vph)	0	0	35	0	1	0	0	2	0	0	56	0
Lane Group Flow (vph)	176	1212	113	5	1266	0	0	161	0	0	147	0
Confl. Peds. (#/hr)	2		1	1		2	5					5
Heavy Vehicles (%)	2%	3%	2%	2%	5%	2%	2%	8%	2%	2%	2%	2%
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Actuated Green, G (s)	18.8	69.0	69.0	1.2	51.4			25.8			25.8	
Effective Green, g (s)	19.3	69.0	69.0	1.7	51.4			27.3			27.3	
Actuated g/C Ratio	0.18	0.63	0.63	0.02	0.47			0.25			0.25	
Clearance Time (s)	4.5	4.0	4.0	4.5	4.0			5.5			5.5	
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8			2.5			2.5	
Lane Grp Cap (vph)	285	2024	894	25	1476			220			348	
v/s Ratio Prot	0.11	c0.38		0.00	c0.40							
v/s Ratio Perm			0.08					c0.18			0.10	
v/c Ratio	0.62	0.60	0.13	0.20	0.86			0.73			0.42	
Uniform Delay, d1	41.9	12.2	8.3	53.5	26.0			38.0			34.7	
Progression Factor	1.00	1.00	1.00	1.00	1.00			1.00			1.00	
Incremental Delay, d2	3.1	1.3	0.3	2.3	6.7			11.3			0.6	
Delay (s)	45.1	13.6	8.6	55.8	32.7			49.3			35.3	
Level of Service	D	В	Α	Е	С			D			D	
Approach Delay (s)		16.7			32.8			49.3			35.3	
Approach LOS		В			С			D			D	
Intersection Summary												
HCM 2000 Control Delay			26.0	HCM 2000 Level of Service					С			
HCM 2000 Volume to Capac	ity ratio		0.79									
Actuated Cycle Length (s)	` '				\ <i>,</i>				12.0			
Intersection Capacity Utilizati	ion		81.2%	IC	U Level o	of Service			D			
Analysis Period (min)			15									

c Critical Lane Group

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	ň	ħβ			4			4	
Traffic Volume (veh/h)	165	1139	139	5	1173	18	121	25	7	42	24	124
Future Volume (veh/h)	165	1139	139	5	1173	18	121	25	7	42	24	124
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	0.99		0.99	1.00		0.99
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1723	1709	1723	1723	1682	1682	1641	1641	1641	1723	1723	1723
Adj Flow Rate, veh/h	176	1212	114	5	1248	18	129	27	5	45	26	72
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Percent Heavy Veh, %	2	3	2	2	5	5	8	8	8	2	2	2
Cap, veh/h	328	2278	1023	16	1664	24	212	37	6	109	71	139
Arrive On Green	0.20	0.70	0.70	0.01	0.52	0.52	0.16	0.18	0.16	0.16	0.18	0.16
Sat Flow, veh/h	1641	3247	1458	1641	3224	46	875	211	35	379	404	794
Grp Volume(v), veh/h	176	1212	114	5	618	648	161	0	0	143	0	0
Grp Sat Flow(s),veh/h/ln	1641	1624	1458	1641	1598	1673	1121	0	0	1577	0	0
Q Serve(g_s), s	10.6	19.6	2.8	0.3	33.6	33.6	6.7	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(g_c), s	10.6	19.6	2.8	0.3	33.6	33.6	15.8	0.0	0.0	9.1	0.0	0.0
Prop In Lane	1.00		1.00	1.00	00.0	0.03	0.80	0.0	0.03	0.31	0.0	0.50
Lane Grp Cap(c), veh/h	328	2278	1023	16	825	864	240	0	0	298	0	0
V/C Ratio(X)	0.54	0.53	0.11	0.31	0.75	0.75	0.67	0.00	0.00	0.48	0.00	0.00
Avail Cap(c_a), veh/h	328	2278	1023	164	886	928	260	0	0	321	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	39.5	7.8	5.3	54.1	21.0	21.0	45.0	0.0	0.0	41.8	0.0	0.0
Incr Delay (d2), s/veh	1.2	0.9	0.2	6.7	6.2	5.9	5.3	0.0	0.0	0.9	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	4.4	6.5	0.9	0.2	13.6	14.3	4.8	0.0	0.0	3.7	0.0	0.0
Unsig. Movement Delay, s/veh		0.0	0.0	0.2	10.0	14.0	4.0	0.0	0.0	0.7	0.0	0.0
LnGrp Delay(d),s/veh	40.7	8.7	5.5	60.8	27.2	27.0	50.3	0.0	0.0	42.7	0.0	0.0
LnGrp LOS	D	Α	Α	60.0 E	C C	27.0 C	D	Α	Α	72.7 D	Α	Α
Approach Vol, veh/h		1502			1271			161			143	
Approach Delay, s/veh		12.2			27.2			50.3			42.7	
		12.2 B			21.2 C			50.5 D			42.7 D	
Approach LOS		D			C			U			U	
Timer - Assigned Phs	1	2		4	5	6		8				
Phs Duration (G+Y+Rc), s	5.1	81.7		23.3	26.0	60.8		23.3				
Change Period (Y+Rc), s	4.5	* 4.5		5.5	4.5	4.0		5.5				
Max Green Setting (Gmax), s	10.5	* 66		19.5	15.5	61.0		19.5				
Max Q Clear Time (g_c+I1), s	2.3	21.6		11.1	12.6	35.6		17.8				
Green Ext Time (p_c), s	0.0	34.6		0.3	0.2	21.2		0.1				
Intersection Summary												
HCM 6th Ctrl Delay			21.8									
HCM 6th LOS			C C									
Notos												

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ň	^	7	7	∱ ∱			4			4	
Traffic Volume (vph)	64	982	39	0	1106	19	160	4	2	25	8	159
Future Volume (vph)	64	982	39	0	1106	19	160	4	2	25	8	159
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Storage Length (ft)	115		100	105		0	0		0	0		0
Storage Lanes	1		1	1		0	0		0	0		0
Taper Length (ft)	100			100			100			100		
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor			0.98		1.00			1.00			0.99	
Frt			0.850		0.997			0.998			0.888	
Flt Protected	0.950							0.954			0.994	
Satd. Flow (prot)	1568	2942	1403	1716	3158	0	0	1603	0	0	1455	0
Flt Permitted	0.950							0.515			0.947	
Satd. Flow (perm)	1568	2942	1372	1716	3158	0	0	864	0	0	1386	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)			77		2			1			173	
Link Speed (mph)		25			25			25			25	
Link Distance (ft)		468			302			365			210	
Travel Time (s)		12.8			8.2			10.0			5.7	
Confl. Peds. (#/hr)			1	1			2					2
Confl. Bikes (#/hr)						1						
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	13%	6%	2%	5%	2%	4%	2%	2%	24%	2%	2%
Adj. Flow (vph)	70	1067	42	0	1202	21	174	4	2	27	9	173
Shared Lane Traffic (%)												
Lane Group Flow (vph)	70	1067	42	0	1223	0	0	180	0	0	209	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA
Median Width(ft)		12			12			0			0	
Link Offset(ft)		-12			0			0			4	
Crosswalk Width(ft)		72			42			32			30	
Two way Left Turn Lane												
Headway Factor	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
Number of Detectors	2	1	1	2	1		2	2		2	2	
Detector Template	Left	Det25	Right	Left	Det25		Left	Side St		Left	Side St	
Leading Detector (ft)	78	153	153	78	153		78	78		78	78	
Trailing Detector (ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Position(ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Size(ft)	16	16	16	16	16		16	16		16	16	
Detector 1 Type	CI+Ex	Cl+Ex	Cl+Ex	CI+Ex	CI+Ex		CI+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 1 Channel												
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 2 Position(ft)	72			72			72	72		72	72	
Detector 2 Size(ft)	6			6			6	6		6	6	
Detector 2 Type	CI+Ex			CI+Ex			Cl+Ex	CI+Ex		Cl+Ex	CI+Ex	
Detector 2 Channel	J. · L∧			J. LA			5. · LX	OI - EX		51 · LX	O L.	
Detector 2 Extend (s)	0.0			0.0			0.0	0.0		0.0	0.0	
= 100001 2 Exterior (8)	0.0			0.0			0.0	0.0		0.0	0.0	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Detector Phase	5	2	2	1	6		8	8		4	4	
Switch Phase												
Minimum Initial (s)	4.0	10.0	10.0	4.0	10.0		6.0	6.0		6.0	6.0	
Minimum Split (s)	8.5	26.0	26.0	8.5	30.0		11.5	11.5		23.5	23.5	
Total Split (s)	29.5	54.0	54.0	19.5	44.0		25.5	25.5		25.5	25.5	
Total Split (%)	29.8%	54.5%	54.5%	19.7%	44.4%		25.8%	25.8%		25.8%	25.8%	
Maximum Green (s)	25.0	50.0	50.0	15.0	40.0		20.0	20.0		20.0	20.0	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5		4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	0.5	0.5	1.0	0.5		1.5	1.5		1.5	1.5	
Lost Time Adjust (s)	-0.5	0.0	0.0	-0.5	0.0			-1.5			-1.5	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lead/Lag	Lag	Lag	Lag	Lead	Lead							
Lead-Lag Optimize?												
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8		2.5	2.5		2.5	2.5	
Minimum Gap (s)	0.5	3.8	3.8	0.5	3.8		2.0	2.0		2.0	2.0	
Time Before Reduce (s)	8.0	10.0	10.0	8.0	10.0		5.0	5.0		5.0	5.0	
Time To Reduce (s)	3.0	10.0	10.0	3.0	10.0		5.0	5.0		5.0	5.0	
Recall Mode	None	Min	Min	None	Min		None	None		None	None	
Walk Time (s)		7.0	7.0		7.0					7.0	7.0	
Flash Dont Walk (s)		15.0	15.0		19.0					11.0	11.0	
Pedestrian Calls (#/hr)		0	0		0					0	0	
Act Effct Green (s)	8.8	46.5	46.5		36.2			22.1			22.1	
Actuated g/C Ratio	0.11	0.61	0.61		0.47			0.29			0.29	
v/c Ratio	0.39	0.60	0.05		0.82			0.72			0.40	
Control Delay	40.5	10.4	0.5		23.8			47.8			9.5	
Queue Delay	0.0	0.0	0.0		0.0			0.0			0.0	
Total Delay	40.5	10.4	0.5		23.8			47.8			9.5	
LOS	D	В	Α		С			D			А	
Approach Delay		11.9			23.8			47.8			9.5	
Approach LOS		В			С			D			Α	
Intersection Summary												

Intersection Summary

Area Type: Other

Cycle Length: 99

Actuated Cycle Length: 76.8)

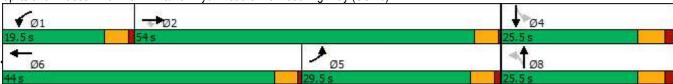
Natural Cycle: 65

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.82

Intersection Signal Delay: 19.2 Intersection LOS: B
Intersection Capacity Utilization 73.9% ICU Level of Service D

Analysis Period (min) 15



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Lane Group	EBL	EBT	EBR	WBT	NBT	SBT
Lane Group Flow (vph)	70	1067	42	1223	180	209
v/c Ratio	0.39	0.60	0.05	0.82	0.72	0.40
Control Delay	40.5	10.4	0.5	23.8	47.8	9.5
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	40.5	10.4	0.5	23.8	47.8	9.5
Queue Length 50th (ft)	34	143	0	264	86	14
Queue Length 95th (ft)	74	193	4	385	#210	73
Internal Link Dist (ft)		388		222	285	130
Turn Bay Length (ft)	115		100			
Base Capacity (vph)	535	2063	985	1692	249	522
Starvation Cap Reductn	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0
Reduced v/c Ratio	0.13	0.52	0.04	0.72	0.72	0.40
Intersection Summary						

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	^	7	ሻ	↑ ↑			4			4	
Traffic Volume (vph)	64	982	39	0	1106	19	160	4	2	25	8	159
Future Volume (vph)	64	982	39	0	1106	19	160	4	2	25	8	159
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)	4.0	4.0	4.0		4.0			4.0			4.0	
Lane Util. Factor	1.00	0.95	1.00		0.95			1.00			1.00	
Frpb, ped/bikes	1.00	1.00	0.98		1.00			1.00			0.99	
Flpb, ped/bikes	1.00	1.00	1.00		1.00			1.00			1.00	
Frt	1.00	1.00	0.85		1.00			1.00			0.89	
FIt Protected	0.95	1.00	1.00		1.00			0.95			0.99	
Satd. Flow (prot)	1568	2942	1373		3159			1601			1455	
Flt Permitted	0.95	1.00	1.00		1.00			0.52			0.95	
Satd. Flow (perm)	1568	2942	1373		3159			865			1387	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	70	1067	42	0	1202	21	174	4	2	27	9	173
RTOR Reduction (vph)	0	0	16	0	1	0	0	1	0	0	124	0
Lane Group Flow (vph)	70	1067	26	0	1222	0	0	179	0	0	85	0
Confl. Peds. (#/hr)			1	1			2					2
Confl. Bikes (#/hr)						1						
Heavy Vehicles (%)	6%	13%	6%	2%	5%	2%	4%	2%	2%	24%	2%	2%
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Actuated Green, G (s)	6.9	47.6	47.6		36.2			20.6			20.6	
Effective Green, g (s)	7.4	47.6	47.6		36.2			22.1			22.1	
Actuated g/C Ratio	0.10	0.61	0.61		0.47			0.28			0.28	
Clearance Time (s)	4.5	4.0	4.0		4.0			5.5			5.5	
Vehicle Extension (s)	2.3	5.8	5.8		5.8			2.5			2.5	
Lane Grp Cap (vph)	149	1802	841		1471			246			394	
v/s Ratio Prot	0.04	c0.36	• • •		c0.39			•				
v/s Ratio Perm	0.0	00.00	0.02		C 0.00			c0.21			0.06	
v/c Ratio	0.47	0.59	0.03		0.83			0.73			0.22	
Uniform Delay, d1	33.3	9.1	5.9		18.1			25.1			21.2	
Progression Factor	1.00	1.00	1.00		1.00			1.00			1.00	
Incremental Delay, d2	1.4	0.9	0.0		4.8			9.7			0.2	
Delay (s)	34.7	10.1	6.0		22.9			34.8			21.4	
Level of Service	С	В	A		C			C			С	
Approach Delay (s)		11.4			22.9			34.8			21.4	
Approach LOS		В			C			С			С	
Intersection Summary												
HCM 2000 Control Delay			18.7	Н	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capac	city ratio		0.79									
Actuated Cycle Length (s)			77.7	S	um of lost	time (s)			12.0			
Intersection Capacity Utilizat	ion		73.9%	IC	CU Level of	of Service			D			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	ሻ	∱ ∱			4			4	
Traffic Volume (veh/h)	64	982	39	0	1106	19	160	4	2	25	8	159
Future Volume (veh/h)	64	982	39	0	1106	19	160	4	2	25	8	159
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		0.98	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1668	1573	1668	1723	1682	1682	1723	1723	1723	1723	1723	1723
Adj Flow Rate, veh/h	70	1067	9	0	1202	20	174	4	1	27	9	39
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	6	13	6	2	5	5	2	2	2	2	2	2
Cap, veh/h	100	2065	976	3	1842	31	356	6	1	146	66	146
Arrive On Green	0.06	0.69	0.69	0.00	0.57	0.57	0.15	0.17	0.15	0.15	0.17	0.15
Sat Flow, veh/h	1589	2988	1413	1641	3215	53	1398	32	8	392	378	834
Grp Volume(v), veh/h	70	1067	9	0	597	625	179	0	0	75	0	0
Grp Sat Flow(s),veh/h/ln	1589	1494	1413	1641	1598	1671	1438	0	0	1603	0	0
Q Serve(g_s), s	2.7	10.9	0.1	0.0	16.2	16.2	4.8	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(g_c), s	2.7	10.9	0.1	0.0	16.2	16.2	7.5	0.0	0.0	2.7	0.0	0.0
Prop In Lane	1.00		1.00	1.00		0.03	0.97		0.01	0.36		0.52
Lane Grp Cap(c), veh/h	100	2065	976	3	916	958	329	0	0	319	0	0
V/C Ratio(X)	0.70	0.52	0.01	0.00	0.65	0.65	0.54	0.00	0.00	0.23	0.00	0.00
Avail Cap(c_a), veh/h	639	2357	1114	401	1008	1054	553	0	0	560	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	0.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	29.1	4.7	3.0	0.0	9.2	9.2	25.2	0.0	0.0	23.3	0.0	0.0
Incr Delay (d2), s/veh	5.4	0.7	0.0	0.0	2.7	2.6	1.0	0.0	0.0	0.3	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.2	2.5	0.0	0.0	5.3	5.5	2.7	0.0	0.0	1.0	0.0	0.0
Unsig. Movement Delay, s/veh												
LnGrp Delay(d),s/veh	34.5	5.4	3.1	0.0	12.0	11.9	26.3	0.0	0.0	23.5	0.0	0.0
LnGrp LOS	С	Α	Α	Α	В	В	С	Α	Α	С	Α	Α
Approach Vol, veh/h		1146			1222			179			75	
Approach Delay, s/veh		7.1			11.9			26.3			23.5	
Approach LOS		Α			В			С			С	
	1	2		4	5	6		8				
Timer - Assigned Phs	•					40.3						
Phs Duration (G+Y+Rc), s	0.0	48.3 * 4.5		15.1	8.0	40.3		15.1 5.5				
Change Period (Y+Rc), s	4.5			5.5	4.5							
Max Green Setting (Gmax), s	15.0	* 50		20.0	25.0	40.0		20.0				
Max Q Clear Time (g_c+l1), s	0.0	12.9		4.7	4.7	18.2		9.5				
Green Ext Time (p_c), s	0.0	25.7		0.2	0.2	18.2		0.5				
Intersection Summary												
HCM 6th Ctrl Delay			11.1									
HCM 6th LOS			В									
Notos												

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	^	7	ሻ	∱ }			4			4	
Traffic Volume (vph)	178	1292	158	6	1331	19	137	28	8	45	27	118
Future Volume (vph)	178	1292	158	6	1331	19	137	28	8	45	27	118
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Storage Length (ft)	115		100	105		0	0		0	0		0
Storage Lanes	1		1	1		0	0		0	0		0
Taper Length (ft)	100		•	100		•	100		•	100		
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	1.00	0.00	0.98	1.00	1.00	0.00	1.00	1.00	1.00	1.00	0.99	1.00
Frt	1.00		0.850	1.00	0.998			0.993			0.916	
Flt Protected	0.950		0.000	0.950	0.000			0.962			0.988	
Satd. Flow (prot)	1630	3228	1458	1630	3161	0	0	1623	0	0	1532	0
Flt Permitted	0.950	OLLO	1 100	0.950	0101	•	•	0.512		J	0.905	v
Satd. Flow (perm)	1629	3228	1426	1629	3161	0	0	861	0	0	1404	0
Right Turn on Red	1023	0220	Yes	1023	0101	Yes	U	001	Yes	O .	1707	Yes
Satd. Flow (RTOR)			95		2	100		2	100		66)	100
Link Speed (mph)		25			25			25			25	
Link Distance (ft)		468			302			365			210	
Travel Time (s)		12.8			8.2			10.0			5.7	
Confl. Peds. (#/hr)	2	12.0	1	1	0.2	2	5	10.0			0.1	5
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Heavy Vehicles (%)	2%	3%	2%	2%	5%	2%	2%	8%	2%	2%	2%	2%
Adj. Flow (vph)	189	1374	168	6	1416	20	146	30	9	48	29	126
Shared Lane Traffic (%)	103	1074	100		1710	20	170	30	,	70	25	120
Lane Group Flow (vph)	189	1374	168	6	1436	0	0	185	0	0	203	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA
Median Width(ft)		12			12	17107		0			0	1117
Link Offset(ft)		-12			0			0			4	
Crosswalk Width(ft)		72			42			32			30	
Two way Left Turn Lane								V-				
Headway Factor	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
Number of Detectors	2	1	1	2	1		2	2		2	2	
Detector Template	Left	Det25	Right	Left	Det25			Side St			Side St	
Leading Detector (ft)	78	153	153	78	153		78	78		78	78	
Trailing Detector (ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Position(ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Size(ft)	16	16	16	16	16		16	16		16	16	
Detector 1 Type	CI+Ex	Cl+Ex	Cl+Ex	CI+Ex	CI+Ex		CI+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 1 Channel												
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 2 Position(ft)	72			72			72	72		72	72	
Detector 2 Size(ft)	6			6			6	6		6	6	
Detector 2 Type	CI+Ex			CI+Ex			CI+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 2 Channel	J			J. L A			J/(J. L.		J. L ,\	J. LA	
Detector 2 Extend (s)	0.0			0.0			0.0	0.0		0.0	0.0	
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
. 3111 1370	1 100	1 4/-1	. 0.111	1 101	14/7		. 0.111	14/-1		. 01111	1 1/-1	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Detector Phase	5	2	2	1	6		8	8		4	4	
Switch Phase												
Minimum Initial (s)	4.0	10.0	10.0	4.0	10.0		6.0	6.0		6.0	6.0	
Minimum Split (s)	8.5	26.0	26.0	8.5	30.0		11.5	11.5		23.5	23.5	
Total Split (s)	20.0	70.0	70.0	15.0	65.0		25.0	25.0		25.0	25.0	
Total Split (%)	18.2%	63.6%	63.6%	13.6%	59.1%		22.7%	22.7%		22.7%	22.7%	
Maximum Green (s)	15.5	66.0	66.0	10.5	61.0		19.5	19.5		19.5	19.5	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5		4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	0.5	0.5	1.0	0.5		1.5	1.5		1.5	1.5	
Lost Time Adjust (s)	-0.5	0.0	0.0	-0.5	0.0			-1.5			-1.5	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lead/Lag	Lag	Lag	Lag	Lead	Lead							
Lead-Lag Optimize?												
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8		2.5	2.5		2.5	2.5	
Minimum Gap (s)	0.5	3.8	3.8	0.5	3.8		2.0	2.0		2.0	2.0	
Time Before Reduce (s)	8.0	10.0	10.0	8.0	10.0		5.0	5.0		5.0	5.0	
Time To Reduce (s)	3.0	10.0	10.0	3.0	10.0		5.0	5.0		5.0	5.0	
Recall Mode	None	C-Min	C-Min	None	C-Min		None	None		None	None	
Walk Time (s)		7.0	7.0		7.0					7.0	7.0	
Flash Dont Walk (s)		15.0	15.0		19.0					11.0	11.0	
Pedestrian Calls (#/hr)		0	0		0					0	0	
Act Effct Green (s)	15.5	75.3	75.3	5.8	58.0			24.5			24.5	
Actuated g/C Ratio	0.14	0.68	0.68	0.05	0.53			0.22			0.22	
v/c Ratio	0.83	0.62	0.17	0.07	0.86			0.96			0.56	
Control Delay	73.8	11.2	3.1	50.8	28.6			100.2			33.4	
Queue Delay	0.0	0.0	0.0	0.0	0.0			0.0			0.0	
Total Delay	73.8	11.2	3.1	50.8	28.6			100.2			33.4	
LOS	Е	В	Α	D	С			F			С	
Approach Delay		17.3			28.7			100.2			33.4	
Approach LOS		В			С			F			С	

Intersection Summary

Area Type: Other

Cycle Length: 110
Actuated Cycle Length: 110

Offset: 0 (0%), Referenced to phase 2:EBT and 6:WBT, Start of Green, Master Intersection

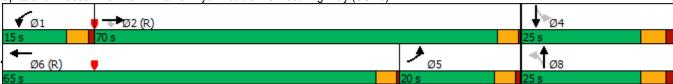
Natural Cycle: 90

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.96

Intersection Signal Delay: 27.1 Intersection LOS: C
Intersection Capacity Utilization 87.9% ICU Level of Service E

Analysis Period (min) 15



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Lane Group	EBL	EBT	EBR	WBL	WBT	NBT	SBT
Lane Group Flow (vph)	189	1374	168	6	1436	185	203
v/c Ratio	0.83	0.62	0.17	0.07	0.86	0.96	0.56
Control Delay	73.8	11.2	3.1	50.8	28.6	100.2	33.4
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	73.8	11.2	3.1	50.8	28.6	100.2	33.4
Queue Length 50th (ft)	129	201	12	4	426	~150	89
Queue Length 95th (ft)	#247	369	44	18	517	#295	171
Internal Link Dist (ft)		388			222	285	130
Turn Bay Length (ft)	115		100	105			
Base Capacity (vph)	241	2210	1006	163	1753	193	364
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.78	0.62	0.17	0.04	0.82	0.96	0.56

Intersection Summary

Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	7	∱ β			4			44	
Traffic Volume (vph)	178	1292	158	6	1331	19	137	28	8	45	27	118
Future Volume (vph)	178	1292	158	6	1331	19	137	28	8	45	27	118
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95			1.00			1.00	
Frpb, ped/bikes	1.00	1.00	0.98	1.00	1.00			1.00			0.99	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00			1.00			1.00	
Frt	1.00	1.00	0.85	1.00	1.00			0.99			0.92	
Flt Protected	0.95	1.00	1.00	0.95	1.00			0.96			0.99	
Satd. Flow (prot)	1630	3228	1426	1630	3160			1618			1533	
FIt Permitted	0.95	1.00	1.00	0.95	1.00			0.51			0.90	
Satd. Flow (perm)	1630	3228	1426	1630	3160			861			1403	
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	189	1374	168	6	1416	20	146	30	9	48	29	126
RTOR Reduction (vph)	0	0	33	0	1 1	0	0	2	0	0	51	0
Lane Group Flow (vph)	189	1374	135	6	1435	0	0	183	0	0	152	0
Confl. Peds. (#/hr)	2	1314	100	1	1400	2	5	100	U	U	102	5
Heavy Vehicles (%)	2%	3%	2%	2%	5%	2%	2%	8%	2%	2%	2%	2%
Turn Type					NA	Z /0		NA	Z /0	Perm	NA	2 /0
Protected Phases	Prot 5	NA 2	Perm	Prot 1	6		Perm	8		Pellii	1NA 4	
Permitted Phases	3	2	2	ı	U		8	0		4	4	
Actuated Green, G (s)	18.6	71.7	71.7	1.3	54.4		0	23.0		4	23.0	
. ,	19.1	71.7	71.7	1.8	54.4			24.5			24.5	
Effective Green, g (s)	0.17	0.65	0.65	0.02	0.49			0.22			0.22	
Actuated g/C Ratio	4.5		4.0	4.5				5.5			5.5	
Clearance Time (s)		4.0			4.0							
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8			2.5			2.5	
Lane Grp Cap (vph)	283	2104	929	26	1562			191			312	
v/s Ratio Prot	0.12	c0.43		0.00	c0.45							
v/s Ratio Perm			0.09					c 0.21			0.11	
v/c Ratio	0.67	0.65	0.15	0.23	0.92			0.96			0.49	
Uniform Delay, d1	42.5	11.6	7.4	53.4	25.8			42.3			37.3	
Progression Factor	1.00	1.00	1.00	1.00	1.00			1.00			1.00	
Incremental Delay, d2	5.0	1.6	0.3	2.6	10.2			53.5			0.9	
Delay (s)	47.5	13.2	7.7	56.1	35.9			95.8			38.1	
Level of Service	D	В	Α	Е	D			F			D	
Approach Delay (s)		16.4			36.0			95.8			38.1	
Approach LOS		В			D			F			D	
Intersection Summary												
HCM 2000 Control Delay			29.7	H	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capaci	ity ratio		0.89									
Actuated Cycle Length (s)	•		110.0	S	um of lost	time (s)			12.0			
Intersection Capacity Utilizati	on		87.9%		CU Level o				Е			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	75	^	7	ሻ	↑ ↑			4			4	
Traffic Volume (veh/h)	178	1292	158	6	1331	19	137	28	8	45	27	118
Future Volume (veh/h)	178	1292	158	6	1331	19	137	28	8	45	27	118
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	0.99		0.99	1.00		0.99
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1723	1709	1723	1723	1682	1682	1641	1641	1641	1723	1723	1723
Adj Flow Rate, veh/h	189	1374	136	6	1416	19	146	30	7	48	29	72
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Percent Heavy Veh, %	2	3	2	2	5	5	8	8	8	2	2	2
Cap, veh/h	264	2224	998	17	1740	23	227	37	8	120	79	146
Arrive On Green	0.16	0.68	0.68	0.01	0.54	0.54	0.18	0.19	0.18	0.18	0.19	0.18
Sat Flow, veh/h	1641	3247	1458	1641	3228	43	882	194	43	401	414	763
Grp Volume(v), veh/h	189	1374	136	6	700	735	183	0	0	149	0	0
Grp Sat Flow(s), veh/h/ln	1641	1624	1458	1641	1598	1674	1118	0	0	1579	0	0
Q Serve(g_s), s	12.0	25.4	3.6	0.4	39.6	39.7	8.6	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(g_c), s	12.0	25.4	3.6	0.4	39.6	39.7	18.0	0.0	0.0	9.4	0.0	0.0
Prop In Lane	1.00	20.4	1.00	1.00	05.0	0.03	0.80	0.0	0.04	0.32	0.0	0.48
Lane Grp Cap(c), veh/h	264	2224	998	17	861	902	257	0	0.04	323	0	0.40
V/C Ratio(X)	0.72	0.62	0.14	0.34	0.81	0.81	0.71	0.00	0.00	0.46	0.00	0.00
Avail Cap(c_a), veh/h	264	2224	998	164	886	928	257	0.00	0.00	323	0.00	0.00
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	43.7	9.5	6.0	54.0	20.8	20.8	44.6	0.0	0.00	40.3	0.0	0.00
Incr Delay (d2), s/veh	8.1	1.3	0.3	7.0	8.3	8.0	8.4	0.0	0.0	0.8	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	5.5	8.7	1.1	0.0	16.2	17.0	5.6	0.0	0.0	3.8	0.0	0.0
Unsig. Movement Delay, s/veh		0.7	1.1	0.2	10.2	17.0	5.0	0.0	0.0	3.0	0.0	0.0
		10.0	6.3	61.0	20.4	20.0	E2 0	0.0	0.0	41.1	0.0	0.0
LnGrp Delay(d),s/veh	51.9	10.8		61.0	29.1	28.8	53.0	0.0	0.0		0.0	0.0
LnGrp LOS	D	В	A	E	<u>C</u>	С	D	A	A	D	A	A
Approach Vol, veh/h		1699			1441			183			149	
Approach Delay, s/veh		15.0			29.1			53.0			41.1	
Approach LOS		В			С			D			D	
Timer - Assigned Phs	1	2		4	5	6		8				
Phs Duration (G+Y+Rc), s	5.2	79.8		25.0	21.7	63.3		25.0				
Change Period (Y+Rc), s	4.5	* 4.5		5.5	4.5	4.0		5.5				
Max Green Setting (Gmax), s	10.5	* 66		19.5	15.5	61.0		19.5				
Max Q Clear Time (g_c+l1), s	2.4	27.4		11.4	14.0	41.7		20.0				
Green Ext Time (p_c), s	0.0	33.5		0.3	0.1	17.6		0.0				
	,,,							7.0				
Intersection Summary			040									
HCM 6th LOS			24.0									
HCM 6th LOS			C									
Notes												

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	*	^	7	ሻ	† }			4			4	
Traffic Volume (vph)	88	982	39	0	1106	22	160	4	2	26	8	166
Future Volume (vph)	88	982	39	0	1106	22	160	4	2	26	8	166
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Storage Length (ft)	115		100	105		0	0		0	0		0
Storage Lanes	1		1	1		0	0		0	0		0
Taper Length (ft)	100			100		_	100		-	100		•
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor		0.00	0.98		1.00	0.00		1.00			0.99	
Frt			0.850		0.997			0.998			0.888	
Flt Protected	0.950		0.000		0.00			0.954			0.994	
Satd. Flow (prot)	1568	2942	1403	1716	3158	0	0	1603	0	0	1455	0
Flt Permitted	0.950	20 12	1100	11 10	0.00			0.499	· ·		0.946	
Satd. Flow (perm)	1568	2942	1372	1716	3158	0	0	837	0	0	1385	0
Right Turn on Red	1000	2072	Yes	17 10	0100	Yes	· ·	001	Yes	O .	1000	Yes
Satd. Flow (RTOR)			77		2	100		1	100		180	100
Link Speed (mph)		25	•		25			25			25	
Link Opeca (mpn) Link Distance (ft)		468			302			365			210	
Travel Time (s)		12.8			8.2			10.0			5.7	
Confl. Peds. (#/hr)		12.0	1	1	0.2		2	10.0			0.1	2
Confl. Bikes (#/hr)						1	2					2
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	13%	6%	2%	5%	2%	4%	2%	2%	24%	2%	2%
Adj. Flow (vph)	96	1067	42	0	1202	24	174	4	2	28	9	180
Shared Lane Traffic (%)	30	1001	72	U	1202	27	117	7		20	3	100
Lane Group Flow (vph)	96	1067	42	0	1226	0	0	180	0	0	217	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	RNA	L NA	R NA	R NA
Median Width(ft)	LINA	12	13 13/3	LIVA	12	13 13/3	LIVA	0	13.13/3	LINA	0	IX IV/X
Link Offset(ft)		-12			0			0			4	
Crosswalk Width(ft)		72			42			32			30	
Two way Left Turn Lane		12			72			52			30	
Headway Factor	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
Number of Detectors	2	1.11	1.11	2	1.11	1.11	2	2	1.11	2	2	1.11
Detector Template	Left	Det25	Right	Left	Det25			Side St			Side St	
Leading Detector (ft)	78	153	153	78	153		78	78		78	78	
Trailing Detector (ft)	2	137	137	2	137		2	2		2	2	
	2	137	137	2	137		2	2		2	2	
Detector 1 Position(ft) Detector 1 Size(ft)	16	16	16	16	16		16	16		16	16	
` ,	CI+Ex	Cl+Ex	Cl+Ex	Cl+Ex	Cl+Ex		Cl+Ex	Cl+Ex		Cl+Ex	CI+Ex	
Detector 1 Type Detector 1 Channel	CI+EX	CI+EX	CI+EX	CI+EX	UI+EX		CI+EX	UI+EX		UI+⊑X	UI+⊑X	
	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 2 Position(ft)	72			72			72	72		72	72	
Detector 2 Size(ft)	6			6			6	6		6	6	
Detector 2 Type	CI+Ex			Cl+Ex			Cl+Ex	Cl+Ex		Cl+Ex	CI+Ex	
Detector 2 Channel												
Detector 2 Extend (s)	0.0			0.0			0.0	0.0		0.0	0.0	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Detector Phase	5	2	2	1	6		8	8		4	4	
Switch Phase												
Minimum Initial (s)	4.0	10.0	10.0	4.0	10.0		6.0	6.0		6.0	6.0	
Minimum Split (s)	8.5	26.0	26.0	8.5	30.0		11.5	11.5		23.5	23.5	
Total Split (s)	29.5	54.0	54.0	19.5	44.0		25.5	25.5		25.5	25.5	
Total Split (%)	29.8%	54.5%	54.5%	19.7%	44.4%		25.8%	25.8%		25.8%	25.8%	
Maximum Green (s)	25.0	50.0	50.0	15.0	40.0		20.0	20.0		20.0	20.0	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5		4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	0.5	0.5	1.0	0.5		1.5	1.5		1.5	1.5	
Lost Time Adjust (s)	-0.5	0.0	0.0	-0.5	0.0			-1.5			-1.5	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lead/Lag	Lag	Lag	Lag	Lead	Lead							
Lead-Lag Optimize?												
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8		2.5	2.5		2.5	2.5	
Minimum Gap (s)	0.5	3.8	3.8	0.5	3.8		2.0	2.0		2.0	2.0	
Time Before Reduce (s)	8.0	10.0	10.0	8.0	10.0		5.0	5.0		5.0	5.0	
Time To Reduce (s)	3.0	10.0	10.0	3.0	10.0		5.0	5.0		5.0	5.0	
Recall Mode	None	Min	Min	None	Min		None	None		None	None	
Walk Time (s)		7.0	7.0		7.0					7.0	7.0	
Flash Dont Walk (s)		15.0	15.0		19.0					11.0	11.0	
Pedestrian Calls (#/hr)		0	0		0					0	0	
Act Effct Green (s)	10.2	47.9	47.9		36.5			22.2			22.2	
Actuated g/C Ratio	0.13	0.61	0.61		0.47			0.28			0.28	
v/c Ratio	0.47	0.59	0.05		0.83			0.76			0.42	
Control Delay	41.9	10.2	0.5		25.2			53.0			9.8	
Queue Delay	0.0	0.0	0.0		0.0			0.0			0.0	
Total Delay	41.9	10.2	0.5		25.2			53.0			9.8	
LOS	D	В	Α		С			D			Α	
Approach Delay		12.4			25.2			53.0			9.8	
Approach LOS		В			С			D			Α	
Intersection Summary												

Intersection Summary

Area Type: Other

Cycle Length: 99

Actuated Cycle Length: 78.3

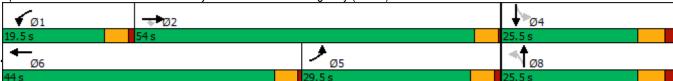
Natural Cycle: 65

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.83

Intersection Signal Delay: 20.3 Intersection LOS: C
Intersection Capacity Utilization 76.0% ICU Level of Service D

Analysis Period (min) 15



	•	-	\rightarrow	•	†	ţ
Lane Group	EBL	EBT	EBR	WBT	NBT	SBT
Lane Group Flow (vph)	96	1067	42	1226	180	217
v/c Ratio	0.47	0.59	0.05	0.83	0.76	0.42
Control Delay	41.9	10.2	0.5	25.2	53.0	9.8
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	41.9	10.2	0.5	25.2	53.0	9.8
Queue Length 50th (ft)	48	143	0	275	89	15
Queue Length 95th (ft)	95	191	4	#406	#220	76
Internal Link Dist (ft)		388		222	285	130
Turn Bay Length (ft)	115		100			
Base Capacity (vph)	526	2064	985	1663	237	520
Starvation Cap Reductn	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0
Reduced v/c Ratio	0.18	0.52	0.04	0.74	0.76	0.42
Intersection Summary						

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	^	7	*	↑ ↑			4			4	
Traffic Volume (vph)	88	982	39	0	1106	22	160	4	2	26	8	166
Future Volume (vph)	88	982	39	0	1106	22	160	4	2	26	8	166
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)	4.0	4.0	4.0		4.0			4.0			4.0	
Lane Util. Factor	1.00	0.95	1.00		0.95			1.00			1.00	
Frpb, ped/bikes	1.00	1.00	0.98		1.00			1.00			0.99	
Flpb, ped/bikes	1.00	1.00	1.00		1.00			1.00			1.00	
Frt	1.00	1.00	0.85		1.00			1.00			0.89	
Flt Protected	0.95	1.00	1.00		1.00			0.95			0.99	
Satd. Flow (prot)	1568	2942	1373		3158			1601			1455	
FIt Permitted	0.95	1.00	1.00		1.00			0.50			0.95	
Satd. Flow (perm)	1568	2942	1373		3158			838			1385	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	96	1067	42	0	1202	24	174	4	2	28	9	180
RTOR Reduction (vph)	0	0	16	0	1	0	0	1	0	0	130	0
Lane Group Flow (vph)	96	1067	26	0	1225	0	0	179	0	0	87	0
Confl. Peds. (#/hr)			1	1			2					2
Confl. Bikes (#/hr)						1						
Heavy Vehicles (%)	6%	13%	6%	2%	5%	2%	4%	2%	2%	24%	2%	2%
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases		_	2	•			8			4	•	
Actuated Green, G (s)	8.0	49.0	49.0		36.5			20.6			20.6	
Effective Green, g (s)	8.5	49.0	49.0		36.5			22.1			22.1	
Actuated g/C Ratio	0.11	0.62	0.62		0.46			0.28			0.28	
Clearance Time (s)	4.5	4.0	4.0		4.0			5.5			5.5	
Vehicle Extension (s)	2.3	5.8	5.8		5.8			2.5			2.5	
Lane Grp Cap (vph)	168	1822	850		1457			234			386	
v/s Ratio Prot	0.06	c0.36	000		c0.39			201			000	
v/s Ratio Perm	0.00	00.00	0.02		0 0.00			c0.21			0.06	
v/c Ratio	0.57	0.59	0.02		0.84			0.77			0.23	
Uniform Delay, d1	33.6	9.0	5.8		18.7			26.1			21.9	
Progression Factor	1.00	1.00	1.00		1.00			1.00			1.00	
Incremental Delay, d2	3.4	0.9	0.0		5.2			13.3			0.2	
Delay (s)	37.0	9.9	5.9		24.0			39.5			22.1	
Level of Service	57.0 D	3.5 A	A		Z-4.0			D			C	
Approach Delay (s)		11.9			24.0			39.5			22.1	
Approach LOS		В			C C			D			C	
Intersection Summary												
HCM 2000 Control Delay			19.7	H	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capacit	v ratio		0.81	,.								
Actuated Cycle Length (s)	•		79.1	Sı	um of lost	time (s)			12.0			
Intersection Capacity Utilization	on		76.0%		U Level c				D			
Analysis Period (min)			15			2.7.00						
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	ሻ	∱ ∱			4			4	
Traffic Volume (veh/h)	88	982	39	0	1106	22	160	4	2	26	8	166
Future Volume (veh/h)	88	982	39	0	1106	22	160	4	2	26	8	166
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		0.98	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1668	1573	1668	1723	1682	1682	1723	1723	1723	1723	1723	1723
Adj Flow Rate, veh/h	96	1067	9	0	1202	23	174	4	1	28	9	39
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	6	13	6	2	5	5	2	2	2	2	2	2
Cap, veh/h	135	2083	985	3	1792	34	351	6	1	146	64	143
Arrive On Green	0.08	0.70	0.70	0.00	0.56	0.56	0.15	0.17	0.15	0.15	0.17	0.15
Sat Flow, veh/h	1589	2988	1413	1641	3205	61	1399	32	8	411	371	824
Grp Volume(v), veh/h	96	1067	9	0	599	626	179	0	0	76	0	0
Grp Sat Flow(s), veh/h/ln	1589	1494	1413	1641	1598	1669	1440	0	0	1606	0	0
Q Serve(g_s), s	3.9	11.0	0.1	0.0	17.3	17.4	5.0	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(g_c), s	3.9	11.0	0.1	0.0	17.3	17.4	7.8	0.0	0.0	2.8	0.0	0.0
Prop In Lane	1.00	11.0	1.00	1.00	17.0	0.04	0.97	0.0	0.01	0.37	0.0	0.51
Lane Grp Cap(c), veh/h	135	2083	985	3	893	933	325	0	0.01	317	0	0.01
V/C Ratio(X)	0.71	0.51	0.01	0.00	0.67	0.67	0.55	0.00	0.00	0.24	0.00	0.00
Avail Cap(c_a), veh/h	617	2277	1077	388	974	1018	535	0.00	0.00	543	0.00	0.00
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	0.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	29.2	4.7	3.0	0.00	10.2	10.2	26.2	0.00	0.00	24.2	0.0	0.00
Incr Delay (d2), s/veh	4.2	0.6	0.0	0.0	3.1	3.0	1.1	0.0	0.0	0.3	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.6	2.6	0.0	0.0	5.9	6.2	2.8	0.0	0.0	1.1	0.0	0.0
Unsig. Movement Delay, s/veh		2.0	0.0	0.0	5.9	0.2	2.0	0.0	0.0	1.1	0.0	0.0
LnGrp Delay(d),s/veh	33.5	5.3	3.0	0.0	13.3	13.2	27.3	0.0	0.0	24.5	0.0	0.0
LnGrp LOS	33.5 C		3.0 A	0.0 A	13.3 B	13.2 B	21.3 C	0.0 A	0.0 A	24.5 C		
	U	A 4470	A	A		D	U		A	U	A 70	A
Approach Vol, veh/h		1172			1225			179			76	
Approach Delay, s/veh		7.6			13.2			27.3			24.5	
Approach LOS		Α			В			С			С	
Timer - Assigned Phs	1	2		4	5	6		8				
Phs Duration (G+Y+Rc), s	0.0	50.2		15.4	9.6	40.7		15.4				
Change Period (Y+Rc), s	4.5	* 4.5		5.5	4.5	4.0		5.5				
Max Green Setting (Gmax), s	15.0	* 50		20.0	25.0	40.0		20.0				
Max Q Clear Time (g_c+l1), s	0.0	13.0		4.8	5.9	19.4		9.8				
Green Ext Time (p_c), s	0.0	25.6		0.2	0.3	17.3		0.5				
Intersection Summary												
HCM 6th Ctrl Delay			12.0									
HCM 6th LOS			В									
Notos												

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ች	^	7	ሻ	ተ ኈ			4			4	
Traffic Volume (vph)	186	1292	158	6	1331	20	137	28	8	47	27	138
Future Volume (vph)	186	1292	158	6	1331	20	137	28	8	47	27	138
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Storage Length (ft)	115		100	105		0	0		0	0		0
Storage Lanes	1		1	1		0	0		0	0		0
Taper Length (ft)	100			100			100		-	100		
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	1.00	0.00	0.98	1.00	1.00	0.00		1.00			0.99	
Frt			0.850		0.998			0.993			0.912	
Flt Protected	0.950		0.000	0.950	0.000			0.962			0.989	
Satd. Flow (prot)	1630	3228	1458	1630	3161	0	0	1623	0	0	1526	0
Flt Permitted	0.950	OLLO	1 100	0.950	0101	•		0.473	•		0.910	J
Satd. Flow (perm)	1629	3228	1426	1629	3161	0	0	796	0	0	1404	0
Right Turn on Red	1020	OLLO	Yes	1020	0101	Yes		100	Yes		1101	Yes
Satd. Flow (RTOR)			95		2	100		2	100		75)	100
Link Speed (mph)		25	00		25			25			25	
Link Distance (ft)		468			302			365			210	
Travel Time (s)		12.8			8.2			10.0			5.7	
Confl. Peds. (#/hr)	2	12.0	1	1	0.2	2	5	10.0			0.1	5
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Heavy Vehicles (%)	2%	3%	2%	2%	5%	2%	2%	8%	2%	2%	2%	2%
Adj. Flow (vph)	198	1374	168	6	1416	21	146	30	9	50	29	147
Shared Lane Traffic (%)	130	1074	100		1410	21	170	30	<u> </u>	30	25	177
Lane Group Flow (vph)	198	1374	168	6	1437	0	0	185	0	0	226	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA
Median Width(ft)	L 11/1	12	13.14/3	LIVA	12	13 13/3	L 11/1	0	13.13/3	L 11/1	0	IX IVA
Link Offset(ft)		-12			0			0			4	
Crosswalk Width(ft)		72			42			32			30	
Two way Left Turn Lane		12			72			52			50	
Headway Factor	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
Number of Detectors	2	1.11	1.11	2	1.11	1.11	2	2	1.11	2	2	1.11
Detector Template	Left	Det25	Right	Left	Det25			Side St		Left		
Leading Detector (ft)	78	153	153	78	153		78	78		78	78	
Trailing Detector (ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Position(ft)	2	137	137	2	137		2	2		2	2	
Detector 1 Size(ft)	16	16	16	16	16		16	16		16	16	
	CI+Ex	Cl+Ex	Cl+Ex	Cl+Ex	Cl+Ex		Cl+Ex	Cl+Ex		Cl+Ex	CI+Ex	
Detector 1 Type Detector 1 Channel	UI+EX	CI+EX	CI+EX	CI+EX	CI+EX		CI+EX	CI+EX		CI+EX	CI+EX	
	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Extend (s)	0.0	0.0	0.0	0.0			0.0			0.0		
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	
Detector 2 Position(ft)	72			72			72	72		72	72	
Detector 2 Size(ft)	6 CL Ev			6 CL Ev			6 CL Ev	6 CL Ev		6 CL Ev	6 CL Ev	
Detector 2 Type	CI+Ex			CI+Ex			Cl+Ex	Cl+Ex		Cl+Ex	CI+Ex	
Detector 2 Channel	0.0			0.0			0.0	0.0		- 0 0	0.0	
Detector 2 Extend (s)	0.0		_	0.0			0.0	0.0		0.0	0.0	
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Detector Phase	5	2	2	1	6		8	8		4	4	
Switch Phase												
Minimum Initial (s)	4.0	10.0	10.0	4.0	10.0		6.0	6.0		6.0	6.0	
Minimum Split (s)	8.5	26.0	26.0	8.5	30.0		11.5	11.5		23.5	23.5	
Total Split (s)	20.0	70.0	70.0	15.0	65.0		25.0	25.0		25.0	25.0	
Total Split (%)	18.2%	63.6%	63.6%	13.6%	59.1%		22.7%	22.7%		22.7%	22.7%	
Maximum Green (s)	15.5	66.0	66.0	10.5	61.0		19.5	19.5		19.5	19.5	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5		4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	0.5	0.5	1.0	0.5		1.5	1.5		1.5	1.5	
Lost Time Adjust (s)	-0.5	0.0	0.0	-0.5	0.0			-1.5			-1.5	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lead/Lag	Lag	Lag	Lag	Lead	Lead							
Lead-Lag Optimize?												
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8		2.5	2.5		2.5	2.5	
Minimum Gap (s)	0.5	3.8	3.8	0.5	3.8		2.0	2.0		2.0	2.0	
Time Before Reduce (s)	8.0	10.0	10.0	8.0	10.0		5.0	5.0		5.0	5.0	
Time To Reduce (s)	3.0	10.0	10.0	3.0	10.0		5.0	5.0		5.0	5.0	
Recall Mode	None	C-Min	C-Min	None	C-Min		None	None		None	None	
Walk Time (s)		7.0	7.0		7.0					7.0	7.0	
Flash Dont Walk (s)		15.0	15.0		19.0					11.0	11.0	
Pedestrian Calls (#/hr)		0	0		0					0	0	
Act Effct Green (s)	15.9	75.7	75.7	5.8	58.0			24.1			24.1	
Actuated g/C Ratio	0.14	0.69	0.69	0.05	0.53			0.22			0.22	
v/c Ratio	0.84	0.62	0.17	0.07	0.86			1.05			0.62	
Control Delay	75.7	11.0	3.1	50.8	28.6			126.5			35.2	
Queue Delay	0.0	0.0	0.0	0.0	0.0			0.0			0.0	
Total Delay	75.7	11.0	3.1	50.8	28.6			126.5			35.2	
LOS	Е	В	Α	D	С			F			D	
Approach Delay		17.6			28.7			126.5			35.2	
Approach LOS		В			С			F			D	

Intersection Summary

Area Type: Other

Cycle Length: 110
Actuated Cycle Length: 110

Offset: 0 (0%), Referenced to phase 2:EBT and 6:WBT, Start of Green, Master Intersection

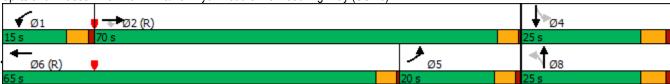
Natural Cycle: 90

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 1.05 Intersection Signal Delay: 28.8 Intersection Capacity Utilization 89.6%

Intersection LOS: C
ICU Level of Service E

Analysis Period (min) 15



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Lane Group	EBL	EBT	EBR	WBL	WBT	NBT	SBT
Lane Group Flow (vph)	198	1374	168	6	1437	185	226
v/c Ratio	0.84	0.62	0.17	0.07	0.86	1.05	0.62
Control Delay	75.7	11.0	3.1	50.8	28.6	126.5	35.2
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	75.7	11.0	3.1	50.8	28.6	126.5	35.2
Queue Length 50th (ft)	136	201	12	4	426	~159	100
Queue Length 95th (ft)	#263	369	44	18	518	#305	#189
Internal Link Dist (ft)		388			222	285	130
Turn Bay Length (ft)	115		100	105			
Base Capacity (vph)	244	2221	1011	163	1753	176	366
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.81	0.62	0.17	0.04	0.82	1.05	0.62

Intersection Summary

Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ		7	ሻ	∱ ∱			4			4	
Traffic Volume (vph)	186	1292	158	6	1331	20	137	28	8	47	27	138
Future Volume (vph)	186	1292	158	6	1331	20	137	28	8	47	27	138
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0			4.0			4.0	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95			1.00			1.00	
Frpb, ped/bikes	1.00	1.00	0.98	1.00	1.00			1.00			0.99	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00			1.00			1.00	
Frt	1.00	1.00	0.85	1.00	1.00			0.99			0.91	
Flt Protected	0.95	1.00	1.00	0.95	1.00			0.96			0.99	
Satd. Flow (prot)	1630	3228	1426	1630	3160			1619			1527	
FIt Permitted	0.95	1.00	1.00	0.95	1.00			0.47			0.91	
Satd. Flow (perm)	1630	3228	1426	1630	3160			796			1405	
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	198	1374	168	6	1416	21	146	30	9	50	29	147
RTOR Reduction (vph)	0	0	33	0	1	0	0	2	0	0	59	0
Lane Group Flow (vph)	198	1374	135	6	1436	0	0	183	0	0	167	0
Confl. Peds. (#/hr)	2		1	1		2	5					5
Heavy Vehicles (%)	2%	3%	2%	2%	5%	2%	2%	8%	2%	2%	2%	2%
Turn Type	Prot	NA	Perm	Prot	NA		Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2				8			4		
Actuated Green, G (s)	19.0	72.1	72.1	1.3	54.4			22.6			22.6	
Effective Green, g (s)	19.5	72.1	72.1	1.8	54.4			24.1			24.1	
Actuated g/C Ratio	0.18	0.66	0.66	0.02	0.49			0.22			0.22	
Clearance Time (s)	4.5	4.0	4.0	4.5	4.0			5.5			5.5	
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8			2.5			2.5	
Lane Grp Cap (vph)	288	2115	934	26	1562			174			307	
v/s Ratio Prot	0.12	c0.43		0.00	c0.45							
v/s Ratio Perm			0.09					c0.23			0.12	
v/c Ratio	0.69	0.65	0.14	0.23	0.92			1.05			0.55	
Uniform Delay, d1	42.4	11.4	7.2	53.4	25.8			42.9			38.1	
Progression Factor	1.00	1.00	1.00	1.00	1.00			1.00			1.00	
Incremental Delay, d2	5.8	1.6	0.3	2.6	10.2			83.3			1.6	
Delay (s)	48.2	12.9	7.5	56.1	36.0			126.3			39.7	
Level of Service	D	В	Α	Е	D			F			D	
Approach Delay (s)		16.4			36.1			126.3			39.7	
Approach LOS		В			D			F			D	
Intersection Summary												
HCM 2000 Control Delay					CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capacity ratio 0.91												
Actuated Cycle Length (s)			110.0		um of lost				12.0			
Intersection Capacity Utilizat	ion		89.6%	IC	CU Level o	of Service			Е			
Analysis Period (min)			15									

c Critical Lane Group

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	ň	∱ }			4			4	
Traffic Volume (veh/h)	186	1292	158	6	1331	20	137	28	8	47	27	138
Future Volume (veh/h)	186	1292	158	6	1331	20	137	28	8	47	27	138
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		0.99	1.00		0.99
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1723	1709	1723	1723	1682	1682	1641	1641	1641	1723	1723	1723
Adj Flow Rate, veh/h	198	1374	137	6	1416	20	146	30	7	50	29	84
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Percent Heavy Veh, %	2	3	2	2	5	5	8	8	8	2	2	2
Cap, veh/h	264	2224	998	17	1739	25	219	35	8	115	74	156
Arrive On Green	0.16	0.68	0.68	0.01	0.54	0.54	0.18	0.19	0.18	0.18	0.19	0.18
Sat Flow, veh/h	1641	3247	1458	1641	3226	46	839	185	41	379	390	818
Grp Volume(v), veh/h	198	1374	137	6	701	735	183	0	0	163	0	0
Grp Sat Flow(s),veh/h/ln	1641	1624	1458	1641	1598	1673	1064	0	0	1587	0	0
Q Serve(g_s), s	12.7	25.4	3.6	0.4	39.6	39.7	8.6	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(g_c), s	12.7	25.4	3.6	0.4	39.6	39.7	18.9	0.0	0.0	10.4	0.0	0.0
Prop In Lane	1.00		1.00	1.00		0.03	0.80		0.04	0.31		0.52
Lane Grp Cap(c), veh/h	264	2224	998	17	861	902	247	0	0	324	0	0
V/C Ratio(X)	0.75	0.62	0.14	0.34	0.81	0.81	0.74	0.00	0.00	0.50	0.00	0.00
Avail Cap(c_a), veh/h	264	2224	998	164	886	928	247	0	0	324	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	44.0	9.5	6.0	54.0	20.8	20.8	45.1	0.0	0.0	40.8	0.0	0.0
Incr Delay (d2), s/veh	10.6	1.3	0.3	7.0	8.3	8.0	10.6	0.0	0.0	0.9	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	5.9	8.7	1.1	0.2	16.3	17.0	5.8	0.0	0.0	4.2	0.0	0.0
Unsig. Movement Delay, s/veh												
LnGrp Delay(d),s/veh	54.6	10.8	6.3	61.0	29.1	28.9	55.8	0.0	0.0	41.7	0.0	0.0
LnGrp LOS	D	В	Α	Е	С	С	Е	Α	Α	D	Α	Α
Approach Vol, veh/h		1709			1442			183			163	
Approach Delay, s/veh		15.5			29.1			55.8			41.7	
Approach LOS		В			С			Е			D	
Timer - Assigned Phs	1	2		4	5	6		8				
Phs Duration (G+Y+Rc), s	5.2	79.8		25.0	21.7	63.3		25.0				
Change Period (Y+Rc), s	4.5	* 4.5		5.5	4.5	4.0		5.5				
Max Green Setting (Gmax), s	10.5	* 66		19.5	15.5	61.0		19.5				
Max Q Clear Time (g_c+l1), s	2.4	27.4		12.4	14.7	41.7		20.9				
Green Ext Time (p_c), s	0.0	33.5		0.3	0.1	17.6		0.0				
. ,	0.0	55.5		0.5	0.1	17.0		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			24.4									
HCM 6th LOS			C									
Notes												

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	^	7	ሻ	^	7		4			4	
Traffic Volume (vph)	88	982	39	0	1106	22	160	4	2	26	8	166
Future Volume (vph)	88	982	39	0	1106	22	160	4	2	26	8	166
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Storage Length (ft)	115		100	105		0	0		0	0		0
Storage Lanes	1		1	1		1	0		0	0		0
Taper Length (ft)	100			100			100			100		
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor			0.98			0.98		1.00			0.99	
Frt			0.850			0.850		0.998			0.888	
Flt Protected	0.950							0.954			0.994	
Satd. Flow (prot)	1568	2942	1403	1716	3167	1458	0	1603	0	0	1455	0
Flt Permitted	0.950							0.504			0.946	
Satd. Flow (perm)	1568	2942	1372	1716	3167	1428	0	846	0	0	1385	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)			77			77		1			180	
Link Speed (mph)		25			25			25			25	
Link Distance (ft)		468			302			365			210	
Travel Time (s)		12.8			8.2			10.0			5.7	
Confl. Peds. (#/hr)			1	1			2					2
Confl. Bikes (#/hr)						1						
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	13%	6%	2%	5%	2%	4%	2%	2%	24%	2%	2%
Adj. Flow (vph)	96	1067	42	0	1202	24	174	4	2	28	9	180
Shared Lane Traffic (%)												
Lane Group Flow (vph)	96	1067	42	0	1202	24	0	180	0	0	217	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA
Median Width(ft)		12			12			0			0	
Link Offset(ft)		-12			0			0			4	
Crosswalk Width(ft)		72			42			32			30	
Two way Left Turn Lane												
Headway Factor	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
Number of Detectors	2	1	1	2	1	1	2	2		2	2	
Detector Template	Left	Det25	Right	Left	Det25	Right	Left	Side St		Left	Side St	
Leading Detector (ft)	78	153	153	78	153	153	78	78		78	78	
Trailing Detector (ft)	2	137	137	2	137	137	2	2		2	2	
Detector 1 Position(ft)	2	137	137	2	137	137	2	2		2	2	
Detector 1 Size(ft)	16	16	16	16	16	16	16	16		16	16	
Detector 1 Type	CI+Ex	CI+Ex	Cl+Ex	CI+Ex	CI+Ex	CI+Ex	CI+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 1 Channel												
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	
Detector 2 Position(ft)	72			72			72	72		72	72	
Detector 2 Size(ft)	6			6			6	6		6	6	
Detector 2 Type	CI+Ex			CI+Ex			CI+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 2 Channel												
Detector 2 Extend (s)	0.0			0.0			0.0	0.0		0.0	0.0	
	3.0						3.0			3.0		

Sandy Health Clinic - PBS Project 71524.000

Synchro 10 Report - by PBS Engineering and Environmental

2029 With Project Conditions - Weekday AM Peak Hour + With WB Right-Turn Lane

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Turn Type	Prot	NA	Perm	Prot	NA	Perm	Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2			6	8			4		
Detector Phase	5	2	2	1	6	6	8	8		4	4	
Switch Phase												
Minimum Initial (s)	4.0	10.0	10.0	4.0	10.0	10.0	6.0	6.0		6.0	6.0	
Minimum Split (s)	8.5	26.0	26.0	8.5	30.0	30.0	11.5	11.5		23.5	23.5	
Total Split (s)	29.5	54.0	54.0	19.5	44.0	44.0	25.5	25.5		25.5	25.5	
Total Split (%)	29.8%	54.5%	54.5%	19.7%	44.4%	44.4%	25.8%	25.8%		25.8%	25.8%	
Maximum Green (s)	25.0	50.0	50.0	15.0	40.0	40.0	20.0	20.0		20.0	20.0	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5	3.5	4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	0.5	0.5	1.0	0.5	0.5	1.5	1.5		1.5	1.5	
Lost Time Adjust (s)	-0.5	0.0	0.0	-0.5	0.0	0.0		-1.5			-1.5	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0	4.0		4.0			4.0	
Lead/Lag	Lag	Lag	Lag	Lead	Lead	Lead						
Lead-Lag Optimize?												
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8	5.8	2.5	2.5		2.5	2.5	
Minimum Gap (s)	0.5	3.8	3.8	0.5	3.8	3.8	2.0	2.0		2.0	2.0	
Time Before Reduce (s)	8.0	10.0	10.0	8.0	10.0	10.0	5.0	5.0		5.0	5.0	
Time To Reduce (s)	3.0	10.0	10.0	3.0	10.0	10.0	5.0	5.0		5.0	5.0	
Recall Mode	None	Min	Min	None	Min	Min	None	None		None	None	
Walk Time (s)		7.0	7.0		7.0	7.0				7.0	7.0	
Flash Dont Walk (s)		15.0	15.0		19.0	19.0				11.0	11.0	
Pedestrian Calls (#/hr)		0	0		0	0				0	0	
Act Effct Green (s)	10.1	46.7	46.7		35.4	35.4		22.3			22.3	
Actuated g/C Ratio	0.13	0.60	0.60		0.46	0.46		0.29			0.29	
v/c Ratio	0.47	0.60	0.05		0.83	0.03		0.74			0.41	
Control Delay	41.5	10.4	0.5		25.1	0.1		50.4			9.7	
Queue Delay	0.0	0.0	0.0		0.0	0.0		0.0			0.0	
Total Delay	41.5	10.4	0.5		25.1	0.1		50.4			9.7	
LOS	D	В	Α		С	Α		D			Α	
Approach Delay		12.5			24.6			50.4			9.7	
Approach LOS		В			С			D			Α	
Intersection Summary												

Intersection Summary

Area Type: Other

Cycle Length: 99

Actuated Cycle Length: 77.3

Natural Cycle: 65

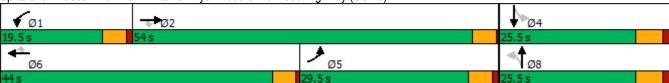
Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.83

Intersection Signal Delay: 20.0 Intersection LOS: B
Intersection Capacity Utilization 75.2% ICU Level of Service D

Analysis Period (min) 15

Splits and Phases: 3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)



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Lane Group	EBL	EBT	EBR	WBT	WBR	NBT	SBT
Lane Group Flow (vph)	96	1067	42	1202	24	180	217
v/c Ratio	0.47	0.60	0.05	0.83	0.03	0.74	0.41
Control Delay	41.5	10.4	0.5	25.1	0.1	50.4	9.7
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	41.5	10.4	0.5	25.1	0.1	50.4	9.7
Queue Length 50th (ft)	48	143	0	267	0	89	15
Queue Length 95th (ft)	95	191	4	391	0	#219	76
Internal Link Dist (ft)		388		222		285	130
Turn Bay Length (ft)	115		100				
Base Capacity (vph)	536	2101	1001	1698	801	244	527
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.18	0.51	0.04	0.71	0.03	0.74	0.41
Intersection Summary							

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	^	7	ሻ	^	7		4			4	
Traffic Volume (vph)	88	982	39	0	1106	22	160	4	2	26	8	166
Future Volume (vph)	88	982	39	0	1106	22	160	4	2	26	8	166
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)	4.0	4.0	4.0		4.0	4.0		4.0			4.0	
Lane Util. Factor	1.00	0.95	1.00		0.95	1.00		1.00			1.00	
Frpb, ped/bikes	1.00	1.00	0.98		1.00	0.98		1.00			0.99	
Flpb, ped/bikes	1.00	1.00	1.00		1.00	1.00		1.00			1.00	
Frt	1.00	1.00	0.85		1.00	0.85		1.00			0.89	
Flt Protected	0.95	1.00	1.00		1.00	1.00		0.95			0.99	
Satd. Flow (prot)	1568	2942	1373		3167	1428		1601			1455	
FIt Permitted	0.95	1.00	1.00		1.00	1.00		0.50			0.95	
Satd. Flow (perm)	1568	2942	1373		3167	1428		846			1386	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	96	1067	42	0	1202	24	174	4	2	28	9	180
RTOR Reduction (vph)	0	0	16	0	0	13	0	1	0	0	129	0
Lane Group Flow (vph)	96	1067	26	0	1202	11	0	179	0	0	88	0
Confl. Peds. (#/hr)			1	1			2					2
Confl. Bikes (#/hr)						1						
Heavy Vehicles (%)	6%	13%	6%	2%	5%	2%	4%	2%	2%	24%	2%	2%
Turn Type	Prot	NA	Perm	Prot	NA	Perm	Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2			6	8			4		
Actuated Green, G (s)	8.0	47.9	47.9		35.4	35.4		20.7			20.7	
Effective Green, g (s)	8.5	47.9	47.9		35.4	35.4		22.2			22.2	
Actuated g/C Ratio	0.11	0.61	0.61		0.45	0.45		0.28			0.28	
Clearance Time (s)	4.5	4.0	4.0		4.0	4.0		5.5			5.5	
Vehicle Extension (s)	2.3	5.8	5.8		5.8	5.8		2.5			2.5	
Lane Grp Cap (vph)	170	1804	842		1435	647		240			393	
v/s Ratio Prot	0.06	c0.36			c0.38							
v/s Ratio Perm			0.02			0.01		c0.21			0.06	
v/c Ratio	0.56	0.59	0.03		0.84	0.02		0.75			0.22	
Uniform Delay, d1	33.0	9.2	6.0		18.8	11.8		25.4			21.4	
Progression Factor	1.00	1.00	1.00		1.00	1.00		1.00			1.00	
Incremental Delay, d2	3.1	0.9	0.0		5.1	0.0		11.4			0.2	
Delay (s)	36.1	10.1	6.0		23.9	11.8		36.8			21.6	
Level of Service	D	В	Α		С	В		D			С	
Approach Delay (s)		12.0			23.7			36.8			21.6	
Approach LOS		В			С			D			С	
Intersection Summary												
HCM 2000 Control Delay			19.4	H	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capac	city ratio		0.80									
Actuated Cycle Length (s)		78.1			um of lost	time (s)			12.0			
Intersection Capacity Utilizat	tion		75.2%	IC	U Level o	of Service	1		D			
Analysis Period (min)			15									
c Critical Lane Group												

	•	→	•	•	←	•	4	†	~	>	ļ	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	ሻ	^	7		4			4	
Traffic Volume (veh/h)	88	982	39	0	1106	22	160	4	2	26	8	166
Future Volume (veh/h)	88	982	39	0	1106	22	160	4	2	26	8	166
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1668	1573	1668	1723	1682	1723	1723	1723	1723	1723	1723	1723
Adj Flow Rate, veh/h	96	1067	8	0	1202	0	174	4	1	28	9	41
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	6	13	6	2	5	2	2	2	2	2	2	2
Cap, veh/h	135	2083	985	3	1786	816	351	6	1	143	63	146
Arrive On Green	0.08	0.70	0.70	0.00	0.56	0.00	0.15	0.17	0.15	0.15	0.17	0.15
Sat Flow, veh/h	1589	2988	1413	1641	3195	1460	1400	32	8	394	367	843
Grp Volume(v), veh/h	96	1067	8	0	1202	0	179	0	0	78	0	0
Grp Sat Flow(s), veh/h/ln	1589	1494	1413	1641	1598	1460	1440	0	0	1604	0	0
Q Serve(g_s), s	3.9	11.0	0.1	0.0	17.4	0.0	4.9	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(g_c), s	3.9	11.0	0.1	0.0	17.4	0.0	7.8	0.0	0.0	2.9	0.0	0.0
Prop In Lane	1.00	11.0	1.00	1.00		1.00	0.97	0.0	0.01	0.36	0.0	0.53
Lane Grp Cap(c), veh/h	135	2083	985	3	1786	816	325	0	0.01	316	0	0.00
V/C Ratio(X)	0.71	0.51	0.01	0.00	0.67	0.00	0.55	0.00	0.00	0.25	0.00	0.00
Avail Cap(c_a), veh/h	618	2280	1078	388	1951	891	535	0.00	0.00	542	0.00	0.00
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	0.00	1.00	0.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	29.2	4.7	3.0	0.0	10.2	0.0	26.1	0.0	0.0	24.2	0.0	0.0
Incr Delay (d2), s/veh	4.2	0.6	0.0	0.0	1.6	0.0	1.1	0.0	0.0	0.3	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.6	2.6	0.0	0.0	5.6	0.0	2.8	0.0	0.0	1.1	0.0	0.0
Unsig. Movement Delay, s/veh		2.0	0.0	0.0	5.0	0.0	2.0	0.0	0.0	1.1	0.0	0.0
LnGrp Delay(d),s/veh	33.4	5.3	3.0	0.0	11.8	0.0	27.2	0.0	0.0	24.5	0.0	0.0
LnGrp LOS	33.4 C	J.5	3.0 A	Α	В	Α	C C	Α	Α	24.3 C	Α	Α
Approach Vol, veh/h		1171			1202			179			78	
Approach Delay, s/veh		7.6			11.8			27.2			24.5	
Approach LOS		Α			В			С			С	
Timer - Assigned Phs	1	2		4	5	6		8				
Phs Duration (G+Y+Rc), s	0.0	50.2		15.3	9.6	40.6		15.3				
Change Period (Y+Rc), s	4.5	* 4.5		5.5	4.5	4.0		5.5				
Max Green Setting (Gmax), s	15.0	* 50		20.0	25.0	40.0		20.0				
Max Q Clear Time (g_c+l1), s	0.0	13.0		4.9	5.9	19.4		9.8				
Green Ext Time (p_c), s	0.0	25.6		0.2	0.3	17.2		0.5				
Intersection Summary												
HCM 6th Ctrl Delay			11.4									
HCM 6th LOS			В									
Notes												

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	^	7	ሻ	^	7		4			4	
Traffic Volume (vph)	186	1292	158	6	1331	20	137	28	8	47	27	138
Future Volume (vph)	186	1292	158	6	1331	20	137	28	8	47	27	138
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Storage Length (ft)	115		100	105		100	0		0	0		0
Storage Lanes	1		1	1		0	0		0	0		0
Taper Length (ft)	100			100			100			100		
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	1.00		0.98	1.00		0.98		1.00			0.99	
Frt			0.850			0.850		0.993			0.912	
Flt Protected	0.950			0.950				0.962			0.989	
Satd. Flow (prot)	1630	3228	1458	1630	3167	1458	0	1623	0	0	1526	0
FIt Permitted	0.950			0.950				0.477			0.909	
Satd. Flow (perm)	1629	3228	1426	1629	3167	1423	0	802	0	0	1403	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)			95			69		2			75)	
Link Speed (mph)		25			25			25			25	
Link Distance (ft)		468			302			365			210	
Travel Time (s)		12.8			8.2			10.0			5.7	
Confl. Peds. (#/hr)	2		1	1		2	5					5
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Heavy Vehicles (%)	2%	3%	2%	2%	5%	2%	2%	8%	2%	2%	2%	2%
Adj. Flow (vph)	198	1374	168	6	1416	21	146	30	9	50	29	147
Shared Lane Traffic (%)												
Lane Group Flow (vph)	198	1374	168	6	1416	21	0	185	0	0	226	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA	L NA	R NA	R NA
Median Width(ft)		12			12			0			0	
Link Offset(ft)		-12			0			0			4	
Crosswalk Width(ft)		72			42			32			30	
Two way Left Turn Lane												
Headway Factor	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
Number of Detectors	2	1	1	2	1	1	2	2		2	2	
Detector Template	Left	Det25	Right	Left	Det25	Right	Left	Side St		Left	Side St	
Leading Detector (ft)	78	153	153	78	153	153	78	78		78	78	
Trailing Detector (ft)	2	137	137	2	137	137	2	2		2	2	
Detector 1 Position(ft)	2	137	137	2	137	137	2	2		2	2	
Detector 1 Size(ft)	16	16	16	16	16	16	16	16		16	16	
Detector 1 Type	CI+Ex	CI+Ex	CI+Ex	CI+Ex	CI+Ex	CI+Ex	CI+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 1 Channel												
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	
Detector 2 Position(ft)	72			72			72	72		72	72	
Detector 2 Size(ft)	6			6			6	6		6	6	
Detector 2 Type	CI+Ex			CI+Ex			CI+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 2 Channel												
Detector 2 Extend (s)	0.0			0.0			0.0	0.0		0.0	0.0	
Turn Type	Prot	NA	Perm	Prot	NA	Perm	Perm	NA		Perm	NA	

Sandy Health Clinic - PBS Project 71524.000

Synchro 10 Report - by PBS Engineering and Environmental

2029 With Project Trips Conditions - Weekday PM Peak Hour + With Right-Turn Lane

Page 1

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2			6	8			4		
Detector Phase	5	2	2	1	6	6	8	8		4	4	
Switch Phase												
Minimum Initial (s)	4.0	10.0	10.0	4.0	10.0	10.0	6.0	6.0		6.0	6.0	
Minimum Split (s)	8.5	26.0	26.0	8.5	30.0	30.0	11.5	11.5		23.5	23.5	
Total Split (s)	20.0	70.0	70.0	15.0	65.0	65.0	25.0	25.0		25.0	25.0	
Total Split (%)	18.2%	63.6%	63.6%	13.6%	59.1%	59.1%	22.7%	22.7%		22.7%	22.7%	
Maximum Green (s)	15.5	66.0	66.0	10.5	61.0	61.0	19.5	19.5		19.5	19.5	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5	3.5	4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	0.5	0.5	1.0	0.5	0.5	1.5	1.5		1.5	1.5	
Lost Time Adjust (s)	-0.5	0.0	0.0	-0.5	0.0	0.0		-1.5			-1.5	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0	4.0		4.0			4.0	
Lead/Lag	Lag	Lag	Lag	Lead	Lead	Lead						
Lead-Lag Optimize?												
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8	5.8	2.5	2.5		2.5	2.5	
Minimum Gap (s)	0.5	3.8	3.8	0.5	3.8	3.8	2.0	2.0		2.0	2.0	
Time Before Reduce (s)	8.0	10.0	10.0	8.0	10.0	10.0	5.0	5.0		5.0	5.0	
Time To Reduce (s)	3.0	10.0	10.0	3.0	10.0	10.0	5.0	5.0		5.0	5.0	
Recall Mode	None	C-Min	C-Min	None	C-Min	C-Min	None	None		None	None	
Walk Time (s)		7.0	7.0		7.0	7.0				7.0	7.0	
Flash Dont Walk (s)		15.0	15.0		19.0	19.0				11.0	11.0	
Pedestrian Calls (#/hr)		0	0		0	0				0	0	
Act Effct Green (s)	16.0	75.4	75.4	5.8	57.5	57.5		24.5			24.5	
Actuated g/C Ratio	0.15	0.69	0.69	0.05	0.52	0.52		0.22			0.22	
v/c Ratio	0.84	0.62	0.17	0.07	0.86	0.03		1.03			0.61	
Control Delay	74.8	11.2	3.1	50.8	28.5	0.1		120.1			34.8	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0		0.0			0.0	
Total Delay	74.8	11.2	3.1	50.8	28.5	0.1		120.1			34.8	
LOS	Е	В	Α	D	С	Α		F			С	
Approach Delay		17.6			28.1			120.1			34.8	
Approach LOS		В			С			F			С	

Intersection Summary

Area Type: Other

Cycle Length: 110

Actuated Cycle Length: 110

Offset: 0 (0%), Referenced to phase 2:EBT and 6:WBT, Start of Green, Master Intersection

Natural Cycle: 90

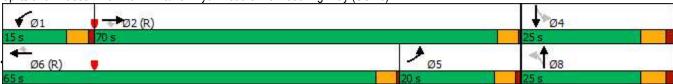
Control Type: Actuated-Coordinated

Maximum v/c Ratio: 1.03

Intersection Signal Delay: 28.2 Intersection LOS: C
Intersection Capacity Utilization 88.9% ICU Level of Service E

Analysis Period (min) 15

Splits and Phases: 3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)



Lane Group EBL EBT EBR WBL WBT WBR NBT SBT Lane Group Flow (vph) 198 1374 168 6 1416 21 185 226 v/c Ratio 0.84 0.62 0.17 0.07 0.86 0.03 1.03 0.61 Control Delay 74.8 11.2 3.1 50.8 28.5 0.1 120.1 34.8 Queue Delay 0.0		•	→	•	•	←	•	†	↓
v/c Ratio 0.84 0.62 0.17 0.07 0.86 0.03 1.03 0.61 Control Delay 74.8 11.2 3.1 50.8 28.5 0.1 120.1 34.8 Queue Delay 0.0	Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBT	SBT
Control Delay 74.8 11.2 3.1 50.8 28.5 0.1 120.1 34.8 Queue Delay 0.0 </td <td>Lane Group Flow (vph)</td> <td>198</td> <td>1374</td> <td>168</td> <td>6</td> <td>1416</td> <td>21</td> <td>185</td> <td>226</td>	Lane Group Flow (vph)	198	1374	168	6	1416	21	185	226
Queue Delay 0.0 <th< td=""><td>v/c Ratio</td><td>0.84</td><td>0.62</td><td>0.17</td><td>0.07</td><td>0.86</td><td>0.03</td><td>1.03</td><td>0.61</td></th<>	v/c Ratio	0.84	0.62	0.17	0.07	0.86	0.03	1.03	0.61
Total Delay 74.8 11.2 3.1 50.8 28.5 0.1 120.1 34.8 Queue Length 50th (ft) 135 201 12 4 418 0 ~158 100 Queue Length 95th (ft) #263 369 44 18 504 0 #304 #190 Internal Link Dist (ft) 388 222 285 130 Turn Bay Length (ft) 115 100 105 100 Base Capacity (vph) 245 2211 1007 163 1756 819 179 370 Starvation Cap Reductn 0 0 0 0 0 0 0 0 Spillback Cap Reductn 0 0 0 0 0 0 0 0 0 Storage Cap Reductn 0 0 0 0 0 0 0 0 0	Control Delay	74.8	11.2	3.1	50.8	28.5	0.1	120.1	34.8
Queue Length 50th (ft) 135 201 12 4 418 0 ~158 100 Queue Length 95th (ft) #263 369 44 18 504 0 #304 #190 Internal Link Dist (ft) 388 222 285 130 Turn Bay Length (ft) 115 100 105 100 Base Capacity (vph) 245 2211 1007 163 1756 819 179 370 Starvation Cap Reductn 0 0 0 0 0 0 0 0 Spillback Cap Reductn 0 0 0 0 0 0 0 0 Storage Cap Reductn 0 0 0 0 0 0 0 0 0	Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Queue Length 95th (ft) #263 369 44 18 504 0 #304 #190 Internal Link Dist (ft) 388 222 285 130 Turn Bay Length (ft) 115 100 105 100 Base Capacity (vph) 245 2211 1007 163 1756 819 179 370 Starvation Cap Reductn 0 0 0 0 0 0 0 Spillback Cap Reductn 0 0 0 0 0 0 0 Storage Cap Reductn 0 0 0 0 0 0 0	Total Delay	74.8	11.2	3.1	50.8	28.5	0.1	120.1	34.8
Internal Link Dist (ft) 388 222 285 130 Turn Bay Length (ft) 115 100 105 100 Base Capacity (vph) 245 2211 1007 163 1756 819 179 370 Starvation Cap Reductn 0 0 0 0 0 0 0 0 Spillback Cap Reductn 0 0 0 0 0 0 0 0 Storage Cap Reductn 0 0 0 0 0 0 0 0	Queue Length 50th (ft)	135	201	12	4	418	0	~158	100
Turn Bay Length (ft) 115 100 105 100 Base Capacity (vph) 245 2211 1007 163 1756 819 179 370 Starvation Cap Reductn 0 0 0 0 0 0 0 0 0 Spillback Cap Reductn 0 0 0 0 0 0 0 0 0 Storage Cap Reductn 0 0 0 0 0 0 0 0 0	Queue Length 95th (ft)	#263	369	44	18	504	0	#304	#190
Base Capacity (vph) 245 2211 1007 163 1756 819 179 370 Starvation Cap Reductn 0 0 0 0 0 0 0 0 Spillback Cap Reductn 0 0 0 0 0 0 0 0 Storage Cap Reductn 0 0 0 0 0 0 0 0	Internal Link Dist (ft)		388			222		285	130
Starvation Cap Reductn 0 0 0 0 0 0 0 Spillback Cap Reductn 0 0 0 0 0 0 0 0 Storage Cap Reductn 0 0 0 0 0 0 0 0	Turn Bay Length (ft)	115		100	105		100		
Spillback Cap Reductn 0 0 0 0 0 0 0 Storage Cap Reductn 0 0 0 0 0 0 0 0	Base Capacity (vph)	245	2211	1007	163	1756	819	179	370
Storage Cap Reductn 0 0 0 0 0 0 0	Starvation Cap Reductn	0	0	0	0	0	0	0	0
U	Spillback Cap Reductn	0	0	0	0	0	0	0	0
Reduced v/c Ratio 0.81 0.62 0.17 0.04 0.81 0.03 1.03 0.61	Storage Cap Reductn	0	0	0	0	0	0	0	0
	Reduced v/c Ratio	0.81	0.62	0.17	0.04	0.81	0.03	1.03	0.61

Intersection Summary

Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

	۶	→	•	•	+	•	1	†	~	/	↓	✓
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	¥	^	7		4			4	
Traffic Volume (vph)	186	1292	158	6	1331	20	137	28	8	47	27	138
Future Volume (vph)	186	1292	158	6	1331	20	137	28	8	47	27	138
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0		4.0			4.0	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00		1.00			1.00	
Frpb, ped/bikes	1.00	1.00	0.98	1.00	1.00	0.98		1.00			0.99	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00	1.00		1.00			1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85		0.99			0.91	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00		0.96			0.99	
Satd. Flow (prot)	1630	3228	1426	1630	3167	1423		1619			1527	
Flt Permitted	0.95	1.00	1.00	0.95	1.00	1.00		0.48			0.91	
Satd. Flow (perm)	1630	3228	1426	1630	3167	1423		803			1404	
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	198	1374	168	6	1416	21	146	30	9	50	29	147
RTOR Reduction (vph)	0	0	33	0	0	11	0	2	0	0	58	0
Lane Group Flow (vph)	198	1374	135	6	1416	10	0	183	0	0	168	0
Confl. Peds. (#/hr)	2		1	1		2	5					5
Heavy Vehicles (%)	2%	3%	2%	2%	5%	2%	2%	8%	2%	2%	2%	2%
Turn Type	Prot	NA	Perm	Prot	NA	Perm	Perm	NA		Perm	NA	
Protected Phases	5	2		1	6			8			4	
Permitted Phases			2			6	8			4		
Actuated Green, G (s)	19.2	71.7	71.7	1.3	53.8	53.8		23.0			23.0	
Effective Green, g (s)	19.7	71.7	71.7	1.8	53.8	53.8		24.5			24.5	
Actuated g/C Ratio	0.18	0.65	0.65	0.02	0.49	0.49		0.22			0.22	
Clearance Time (s)	4.5	4.0	4.0	4.5	4.0	4.0		5.5			5.5	
Vehicle Extension (s)	2.3	5.8	5.8	2.3	5.8	5.8		2.5			2.5	
Lane Grp Cap (vph)	291	2104	929	26	1548	695		178			312	
v/s Ratio Prot	0.12	c0.43		0.00	c0.45							
v/s Ratio Perm			0.09			0.01		c0.23			0.12	
v/c Ratio	0.68	0.65	0.15	0.23	0.91	0.01		1.03			0.54	
Uniform Delay, d1	42.2	11.6	7.4	53.4	26.0	14.5		42.8			37.7	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00		1.00			1.00	
Incremental Delay, d2	5.6	1.6	0.3	2.6	9.9	0.0		75.7			1.4	
Delay (s)	47.8	13.2	7.7	56.1	35.9	14.5		118.5			39.1	
Level of Service	D	В	Α	Е	D	В		F			D	
Approach Delay (s)		16.6			35.7			118.5			39.1	
Approach LOS		В			D			F			D	
Intersection Summary												
HCM 2000 Control Delay 30.9				H	CM 2000	Level of S	Service		С			
	HCM 2000 Volume to Capacity ratio 0.91			_					40.0			
Actuated Cycle Length (s)					um of lost				12.0			
Intersection Capacity Utilization	on		88.9%	IC	U Level	of Service			Е			
Analysis Period (min)			15									

	•	→	•	•	←	•	•	†	~	>	ļ	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	^	7	ň	^	7		4			4	
Traffic Volume (veh/h)	186	1292	158	6	1331	20	137	28	8	47	27	138
Future Volume (veh/h)	186	1292	158	6	1331	20	137	28	8	47	27	138
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		0.99	1.00		0.99
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1723	1709	1723	1723	1682	1723	1641	1641	1641	1723	1723	1723
Adj Flow Rate, veh/h	198	1374	137	6	1416	0	146	30	7	50	29	84
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Percent Heavy Veh, %	2	3	2	2	5	2	8	8	8	2	2	2
Cap, veh/h	264	2224	998	17	1722	787	219	35	8	115	74	156
Arrive On Green	0.16	0.68	0.68	0.01	0.54	0.00	0.18	0.19	0.18	0.18	0.19	0.18
Sat Flow, veh/h	1641	3247	1458	1641	3195	1460	839	185	41	379	390	818
Grp Volume(v), veh/h	198	1374	137	6	1416	0	183	0	0	163	0	0
Grp Sat Flow(s),veh/h/ln	1641	1624	1458	1641	1598	1460	1064	0	0	1587	0	0
Q Serve(g_s), s	12.7	25.4	3.6	0.4	40.4	0.0	8.6	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(g_c), s	12.7	25.4	3.6	0.4	40.4	0.0	18.9	0.0	0.0	10.4	0.0	0.0
Prop In Lane	1.00		1.00	1.00		1.00	0.80		0.04	0.31		0.52
Lane Grp Cap(c), veh/h	264	2224	998	17	1722	787	247	0	0	324	0	0
V/C Ratio(X)	0.75	0.62	0.14	0.34	0.82	0.00	0.74	0.00	0.00	0.50	0.00	0.00
Avail Cap(c_a), veh/h	264	2224	998	164	1772	810	247	0	0	324	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	0.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	44.0	9.5	6.0	54.0	21.0	0.0	45.1	0.0	0.0	40.8	0.0	0.0
Incr Delay (d2), s/veh	10.6	1.3	0.3	7.0	4.6	0.0	10.6	0.0	0.0	0.9	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	5.9	8.7	1.1	0.2	15.6	0.0	5.8	0.0	0.0	4.2	0.0	0.0
Unsig. Movement Delay, s/veh												
LnGrp Delay(d),s/veh	54.6	10.8	6.3	61.0	25.6	0.0	55.8	0.0	0.0	41.7	0.0	0.0
LnGrp LOS	D	В	Α	Е	С	Α	Е	Α	Α	D	Α	Α
Approach Vol, veh/h		1709			1422			183			163	
Approach Delay, s/veh		15.5			25.7			55.8			41.7	
Approach LOS		В			С			Е			D	
Timer - Assigned Phs	1	2		4	5	6		8				
Phs Duration (G+Y+Rc), s	5.2	79.8		25.0	21.7	63.3		25.0				
Change Period (Y+Rc), s	4.5	* 4.5		5.5	4.5	4.0		5.5				
Max Green Setting (Gmax), s	10.5	* 66		19.5	15.5	61.0		19.5				
Max Q Clear Time (g_c+l1), s	2.4	27.4		12.4	14.7	42.4		20.9				
Green Ext Time (p_c), s	0.0	33.5		0.3	0.1	16.9		0.0				
. ,	0.0	55.5		0.5	0.1	10.9		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			23.0									
HCM 6th LOS			C									
Notes												

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

Movement	EBL	EBR	NBL	NBT	SBT	SBR	All
Vehicles Entered	17	25	18	56	163	24	303
Vehicles Exited	17	25	18	56	163	24	303
Hourly Exit Rate	17	25	18	56	163	24	303
Input Volume	18	24	19	54	169	21	306
% of Volume	94	105	94	103	97	113	99

2: Ten Eyck Road & Pleasant Street (E) Performance by movement

Movement	NBT	NBR	SBT	All
Vehicles Entered	78	10	192	280
Vehicles Exited	78	10	192	280
Hourly Exit Rate	78	10	192	280
Input Volume	78	11	196	284
% of Volume	101	93	98	99

3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26) Performance by movement

Movement	EBL	EBT	EBR	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	All
Vehicles Entered	63	958	46	1086	20	162	4	2	23	12	157	2533
Vehicles Exited	63	959	46	1087	20	162	4	2	23	12	157	2535
Hourly Exit Rate	63	959	46	1087	20	162	4	2	23	12	157	2535
Input Volume	64	982	39	1106	19	160	4	2	25	13	159	2572
% of Volume	98	98	118	98	107	101	100	100	93	91	99	99

Vehicles Entered	2579
Vehicles Exited	2582
Hourly Exit Rate	2582
Input Volume	7900
% of Volume	33

Movement	EB	NB	SB
Directions Served	LR	LT	TR
Maximum Queue (ft)	70	63	40
Average Queue (ft)	25	7	1
95th Queue (ft)	52	35	19
Link Distance (ft)	624	59	201
Upstream Blk Time (%)		0	
Queuing Penalty (veh)		0	
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 2: Ten Eyck Road & Pleasant Street (E)

Movement	NB	SB
Directions Served	TR	LT
Maximum Queue (ft)	3	71
Average Queue (ft)	0	8
95th Queue (ft)	3	41
Link Distance (ft)	105	59
Upstream Blk Time (%)		1
Queuing Penalty (veh)		2
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)

Movement	EB	EB	EB	EB	WB	WB	В8	B8	NB	SB	
Directions Served	L	Т	Т	R	Т	TR	T	T	LTR	LTR	
Maximum Queue (ft)	152	291	233	106	283	267	108	68	183	143	
Average Queue (ft)	33	142	94	15	174	162	9	3	84	83	
95th Queue (ft)	94	249	189	59	267	252	(55	30	151	140	
Link Distance (ft)		349	349		199	199	1221	1221	285	105	
Upstream Blk Time (%)		0			4	3				6	
Queuing Penalty (veh)		0			0	0				12	
Storage Bay Dist (ft)	115			100							
Storage Blk Time (%)	0	7	3		19						
Queuing Penalty (veh)	1	5	1		0						

Intersection: 8: Bend

Movement	EB
Directions Served	T
Maximum Queue (ft)	6
Average Queue (ft)	0
95th Queue (ft)	6
Link Distance (ft)	199
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Network Summary

Movement	EBL	EBR	NBL	NBT	SBT	SBR	All
Vehicles Entered	52	48	14	194	140	15	463
Vehicles Exited	52	48	14	194	141	15	464
Hourly Exit Rate	52	48	14	194	141	15	464
Input Volume	53	48	17	198	138	13	466
% of Volume	98	101	82	98	102	118	100

2: Ten Eyck Road & Pleasant Street (E) Performance by movement

Movement	WBL	WBR	NBT	NBR	SBL	SBT	All
Vehicles Entered	12	6	204	20	4	187	433
Vehicles Exited	12	6	205	21	4	187	435
Hourly Exit Rate	12	6	205	21	4	187	435
Input Volume	12	5	211	21	4	184	437
% of Volume	102	114	97	100	94	102	100

3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26) Performance by movement

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Vehicles Entered	167	1289	160	6	1333	19	137	31	8	44	34	120
Vehicles Exited	165	1289	161	6	1338	19	139	32	8	44	34	120
Hourly Exit Rate	165	1289	161	6	1338	19	139	32	8	44	34	120
Input Volume	178	1292	158	6	1331	19	137	28	8	45	33	118
% of Volume	93	100	102	100	101	99	101	115	97	98	103	102

3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26) Performance by movement

Movement	All
Vehicles Entered	3348
Vehicles Exited	3355
Hourly Exit Rate	3355
Input Volume	3354
% of Volume	100

Vehicles Entered	3433
Vehicles Exited	3436
Hourly Exit Rate	3436
Input Volume	10386
% of Volume	33

Movement	EB	NB	SB
Directions Served	LR	LT	TR
Maximum Queue (ft)	100	58	75
Average Queue (ft)	39	3	5
95th Queue (ft)	72)	26	36
Link Distance (ft)	624	59	201
Upstream Blk Time (%)		0	
Queuing Penalty (veh)		0	
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 2: Ten Eyck Road & Pleasant Street (E)

Movement	WB	NB	SB
Directions Served	LR	TR	LT
Maximum Queue (ft)	44	9	91
Average Queue (ft)	15	0	25
95th Queue (ft)	41)	7	78
Link Distance (ft)	599	106	59
Upstream Blk Time (%)			7
Queuing Penalty (veh)			12
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)

Movement	EB	EB	EB	EB	WB	WB	WB	B8	B8	NB	SB	
Directions Served	L	Т	Т	R	L	T	TR	T	Т	LTR	LTR	
Maximum Queue (ft)	214	437	402	200	67	292	289	365	342	297	142	
Average Queue (ft)	127	215	186	52	7	257	247	111	84	153	109	
95th Queue (ft)	224	368	340	159	39	308	314	(280	246)	268	157	
Link Distance (ft)		700	700			200	200	1221	1221	882	106	
Upstream Blk Time (%)					0	24	20				25	
Queuing Penalty (veh)					0	0	0				49	
Storage Bay Dist (ft)	115			100	105							
Storage Blk Time (%)	15	14	13	0		36						
Queuing Penalty (veh)	98	25	20	0		2						

Network Summary

Movement	EBL	EBR	NBL	NBT	SBT	SBR	All
Vehicles Entered	16	24	17	58	166	24	305
Vehicles Exited	16	24	17	58	167	25	307
Hourly Exit Rate	16	24	17	58	167	25	307
Input Volume	18	24	19	54	169	21	306
% of Volume	89	101	88	106	99	118	100

2: Ten Eyck Road & Pleasant Street (E) Performance by movement

Movement	WBL	NBT	NBR	SBT	All	
Vehicles Entered	7	79	38	195	319	
Vehicles Exited	7	78	38	195	318	
Hourly Exit Rate	7	78	38	195	318	
Input Volume	8	78	38	196	320	
% of Volume	90	100	99	100	100	

3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26) Performance by movement

Movement	EBL	EBT	EBR	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	All
Vehicles Entered	87	974	40	1102	23	160	4	2	25	14	163	2594
Vehicles Exited	87	977	40	1103	23	161	4	2	25	15	163	2600
Hourly Exit Rate	87	977	40	1103	23	161	4	2	25	15	163	2600
Input Volume	88	982	39	1106	22	160	4	2	26	14	166	2608
% of Volume	99	99	103	100	106	101	100	100	97	105	98	100

Vehicles Entered	2639	
Vehicles Exited	2650	
Hourly Exit Rate	2650	
Input Volume	8011	
% of Volume	33	

Movement	EB	NB	SB
Directions Served	LR	LT	TR
Maximum Queue (ft)	55	52	12
Average Queue (ft)	23	5	1
95th Queue (ft)	49)	28	8
Link Distance (ft)	624	59	201
Upstream Blk Time (%)		0	
Queuing Penalty (veh)		0	
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 2: Ten Eyck Road & Pleasant Street (E)

Movement	WB	NB	SB
Directions Served	LR	TR	LT
Maximum Queue (ft)	33	9	75
Average Queue (ft)	7	0	8
95th Queue (ft)	28)	6	42
Link Distance (ft)	599	105	59
Upstream Blk Time (%)			1
Queuing Penalty (veh)			2
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)

Movement	EB	EB	EB	EB	WB	WB	B8	B8	NB	SB	
Directions Served	L	T	Т	R	T	TR	T	T	LTR	LTR	
Maximum Queue (ft)	149	310	233	55	272	269	98	75	204	141	
Average Queue (ft)	44	143	96	12	190	173	11	5	91	85	
95th Queue (ft)	109	251	193	40	283	267	(56	37	164	143	
Link Distance (ft)		349	349		199	199	1221	1221	285	105	
Upstream Blk Time (%)		0			6	4			0	7	
Queuing Penalty (veh)		0			0	0			0	13	
Storage Bay Dist (ft)	115			100							
Storage Blk Time (%)	0	7	3	0	22						
Queuing Penalty (veh)	2	7	1	0	0						

Intersection: 8: Bend

Movement	EB
Directions Served	T
Maximum Queue (ft)	6
Average Queue (ft)	0
95th Queue (ft)	6
Link Distance (ft)	199
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Network Summary

Movement	EBL	EBR	NBL	NBT	SBT	SBR	All
Vehicles Entered	56	46	18	196	142	12	470
Vehicles Exited	56	46	18	196	143	12	471
Hourly Exit Rate	56	46	18	196	143	12	471
Input Volume	53	48	17	198	138	13	466
% of Volume	106	96	106	99	103	94	101

2: Ten Eyck Road & Pleasant Street (E) Performance by movement

Movement	WBL	WBR	NBT	NBR	SBL	SBT	All
Vehicles Entered	33	7	208	27	4	186	465
Vehicles Exited	34	6	210	27	4	186	467
Hourly Exit Rate	34	6	210	27	4	186	467
Input Volume	34	5	212	30	4	184	468
% of Volume	100	114	99	91	94	101	100

3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26) Performance by movement

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Vehicles Entered	180	1297	162	5	1350	20	136	29	8	45	35	141
Vehicles Exited	179	1298	163	5	1354	20	137	29	8	45	36	141
Hourly Exit Rate	179	1298	163	5	1354	20	137	29	8	45	36	141
Input Volume	186	1292	158	6	1331	20	137	28	8	47	34	138
% of Volume	96	100	103	83	102	99	100	105	97	96	107	102

3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26) Performance by movement

Movement	All	
Vehicles Entered	3408	
Vehicles Exited	3415	
Hourly Exit Rate	3415	
Input Volume	3386	
% of Volume	101	

Vehicles Entered	3490
Vehicles Exited	3494
Hourly Exit Rate	3494
Input Volume	10484
% of Volume	33

Movement	EB	NB	SB
Directions Served	LR	LT	TR
Maximum Queue (ft)	131	46	96
Average Queue (ft)	42	4	9
95th Queue (ft)	97	28	56
Link Distance (ft)	624	59	201
Upstream Blk Time (%)		0	0
Queuing Penalty (veh)		0	0
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 2: Ten Eyck Road & Pleasant Street (E)

Movement	WB	NB	SB
Directions Served	LR	TR	LT
Maximum Queue (ft)	128	24	89
Average Queue (ft)	39	1	32
95th Queue (ft)	102)	16	88
Link Distance (ft)	599	106	59
Upstream Blk Time (%)		0	10
Queuing Penalty (veh)		0	20
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)

Movement	EB	EB	EB	EB	WB	WB	WB	B8	B8	NB	SB	
Directions Served	L	T	T	R	L	Т	TR	T	T	LTR	LTR	
Maximum Queue (ft)	215	556	500	200	126	304	307	371	336	284	145	
Average Queue (ft)	147	254	213	58	8	259	249	116	90	145	115	
95th Queue (ft)	243	470	419	170	54	316	314	284	251)	248	158	
Link Distance (ft)		700	700			200	200	1221	1221	882	106	
Upstream Blk Time (%)		0	0		0	24	20				34	
Queuing Penalty (veh)		0	0		0	0	0				76	
Storage Bay Dist (ft)	115			100	105							
Storage Blk Time (%)	23	15	14	0	0	35						
Queuing Penalty (veh)	148	28	22	0	0	2						

Intersection: 8: Bend

Movement	EB	EB
Directions Served	T	T
Maximum Queue (ft)	6	11
Average Queue (ft)	0	0
95th Queue (ft)	6	8
Link Distance (ft)	200	200
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Network Summary

Movement	EBL	EBR	NBL	NBT	SBT	SBR	All
Vehicles Entered	18	26	17	56	172	24	313
Vehicles Exited	18	26	17	56	172	24	313
Hourly Exit Rate	18	26	17	56	172	24	313
Input Volume	18	24	19	54	169	21	306
% of Volume	100	109	88	103	102	113	102

2: Ten Eyck Road & Pleasant Street (E) Performance by movement

Movement	WBL	NBT	NBR	SBT	All
Vehicles Entered	7	78	36	201	322
Vehicles Exited	7	78	37	201	323
Hourly Exit Rate	7	78	37	201	323
Input Volume	8	78	38	196	320
% of Volume	90	100	97	103	101

3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26) Performance by movement

Movement	EBL	EBT	EBR	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	All
Vehicles Entered	88	993	39	1119	21	165	4	4	24	13	173	2643
Vehicles Exited	87	993	39	1123	21	165	4	4	24	13	173	2646
Hourly Exit Rate	87	993	39	1123	21	165	4	4	24	13	173	2646
Input Volume	88	982	39	1106	22	160	4	2	26	14	166	2608
% of Volume	99	101	100	102	97	103	100	200	93	91	104	101

Vehicles Entered	2691
Vehicles Exited	2693
Hourly Exit Rate	2693
Input Volume	8011
% of Volume	34

Movement	EB	NB	SB
Directions Served	LR	LT	TR
Maximum Queue (ft)	58	46	19
Average Queue (ft)	24	5	1
95th Queue (ft)	49)	27	17
Link Distance (ft)	624	59	201
Upstream Blk Time (%)		0	
Queuing Penalty (veh)		0	
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 2: Ten Eyck Road & Pleasant Street (E)

Movement	WB	SB
Directions Served	LR	LT
Maximum Queue (ft)	34	41
Average Queue (ft)	7	2
95th Queue (ft)	28)	20
Link Distance (ft)	601	59
Upstream Blk Time (%)		0
Queuing Penalty (veh)		1
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)

Movement	EB	EB	EB	EB	WB	WB	B8	B8	NB	SB	SB	
Directions Served	L	Т	Т	R	Т	TR	T	Т	LTR	L	TR	
Maximum Queue (ft)	193	301	242	80	275	262	143	113	202	81	130	
Average Queue (ft)	47	139	92	12	190	176	16	10	90	22	67	
95th Queue (ft)	119	252	195	49	285	268	(84	65	158	60	118	
Link Distance (ft)		341	341		192	192	1221	1221	285	104	104	
Upstream Blk Time (%)		0	0		7	6				0	3	
Queuing Penalty (veh)		0	0		0	0				0	3	
Storage Bay Dist (ft)	115			100								
Storage Blk Time (%)	0	7	3	0	22							
Queuing Penalty (veh)	2	6	1	0	0							

Network Summary

Movement	EBL	EBR	NBL	NBT	SBT	SBR	All
Vehicles Entered	50	48	17	198	144	14	471
Vehicles Exited	51	48	17	198	145	14	473
Hourly Exit Rate	51	48	17	198	145	14	473
Input Volume	53	48	17	198	138	13	466
% of Volume	96	101	100	100	105	110	101

2: Ten Eyck Road & Pleasant Street (E) Performance by movement

Movement	WBL	WBR	NBT	NBR	SBL	SBT	All
Vehicles Entered	31	5	212	29	4	191	472
Vehicles Exited	32	5	213	29	4	191	474
Hourly Exit Rate	32	5	213	29	4	191	474
Input Volume	34	5	212	30	4	184	468
% of Volume	94	95	101	97	94	104	101

3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26) Performance by movement

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Vehicles Entered	190	1277	152	6	1336	20	136	23	8	45	38	141
Vehicles Exited	190	1279	153	5	1340	20	139	24	8	44	38	140
Hourly Exit Rate	190	1279	153	5	1340	20	139	24	8	44	38	140
Input Volume	186	1292	158	6	1331	20	137	28	8	47	34	138
% of Volume	102	99	97	83	101	99	101	86	97	94	113	101

3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26) Performance by movement

Movement	All
Vehicles Entered	3372
Vehicles Exited	3380
Hourly Exit Rate	3380
Input Volume	3386
% of Volume	100

Vehicles Entered	3449
Vehicles Exited	3456
Hourly Exit Rate	3456
Input Volume	10484
% of Volume	33

Movement	EB	NB	SB
Directions Served	LR	LT	TR
Maximum Queue (ft)	95	56	56
Average Queue (ft)	38	5	4
95th Queue (ft)	70)	33	32
Link Distance (ft)	624	59	201
Upstream Blk Time (%)		0	
Queuing Penalty (veh)		0	
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 2: Ten Eyck Road & Pleasant Street (E)

Movement	WB	NB	SB
Directions Served	LR	TR	LT
Maximum Queue (ft)	96	40	86
Average Queue (ft)	28	2	14
95th Queue (ft)	68	21	59
Link Distance (ft)	601	104	59
Upstream Blk Time (%)		0	3
Queuing Penalty (veh)		0	6
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 3: Wolf Drive/Ten Eyck Road & Mt. Hood Highway (US 26)

Movement	EB	EB	EB	EB	WB	WB	WB	B8	B8	NB	SB	SB
Directions Served	L	Т	Т	R	L	Т	TR	Т	Т	LTR	L	TR
Maximum Queue (ft)	215	550	490	200	128	302	289	376	353	280	102	144
Average Queue (ft)	145	240	197	50	10	253	242	121	94	147	36	86
95th Queue (ft)	239	440	385	153	64	306	302	303	281)	247	85	147
Link Distance (ft)		692	692			193	193	1221	1221	881	104	104
Upstream Blk Time (%)		0			0	25	20				1	13
Queuing Penalty (veh)		0			0	0	0				1	15
Storage Bay Dist (ft)	115			100	105							
Storage Blk Time (%)	24	14	13	0		35						
Queuing Penalty (veh)	153	26	20	0		2						

Network Summary

Appendix D Crash History

CDS380 OREGON DEPARTMENT OF TRANSPORTATION - TRANSPORTATION DEVELOPMENT DIVISION Page: 1

TRANSPORTATION DATA SECTION - CRASH ANAYLYSIS AND REPORTING UNIT

CONTINUOUS SYSTEM CRASH LISTING

026: MT. HOOD Highway 026 ALL ROAD TYPES, MP 24.61 to 24.64 01/01/2014 to 12/31/2018, Both Add and Non-Add mileage

1 - 4 of 11 Crash records shown.

S D M																				
SER# P R J S	W DATE	COUNTY	RD# FC CONN#	RD CHAR	INT-TYPE	3				SPCL USE										
INVEST E A U I C	O DAY	CITY	COMPNT FIRST STREET	DIRECT	(MEDIAN)) INT-REL	OFFRD	WTHR	CRASH	TRLR QTY	MOVE				A S					
RD DPT E L G N H	R TIME	URBAN AREA	MLG TYP SECOND STREET	LOCTN	LEGS	TRAF-	RNDBT	SURF	COLL	OWNER	FROM	PRTC	INJ		3 E	LICNS	PED			
UNLOC? D C S V L	K LAT	LONG	MILEPNT LRS		(#LANES)	CONTL	DRVWY	LIGHT	SVRTY	V# TYPE	TO	P# TYPE	SVR	TY	E X	RES	LOC	ERROR	ACT EVENT	CAUSE
03162 N N N N	08/16/2014	CLACKAMAS	1 14	INTER	5-LEG	N	N	CLR	S-1STOP	01 NONE 0	STRGHT									29
NO RPT	SA	SANDY	MN 0 PIONEER BLVD	E		TRF SIGNAL	N	DRY	REAR	UNKN	E -W								000	00
N	4P	SANDY UA	24.61 SE TEN EYCK RD	06	0		N	DAY	INJ	MTRCYCLE		01 DRVR	NON	E 0) M	UNK		026	000	29
N	45 23 49.25	-122 15 19.74	002600100S00													UNK				
										02 NONE 0	STOP									
										PRVTE	E -W								011	00
										PSNGR CAR		01 DRVR	NON	E 7	2 M	OR-Y OR<25	5	000	000	00
										02 NONE 0	STOP									
										PRVTE	E -W								011	00
										PSNGR CAR		02 PSNG	INJ	C 6	l F			000	000	00
03787 N N N N	N 09/15/2015	CLACKAMAS	1 14	INTER	5-LEG	N	N	CLR	S-1STOP	01 NONE 0	STRGHT									29
NONE	TU	SANDY	MN 0 PIONEER BLVD	E		TRF SIGNAL	N	DRY	REAR	PRVTE	E -W								000	00
N	1P	SANDY UA	24.61 SE TEN EYCK RD	06	0		N	DAY	INJ	PSNGR CAR		01 DRVR	NON	E 7	L M	OR-Y		026	000	29
N	45 23 49.24	-122 15 19.74	002600100800													OR<25	;			
										02 NONE 0	STOP									
										PRVTE	E -W								011	00
										PSNGR CAR		01 DRVR	INJ	C 3	3 F	OTH-Y N-RES		000	000	00
02412 N N N N	06/24/2014	CLACKAMAS	1 14	INTER	5-LEG	N	N	CLR	S-1STOP	01 NONE 0	STRGHT									29
NONE	TU	SANDY	MN 0 PIONEER BLVD	SE		TRF SIGNAL	N	DRY	REAR	PRVTE	SE-NW								000	00
N	8A	SANDY UA	24.61 SE TEN EYCK RD	06	0		N	DAY	INJ	PSNGR CAR		01 DRVR	NON	E 5	5 F	OR-Y		026	000	29
N	45 23 49.25	-122 15 19.74	002600100s00													OR<25	;			
										02 NONE 0	STOP									
										PRVTE	SE-NW								011	00
										PSNGR CAR		01 DRVR	INJ	C 5	F			000	000	00
																OR<25	5			
04899 N N N N N		CLACKAMAS	1 14	STRGHT		Y	N	CLR	S-1STOP	01 NONE 0	STRGHT									10
CITY	TU	SANDY	MN 0 PIONEER BLVD	E	(NONE)	TRF SIGNAL	N	DRY	SS-O	PRVTE	E -W								000	00
N	8A	SANDY UA	24.63 WOLF DR	04			N	DAY	INJ	PSNGR CAR		01 DRVR	INJ	C 4	} F	SUSP		080	026	10
N	45 23 49.07	-122 15 18.32	002600100S00		(04)											OR<25	5			
										02 NONE 0	STOP									
										PUBLC	E -W								011	00
										SCHL BUS		01 DRVR	NON	E 4	l F	OR-Y OR<25		000	000	00
00248 N N N N	01/20/2018	CLACKAMAS	1 14	STRGHT		N	N	CLD	S-1STOP	01 NONE 0	STRGHT								003	07,29
CITY	SA	SANDY	MN 0 PROCTOR BLVD	SE	(NONE)	NONE	N	DRY	REAR	PRVTE	SE-NW								000	00
И	3P	SANDY UA	24.64 WOLF DR	05			N	DAY	INJ	PSNGR CAR		01 DRVR	NON	E 2	2 F	OR-Y		043,026	038 003	07,29
N	45 23 48.99	-122 15 17.63	002600100S00		(04)											OR>25	5			

CDS380 OREGON DEPARTMENT OF TRANSPORTATION - TRANSPORTATION DEVELOPMENT DIVISION Page: 3

TRANSPORTATION DATA SECTION - CRASH ANAYLYSIS AND REPORTING UNIT

CONTINUOUS SYSTEM CRASH LISTING

026: MT. HOOD Highway 026 ALL ROAD TYPES, MP 24.61 to 24.64 01/01/2014 to 12/31/2018, Both Add and Non-Add mileage

5 - 9 of 11 Crash records shown.

	S D M																			
SER#	P RJS	W DATE	COUNTY	RD# FC CONN#	RD CHAR	INT-TYPE					SPCL USE									
INVEST	EAUIC	O DAY	CITY	COMPNT FIRST STREET	DIRECT	(MEDIAN)	INT-REL	OFFRD	WTHR	CRASH	TRLR QTY	MOVE			А	S				
	ELGNH		URBAN AREA	MLG TYP SECOND STREET	LOCTN	LEGS	TRAF-	RNDBT		COLL	OWNER	FROM	PRTC	INJ		E LICNS	PED			
	D C S V L		LONG	MILEPNT LRS	200111	(#LANES)			LIGHT		V# TYPE	TO	P# TYPE				LOC	ERROR	ACT EVENT	CAUSE
											02 NONE 0	STOP								
											PRVTE	SE-NW							011	00
											PSNGR CAR		01 DRVR	INJC	43 M			000	000	00
											02 NONE 0	STOP				OR<25				
											PRVTE	SE-NW							011	00
											PSNGR CAR		02 PSNG	INJC	35 F			000	000	00
											02 NONE 0	STOP								
											PRVTE	SE-NW							011	00
											PSNGR CAR		03 PSNG	NONE	04 M			000	000	00
	N N N N	10/14/2014	CLACKAMAS	1 14	INTER	6-LEG	N	N	RAIN	S-1STOP	01 NONE 0	STRGHT							0.00	29
NO RPT		TU	SANDY	CP 0 PIONEER BLVD	W		TRF SIGNAL	N	WET	REAR	UNKN	W -E							000	00
N		6A	SANDY UA	24.61 WOLF DR	06	0		N	DLIT	INJ	PSNGR CAR		01 DRVR	NONE	00 M	OR-Y		026	000	29
NT		45 22 40 25	100 15 10 74	002600100S00												TINTE				
N		45 23 49.25	-122 15 19.74	002600100800							02 NONE 0	STOP				UNK				
											PRVTE	W -E							011	00
											PSNGR CAR		01 DRVR	INJC	70 M	OR-Y		000	000	00
																OR<25				
03023	N N N N N	N 08/06/2014	CLACKAMAS	1 14	INTER	5-LEG	N	N	CLR	ANGL-OTH	01 NONE 0	STRGHT							082	04
CITY		WE	SANDY	CP 0 PIONEER BLVD	CN		TRF SIGNAL	N	DRY	ANGL	PRVTE	W -E							000	00
37		1.0	CANDY III	24 61 WOLE DD	0.2	0		37	D311	DDO	DOMOD GAD		01 DDID	MONTE	10 5	00 11		000	000	0.0
N		1P	SANDY UA	24.61 WOLF DR	03	0		N	DAY	PDO	PSNGR CAR		01 DRVR	NONE	19 F	OR-Y		000	000	00
N		45 23 49.25	-122 15 19.74	002600100500												OR<25				
											02 NONE 0	STRGHT								
											PRVTE	N -S							000	00
											PSNGR CAR		01 DRVR	NONE	59 M			020	000 082	04
																OR<25				
	N N N N N		CLACKAMAS	1 14	INTER	5-LEG	N	N	CLR	ANGL-OTH	01 NONE 0	STRGHT							0.00	04
NONE		SA	SANDY	CP 0 PIONEER BLVD	CN		TRF SIGNAL	N	DRY	ANGL	PRVTE	S -N							000	00
N		6A	SANDY UA	24.61 WOLF DR	04	0		N	DAY	PDO	PSNGR CAR		01 DRVR	NONE	25 M	OTH-Y		020	026	04
NT		4E 22 40 2E	100 15 10 74	002600100500												OD - 2E				
N		40 40 49.40	-122 15 19.74	002600100S00							02 NONE 0	STRGHT				OR<25				
											PRVTE	W -E							000	00
											PSNGR CAR		01 DRVR	NONE	51 F	OR-Y		000	000	00
																OR<25				
00512	NNNNN	N 02/07/2017	CLACKAMAS	1 14	INTER	5-LEG	N	N	RAIN	ANGL-OTH	01 NONE 0	TURN-L								04
CITY		TU	SANDY	CP 0 PIONEER BLVD	CN		TRF SIGNAL	N	WET	TURN	PRVTE	S -W							000	00
3.7		4.5	CANDY III	24 61 WOLE DD	0.4	0		37	DIIGI	T.N. T	DOMOD GAD		01 DDID	TNT0	FF 5	OD 11		000	000	0.0
N		4P	SANDY UA	24.61 WOLF DR	04	0		N	DUSK	TNU	PSNGR CAR		01 DRVR	INJC	55 F	OK-Y		000	000	00
N		45 23 49.25	-122 15 19.74	002600100800												OR<25				
											02 NONE 0	STRGHT								
											PRVTE	M -E							000	00
											PSNGR CAR		01 DRVR	NONE	63 M			020	000	04
																OR>25				

TRANSPORTATION DATA SECTION - CRASH ANAYLYSIS AND REPORTING UNIT

CONTINUOUS SYSTEM CRASH LISTING

026: MT. HOOD Highway 026 ALL ROAD TYPES, MP 24.61 to 24.64 01/01/2014 to 12/31/2018, Both Add and Non-Add mileage

10 - 11 of 11 Crash records shown.

S D M																				
SER# P R J S	W DATE	COUNTY	RD# FC	CONN#	RD CHAR	INT-TYPE					SPCL USE									
INVEST E A U I C	O DAY	CITY	COMPNT	FIRST STREET	DIRECT	(MEDIAN)	INT-REL	OFFRD	WTHR	CRASH	TRLR QTY	MOVE			A	S				
RD DPT E L G N H	R TIME	URBAN AREA	MLG TYP	SECOND STREET	LOCTN	LEGS	TRAF-	RNDBT	SURF	COLL	OWNER	FROM	PRTC	INJ	G	E LICNS	S PED			
UNLOC? D C S V L	K LAT	LONG	MILEPNI	LRS		(#LANES)	CONTL	DRVWY	LIGHT	SVRTY	V# TYPE	TO	P# TYPE	SVRTY	E	X RES	LOC	ERROR	ACT EVENT	CAUSE
03089 N N N N	09/03/2018	CLACKAMAS	2 14	Į.	INTER	5-LEG	N	N	CLR	S-1STOP	01 NONE 0	STRGHT								29
NONE	MO	SANDY	MN 0	PROCTOR BLVD	SE		TRF SIGNAL	N	DRY	REAR	UNKN	SE-NW							000	00
N	3P	SANDY UA	24.63	SE TEN EYCK RD	06	0		N	DAY	INJ	PSNGR CAR		01 DRVR	NONE	00 F	UNK		026	000	29
N	45 23 49.25	-122 15 19.75		002600200S00												UNK				
											02 NONE 0	STOP								
											PRVTE	SE-NW							011	00
											PSNGR CAR		01 DRVR	INJC	25 F	OR-Y		000	000	00
																OR>25	5			
05173 N N N N	11/08/2016	CLACKAMAS	2 14	Į.	INTER	5-LEG	N	N	CLR	ANGL-OTH	01 NONE 9	U-TURN								06
NONE	TU	SANDY	CP 0	PROCTOR BLVD	М		TRF SIGNAL	N	DRY	TURN	N/A	M - M							000	00
N	5P	SANDY UA	24.63	SE TEN EYCK RD	05	0		N	DUSK	PDO	PSNGR CAR		01 DRVR	NONE	00 U	nk UNK		000	000	00
N	45 23 49.25	-122 15 19.74		002600200s00		(02)										UNK				
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											N/A	NE-W							000	00
											PSNGR CAR		01 DRVR	NONE	00 U	nk UNK		000	000	00

UNK

General & Site Information									
Analyst:	John Manix PE								
Agency/Company:	PBS Engineering and Env.								
Date:	3/10/2020								
Project Name:	Sandy Health Clinic								

		Intersecti	on Crash Data	l			
	Intersection			Year			
Intersection	Type Urban 4SG	2014	2015	2016	2017	2018	Total
Highway 26 and Ten Eyck	Urban 4SG	4	2	1	1	3	11
							0
							0
							0
							0
							0
							0
							0
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							0
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							0
							0
							0
							0
							0
	Total	4	2	1	1	3	11

Intersection P	Intersection Population Type Crash Rate								
Average Crash	Average Crash Rate per intersection type								
			Avg Crash						
	Sum of	Sum of 5-	Rate for Ref						
Intersection Pop. Type	Crashes	year MEV	Pop.	INT in Pop					
Rural 3SG	0	0							
Rural 3ST	0	0							
Rural 4SG	0	0							
Rural 4ST	0	0							
Urban 3ST	0	0							
Urban 3SG	0	0							
Urban 4ST	0	0							
Urban 4SG	11	43	0.2567	1					

			Critical Rate	Calculation				
				Intersection		Reference		
	AADT Entering			Population	Intersection	Population Crash	Critical	Over
Intersection	Intersection	5-year MEV	Crash Total	Type	Crash Rate	Rate	Rate	Critical
Highway 26 and Ten Eyck	23,480	42.9	11	Urban 4SG	0.26	0.26	0.40	Under
<u> </u>		ļ						



Deborah Cockrell, FOHC Director Clackamas Health Centers

Administration
Public Service Building
2051 Kaen Road, Suite 367
Oregon City, OR 97045-4035
503-742-5300

Beavercreek Health Center 110 Beavercreek Road Oregon City, OR 97045-4023 503-655-8471 Primary Care, Dental Services and Behavioral Health

Sunnyside Health Center 9775 SE Sunnyside Road Suite 200 Clackamas, OR 97015-5721 503-655-8471 Primary Care, Dental Services and Behavioral Health

Gladstone Health Clinic 18911 Portland Avenue Gladstone, OR 97027-1630 503-850-4472 Primary Care, Pediatrics, Dental Services and Behavioral Health

Sandy Health Clinic 37400 SE Bell Street Sandy, OR 97055-7868 503-668-3493 Primary Care and Behavioral Health

Hilltop Behavioral Health Clinic 998 Library Court Oregon City, OR 97045-4041 503-655-8401

Stewart Behavioral Health Clinic 1002 Library Court Oregon City, OR 97045-4066 503-655-8264

> Sandy Behavioral Health Clinic 38872 Proctor Boulevard PO Box 1390 Sandy, OR 97055-8035 503-722-6950

School Based Health Centers
Oregon City High School
19761 S Beavercreek Road
Oregon City, OR 97045-9557
503-785-8770

Rex Putnam High School 4950 SE Roethe Rd. Milwaukie, OR 97267-5746 503-722-6858

> **Sandy High School** 37400 Bell Street Sandy, OR 97055-7868 503-668-3483

February 10, 2020

Police Chief Ernie Roberts Sandy Police Department 39850 Pleasant Street Sandy, Oregon 97055

RE: SIX SHARED PARKING SPACES ALIGNED ON THE PROPERTY LINE BETWEEN OUR PROPERTIES

Dear Chief Roberts:

This letter is to communicate openly with your office regarding the six shared parking spaces, along your west property line. At the time of our interest in the vacant building (i.e. property) adjacent to your precinct, we were informed by the seller(s) of the existing six shared parking spaces agreement that was established some time ago. The City of Sandy Design Review Process requires the County to maintain the use of the existing six shared parking spaces.

Our architectural firm, Ankrom Moisan Architects, Inc. on our behalf is working with the City of Sandy Planning Office to meet their requirements for our new building design. At this point, we are unaware of an exact start of our construction schedule for the New Sandy Health Clinic. However, the construction project will occur sometime in 2020-2021. As soon as our project is released to the public via the bidding process to contractors, we will alert your office of our planned steps and keep you apprised of an established construction schedule, once we receive bids. Once a general contractor is hired, we will need to use the parking spaces between our property lines for staging for the project. We are hopeful this is an allowable request.

In regards to the shared parking spaces, no employee will park there in the future, once the new building opens to the public. Only patients will be parking in our new lot and periodically using the shared parking spaces. Attached please find the proposed building site plan, which includes the shared parking spaces.

It is the County's full intention to be good neighbors of the Sandy Police Department. If you have questions, I can reach me at my office phone number 503-742-5495. The assigned Project Coordinator is Steve Kelly and his phone number is 503-650-5665. Thank you for your valuable time.

Sincerely,

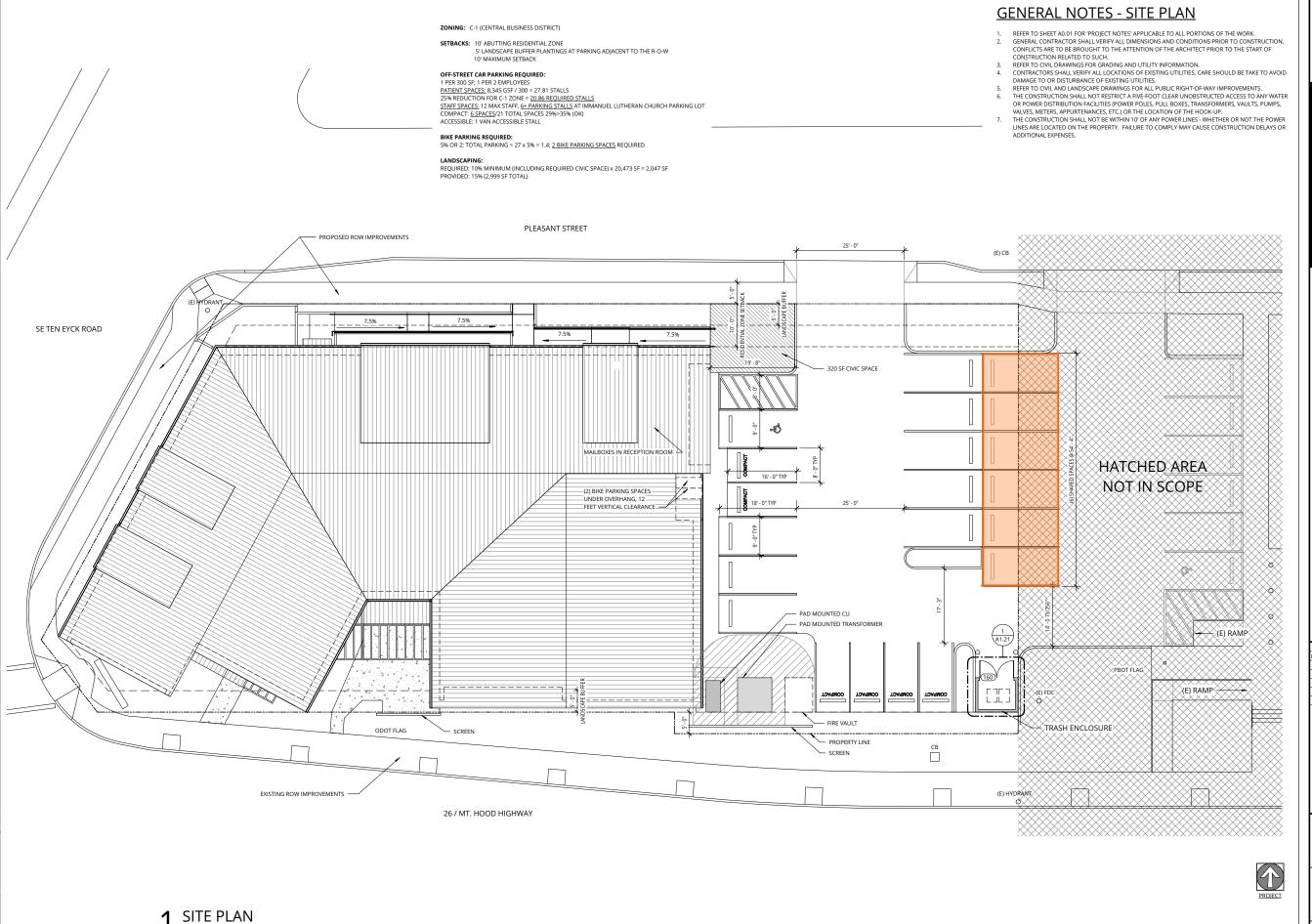
Deborah Cockrell, FQHC Health Centers, Director

Cc: Steve Kelly, Project Coordinator

Ankrom Moisan Architects, Inc.

Healthy Families. Strong Communities.

2051 Kaen Road, Oregon City, OR 97045 • www.clackamas.us/healthcenters
Phone (503) 742-5300 • Fax (503) 742-5979







38 NORTHWEST DAVIS, SUITE 300 PORTLAND, OR 97209 503.245.7100

1505 5TH AVE. SUITE 300 SEATTLE, WA 98101 206.576.1600

1014 HOWARD STREET SAN FRANCISCO, CA 94103 415.252.7063

© ANKROM MOISAN ARCHITECTS, INC.

SANDY HEALTH CLINIC 39831 HIGHWAY 26 SANDY, OR 97055

REASON FOR ISSUE

SITE PLAN

DESIGN **DEVELOPMENT**

1.24.2020

PROJECT NUMBER 192530

A1.01

PARKING SPACE LEASE AGREEMENT

This agreement is made and entered into this day of, 2020, by and between Immanuel Lutheran Church ("Owner") and Clackamas County ("County") for the lease of Seventeen (17) parking spaces, in the south parking lot across Pleasant Street from property described as Lots One (1) to including Lot Twelve (12), Block Two (2), Minnie Meinig's Pine View Tracts and commonly known as 39901 Pleasant Street, Sandy OR 97055 (map attached).
Owner represents that it has the right to lease these parking spaces to the County for the County's exclusive use, subject to the following terms and conditions.
1. Term . The lease shall commence on, 2020 and shall end on, 2027. County shall be allowed use of the spaces between the hours of 6am to 8pm, Monday through Friday.
2. Hold Over. If County shall hold over and remain in possession of said premises after expiration of this Lease without any written lease actually being made, such holding over shall not be deemed to operate as a renewal or extension of this Lease but shall only create a tenancy which may be terminated at any time by Owner upon sixty (60) days written notice to County.
3. Renewal . This Lease may be renewed for successive seven (7) year terms ("Renewal Term") by mutual written agreement of the parties, executed not less than six (6) months prior to the expiration of the Initial Term or any Renewal Term, as applicable.
4. Use. County will use the leased parking spaces only for the parking of vehicles. Owner will provide County with exclusive use of the leased parking spaces, and Owner will provide signage indicating that these spaces are reserved for County use during the hours of operation noted in 1. Above. County shall be entitled to full use and possession of the parking spaces for the entire lease term.
5. Fees and Payment . The annual fee will be \$6,000 per year. Payment is due on the first day of and is payable by the 14 th day of A late fee of \$100 will be assessed on the 15 th day of if payment has not been received by the 14 th day. No deposit is required. Checks for payment should be made payable to:
Immanuel Lutheran Church 39901 Pleasant Street

- **6. Property Taxes and other expenses.** Owner is solely responsible for property taxes or other expenses such as electric bill for lighting (if any) on the leased parking spaces.
- **7. Maintenance.** County shall be responsible for any necessary trash collection, sweeping, or maintenance of the leased parking spaces. Owner shall be responsible for all other necessary maintenance of the leased parking spaces.

8. Termination.

- **a.** Either party may terminate the Lease upon occurrence of an event of default. An event of default shall be deemed to occur should any of the following events happen:
 - 1. Failure of County to pay lease fees within 30 days from written notice by Owner to County that lease fees are overdue;
 - Repeated failure of County or its employees to obey reasonable rules of the Owner concerning matters of security, safety, or preservation of the Owner's facilities, during the term of the Agreement; or
 - 3. Failure of either party to comply with any term or condition of this Agreement.

In the event of default, the defaulting party shall be given notice of the default in writing by the other party. The party which has been given notice of default shall have 30 days to correct said default. If the default is not corrected within the 30 day notice period, the other party shall have the right to terminate this lease by giving written notice of uncorrected default and termination to the defaulting party. Any notice shall be given by in writing through certified mail, and shall be effective upon receipt. Notice shall be sent to the address for the receiving party as designated herein.

- **b.** County may terminate this Lease in the event the County fails to receive expenditure authority sufficient to allow County, in the exercise of its reasonable administrative discretion, to continue to make payments for performance of this Lease, or if federal or state laws, regulations or guidelines are modified or interpreted in such a way that County is prohibited from performing under the Lease.
- **c.** Any termination of this Lease shall not prejudice any rights or obligations accrued to the parties prior to termination.
- **9. Constitutional Debt Limitation.** This Lease is expressly subject to the debt limitation of Oregon Counties set forth in Article XI, Section 10 of the Oregon Constitution, and is contingent

upon funds being appropriated therefor. Any provisions herein which would conflict with law are deemed inoperative to that extent.

- **10**. **No Attorney Fees:** In the event any arbitration, action or proceeding, including any bankruptcy proceeding, is instituted to enforce any term of this Lease, each party shall be responsible for its own attorneys' fees and expenses.
- **11. Warrant of Authority:** Owner warrants and represents that it is the sole owner of the leased premises subject to this Lease, and that Owner has full authority to execute this Lease. The undersigned warrants and represents that he/she has full authority to sign on behalf of Owner.

[SIGNATURES TO FOLLOW]

Lessee: CLACKAMAS COUNTY	Lessor: IMMANUEL LUTHERAN CHURCH
Commissioner Jim Bernard, Chair	39901 Pleasant Street
Commissioner Sonya Fischer	Sandy, Oregon 97055
Commissioner Ken Humberston	
Commissioner Paul Savas	
Commissioner Martha Schrader	
Signing on Behalf of the Board.	
 Richard Swift, Director	Duight Beigert Legal Signer
Health, Housing, and Human Services	Dwight Reigert, Legal Signer
Department	
Date	Date
STATE OF OREGON, County of Clackamas) ss	
BE IT REMEMBERED, that on this day	of, 2020, before me, th
undersigned, a Notary Public in and for said C	County and State, personally appeared <u>DWIGHT</u>
REIGERT known to be to be the individual(s)	described in and who executed the within Parking
Space Lease Agreement, and acknowledged t freely and voluntarily.	o me that said individual(s) executed the same
IN TESTIMONY WHEREOF, I have hereunto se and year last about written.	ent my hand and affixed my official seal the day
	NOTARY PUBLIC FOR OREGON

[PROPERTY MAP TO FOLLOW]





MEMORANDUM

DATE:

03/23/2020

BY:

Norm Scheg

SUBJECT:

Stormwater Utility Narrative

PROJECT:

Sandy Health Clinic

PROJECT NO.:

A19188.10

This memorandum is to outline the stormwater requirements for the Sandy Health Clinic project located at 39831 Highway 26, Sandy, OR 97055. The project consists of construction of a 10,940SF building, 5,291SF of pervious parking lot with associated pedestrian pathways and utilities. The total site is 20,204SF and is predominately impervious with an existing building and parking lot. Post construction we will be collecting roof runoff in downspouts that will be hard piped to a drywell. This drywell is "authorized by rule" by Oregon DEQ as it will infiltrate runoff from roofs and a parking lot of less than 50 vehicles. We will be constructing pervious pavement for the parking area as well. Both of these facilities have been modeled utilizing 2" per hour as a basis for storage sizing. Once the site has been cleared, and before construction of any utilities, a Geotechnical Engineer will be retained to test the actual infiltration rates of the native soils to assure they have at least a design infiltration rate of 2" per hour or more. The drywell sizing will be reviewed at that time to see it the annulus of rock can be reduced. The rock under the pervious pavement is the minimum thickness for structural integrity. Attached are HydroCAD calculations verifying the infiltration systems meets the stated requirements. A comprehensive stormwater plan will be submitted with the next submittal.



Pervious Pavement

Pavement Aggregate









A19188.10 - Sandy Health Clinic

Type IA 24-hr 25yr Rainfall=5.00" Printed 3/23/2020

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Page 2

Time span=5.00-48.00 hrs, dt=0.05 hrs, 861 points
Runoff by SBUH method, Split Pervious/Imperv.
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Pervious Pavement

Runoff Area=5,291 sf 100.00% Impervious Runoff Depth>4.19" Tc=0.0 min CN=0/98 Runoff=0.15 cfs 0.042 af

Pond 1P: Pavement Aggregate

Peak Elev=0.00' Storage=16 cf Inflow=0.15 cfs 0.042 af Outflow=0.15 cfs 0.042 af

Total Runoff Area = 0.121 ac Runoff Volume = 0.042 af Average Runoff Depth = 4.19" 0.00% Pervious = 0.000 ac 100.00% Impervious = 0.121 ac

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Printed 3/23/2020

Page 3

Summary for Subcatchment 1S: Pervious Pavement

Runoff

=

0.15 cfs @

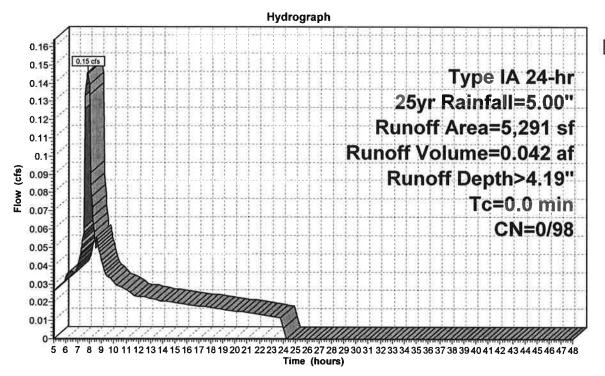
7.80 hrs, Volume=

0.042 af, Depth> 4.19"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type IA 24-hr 25yr Rainfall=5.00"

	Area (sf)	CN	Description	
*	5,291	98	Pervious Pavement	
	5,291	98	100.00% Impervious Area	

Subcatchment 1S: Pervious Pavement



■ Runoff

Prepared by AAI Enginering Inc.

Printed 3/23/2020

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Page 4

Summary for Pond 1P: Pavement Aggregate

Inflow Area = 0.121 ac,100.00% Impervious, Inflow Depth > 4.19" for 25yr event

Inflow = 0.15 cfs @ 7.80 hrs, Volume= 0.042 af

Outflow = 0.15 cfs @ 7.83 hrs, Volume= 0.042 af, Atten= 0%, Lag= 1.8 min

Discarded = 0.15 cfs @ 7.83 hrs, Volume= 0.042 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 0.00' @ 7.83 hrs Surf.Area= 211,640 sf Storage= 16 cf

Plug-Flow detention time= 2.6 min calculated for 0.042 af (100% of inflow)

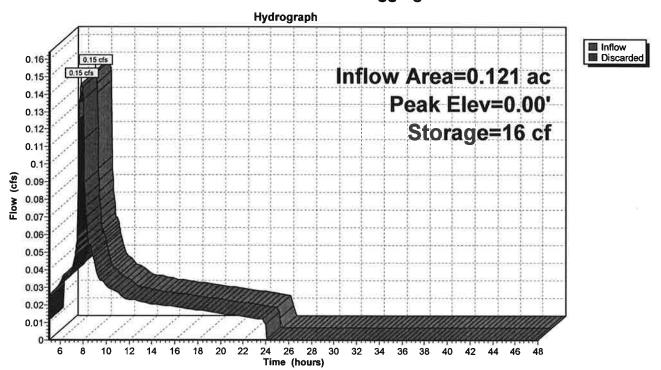
Center-of-Mass det. time= 1.8 min (714.7 - 712.9)

Volume	Invert	Avail.S	Storage	Storage	Description	
#1	0.00'	105	,820 cf	Custon	n Stage Data (Pr	ismatic) Listed below (Recalc) x 40
Elevation (feet)		Area sq-ft)		Store -feet)	Cum.Store (cubic-feet)	
0.00		5,291	(Oubit	0	0	
0.50	5	5.291		2.646	2 646	

Device	Routing	Invert	Outlet Devices	
#1	Discarded	0.00'	2.000 in/hr Exfiltration over Surface area	

Discarded OutFlow Max=9.80 cfs @ 7.83 hrs HW=0.00' (Free Discharge)
1=Exfiltration (Exfiltration Controls 9.80 cfs)

Pond 1P: Pavement Aggregate



A19188.10 - Sandy Health Clinic

Type IA 24-hr 100yr Rainfall=6.00" Printed 3/23/2020

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Time span=5.00-48.00 hrs, dt=0.05 hrs, 861 points
Runoff by SBUH method, Split Pervious/Imperv.
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Pervious Pavement

Runoff Area=5,291 sf 100.00% Impervious Runoff Depth>5.05" Tc=0.0 min CN=0/98 Runoff=0.18 cfs 0.051 af

Pond 1P: Pavement Aggregate

Peak Elev=0.00' Storage=19 cf Inflow=0.18 cfs 0.051 af Outflow=0.18 cfs 0.051 af

Total Runoff Area = 0.121 ac Runoff Volume = 0.051 af Average Runoff Depth = 5.05" 0.00% Pervious = 0.000 ac 100.00% Impervious = 0.121 ac

Page 6

Summary for Subcatchment 1S: Pervious Pavement

Runoff

0.18 cfs @

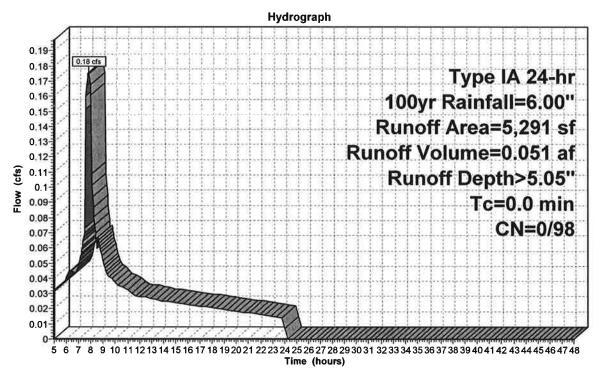
7.80 hrs, Volume=

0.051 af, Depth> 5.05"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type IA 24-hr 100yr Rainfall=6.00"

	Area (sf)	CN	Description	
*	5,291	98	Pervious Pavement	
	5,291	98	100.00% Impervious Area	

Subcatchment 1S: Pervious Pavement



Runoff

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Summary for Pond 1P: Pavement Aggregate

Inflow Area =

0.121 ac,100.00% Impervious, Inflow Depth > 5.05" for 100yr event

Inflow =

0.18 cfs @ 7.80 hrs, Volume=

0.051 af

Outflow =

0.18 cfs @

7.83 hrs, Volume=

0.051 af, Atten= 0%, Lag= 1.8 min

Discarded =

0.18 cfs @

7.83 hrs, Volume=

0.051 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 0.00' @ 7.83 hrs Surf.Area= 211,640 sf Storage= 19 cf

Plug-Flow detention time= 2.6 min calculated for 0.051 af (100% of inflow)

Center-of-Mass det. time= 1.8 min (714.1 - 712.3)

<u>Volume</u>	Invert	Avail.Storage	Storage Description
#1	0.00'	105,820 cf	Custom Stage Data (Prismatic) Listed below (Recalc) x 40

Cum.Store	Inc.Store	Surt.Area	Elevation Surf	
(cubic-feet)	(cubic-feet)	(sq-ft)	(feet)	
0	0	5,291	0.00	
2,646	2,646	5,291	0.50	

Device Routing

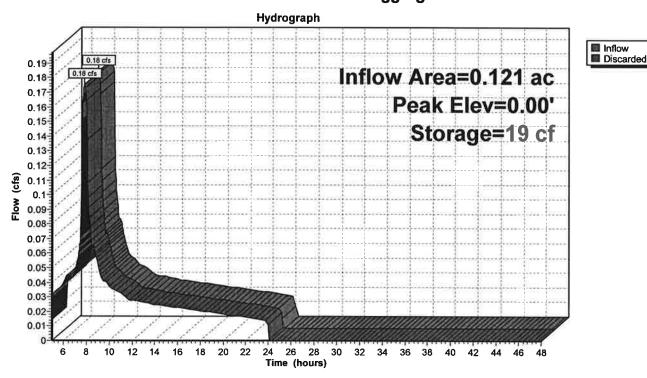
Invert Outlet Devices

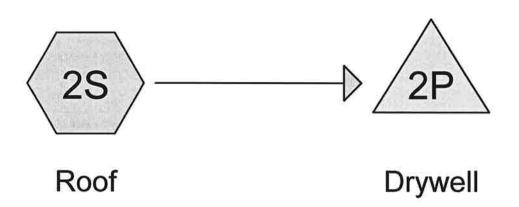
#1 Discarded

0.00' 2.000 in/hr Exfiltration over Surface area

Discarded OutFlow Max=9.80 cfs @ 7.83 hrs HW=0.00' (Free Discharge) 1=Exfiltration (Exfiltration Controls 9.80 cfs)

Pond 1P: Pavement Aggregate













A19188.10 - Sandy Health Clinic

Type IA 24-hr 25yr Rainfall=5.00" Printed 3/23/2020

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Page 2

Time span=5.00-48.00 hrs, dt=0.05 hrs, 861 points
Runoff by SBUH method, Split Pervious/Imperv.
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 2S: Roof

Runoff Area=10,940 sf 100.00% Impervious Runoff Depth>4.19"

Tc=0.0 min CN=0/98 Runoff=0.30 cfs 0.088 af

Pond 2P: Drywell

Peak Elev=12.83' Storage=2,396 cf Inflow=0.30 cfs 0.088 af

Outflow=0.02 cfs 0.074 af

Total Runoff Area = 0.251 ac Runoff Volume = 0.088 af Average Runoff Depth = 4.19" 0.00% Pervious = 0.000 ac 100.00% Impervious = 0.251 ac

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Page 3

Summary for Subcatchment 2S: Roof

Runoff

= 0.3

0.30 cfs @

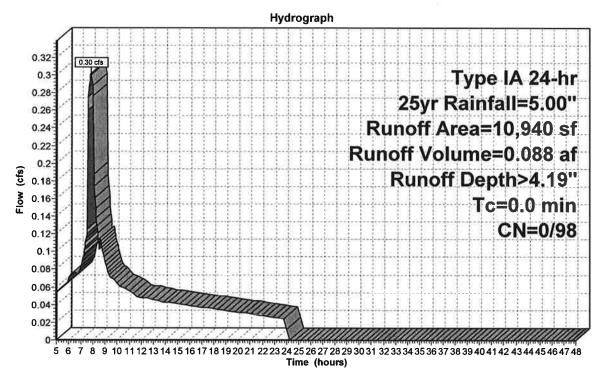
7.80 hrs, Volume=

0.088 af, Depth> 4.19"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type IA 24-hr 25yr Rainfall=5.00"

-	Area (sf)	CN	Description	
*	10,940	98	Roof	
	10.940	98	100 00% Impervious Area	

Subcatchment 2S: Roof



Runoff

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Page 4

Summary for Pond 2P: Drywell

Inflow Area = 0.251 ac,100.00% Impervious, Inflow Depth > 4.19" for 25yr event

Inflow = 0.30 cfs @ 7.80 hrs, Volume= 0.088 af

Outflow = 0.02 cfs @ 5.25 hrs, Volume= 0.074 af, Atten= 93%, Lag= 0.0 min

Discarded = 0.02 cfs @ 5.25 hrs, Volume= 0.074 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 12.83' @ 23.99 hrs Surf.Area= 452 sf Storage= 2,396 cf

Plug-Flow detention time= 982.6 min calculated for 0.074 af (85% of inflow) Center-of-Mass det. time= 880.4 min (1,593.3 - 712.9)

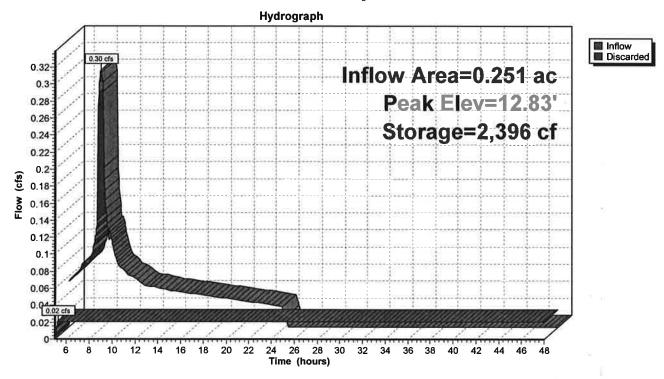
Volume	Invert	Avail.Storage	Storage Description
#1	0.00'	3,482 cf	24.00'D x 20.00'H Vertical Cone/Cylinder
			9,048 cf Overall - 342 cf Embedded = 8,706 cf x 40.0% Voids
#2	0.00'	251 cf	4.00'D x 20.00'H Vertical Cone/Cylinder Inside #1
_			342 cf Overall - 4.0" Wall Thickness = 251 cf

3,734 cf Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	0.00'	2.000 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.02 cfs @ 5.25 hrs HW=0.23' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.02 cfs)

Pond 2P: Drywell



A19188.10 - Sandy Health Clinic

Prepared by AAI Enginering Inc.

Type IA 24-hr 100yr Rainfall=6.00" Printed 3/23/2020

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Time span=5.00-48.00 hrs, dt=0.05 hrs, 861 points
Runoff by SBUH method, Split Pervious/Imperv.
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 2S: Roof

Runoff Area=10,940 sf 100.00% Impervious Runoff Depth>5.05" Tc=0.0 min CN=0/98 Runoff=0.36 cfs 0.106 af

Pond 2P: Drywell

Peak Elev=16.98' Storage=3,170 cf Inflow=0.36 cfs 0.106 af Outflow=0.02 cfs 0.074 af

Total Runoff Area = 0.251 ac Runoff Volume = 0.106 af Average Runoff Depth = 5.05" 0.00% Pervious = 0.000 ac 100.00% Impervious = 0.251 ac

■ Runoff

Summary for Subcatchment 2S: Roof

Runoff

= (

0.36 cfs @

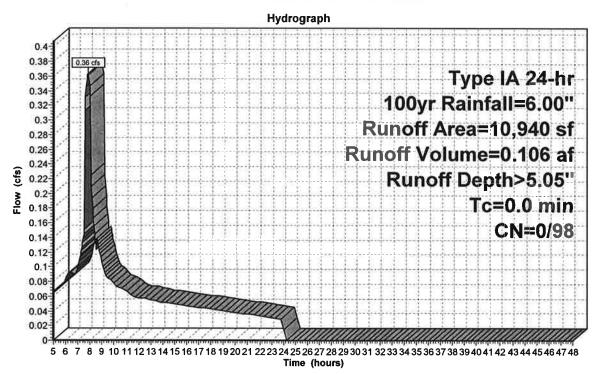
7.80 hrs, Volume=

0.106 af, Depth> 5.05"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type IA 24-hr 100yr Rainfall=6.00"

	Area (sf)	CN	Description	
*	10,940	98	Roof	
	10,940	98	100.00% Impervious Area	

Subcatchment 2S: Roof



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Summary for Pond 2P: Drywell

Inflow Area = 0.251 ac,100.00% Impervious, Inflow Depth > 5.05" for 100yr event

Inflow = 0.36 cfs @ 7.80 hrs, Volume= 0.106 af

Outflow = 0.02 cfs @ 5.20 hrs, Volume= 0.074 af, Atten= 94%, Lag= 0.0 min

Discarded = 0.02 cfs @ 5.20 hrs, Volume= 0.074 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 16.98' @ 24.00 hrs Surf.Area= 452 sf Storage= 3,170 cf

Plug-Flow detention time= 1,057.8 min calculated for 0.074 af (70% of inflow) Center-of-Mass det. time= 880.3 min (1,592.6 - 712.3)

Volume	Invert	Avail.Storage	Storage Description
#1	0.00'	3,482 cf	24.00'D x 20.00'H Vertical Cone/Cylinder
			9,048 cf Overall - 342 cf Embedded = 8,706 cf x 40.0% Voids
#2	0.00'	251 cf	4.00'D x 20.00'H Vertical Cone/Cylinder Inside #1
			342 cf Overall - 4.0" Wall Thickness = 251 cf

3,734 cf Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	0.00'	2.000 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.02 cfs @ 5.20 hrs HW=0.24' (Free Discharge)
1=Exfiltration (Exfiltration Controls 0.02 cfs)

Pond 2P: Drywell

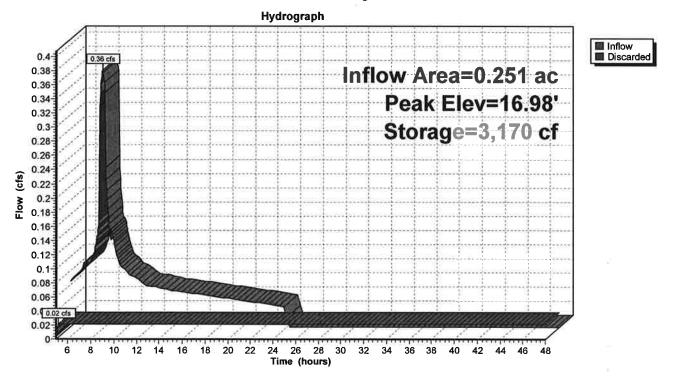
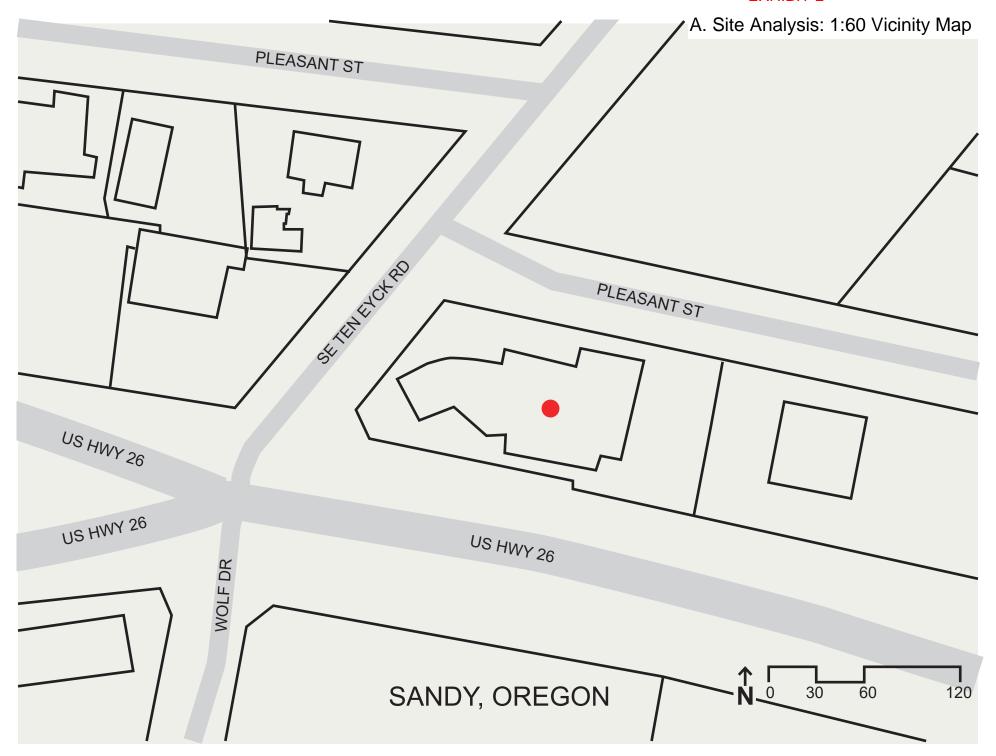


EXHIBIT L





500 ft radius

CURRAN-MCLEOD, INC. CONSULTING ENGINEERS 6655 SW HAMPTON, SUITE 210 PORTLAND, OR 97223

May 29, 2020

Ms. Emily Meharg City of Sandy 39250 Pioneer Blvd. Sandy, OR 97055

RE: CITY OF SANDY

SANDY HEALTH CLINIC (File # 20-006 DR//VAR/DEV/ADJ)
PRELIMINARY REVIEW

Dear Emily:

We have reviewed the preliminary submittal for the above noted development and have the following comments/ recommendations:

- 1. All earthwork activities shall follow the requirements of the most current edition of the Oregon Structural Specialty Code. Site grading shall not in any way impede or impound or inundate the surface drainage flow from the adjoining properties without a proper collection system. The earthwork activities shall be observed and documented under the supervision of the geotechnical Engineer.
- 2. The proposed driveway accesses on Pleasant Street shall be Concrete Commercial Driveway Approach constructed in conformance with the applicable City of Sandy driveway detail and meeting PROWAG requirements.
- 3. Where the existing driveway is removed on Pleasant Street, it shall be replaced with sidewalks and an ADA ramp shall be constructed at the intersection with Ten Eyck Road to current PROPWAG requirements.
- 4. Ten Eyck Road is a County road, we recommend the county requires sidewalks to be constructed along the entire site frontage to match the existing sidewalks on Hwy 26.
- 5. A demolition permit shall be required from the City prior to demoing the existing building.

- 6. We have reviewed the preliminary stormwater calculations that was provided with this submittal. The calculations were found not meeting the water quality/quantity criteria as stated in the City of Sandy Development Code (SDC) 13.18 Standards and the 2016 City of Portland Stormwater Management Manual (SWMM) Standards, that were adopted by reference into the Sandy Development Code. The water quality shall be designed based on 0.19 in/hr rate for 5 minutes time of concentration. While the water quality shall be designed for 2, 5, 10 and 25 year storm events and not 25 and 100 year storm events only. A detailed final report stamped by a licensed professional shall be resubmitted for review with the final construction plans.
- 7. The proposed 6" sanitary sewer service should be adequate to serve this building, unless the City public works department determines a sanitary sewer service exists and a new one is not needed.
- 8. The final construction plans shall be submitted to Sandy Fire Department for review and approval to ensure that the proposed vault has adequate fire protection and also acceptable access is provided to the building.
- 9. The final construction plans shall verify the domestic 2" meter size is adequate based on the meter flow and the building fixture counts found in the 2017 Oregon Plumbing Specialty Code, if larger than 2" meter size is needed shall be verified in the AWWA series 700 and the Oregon Plumbing Specialty Code.

We have no concerns about the proceedings with this project subject to the above stated comments.

Sincerely,

CURRAN-McLEOD, INC.

Hassan A. Ibrahim, P.E.

cc: Mr. Mike Walker, City of Sandy





Emily Meharg <emeharg@ci.sandy.or.us>

Clackamas County Health Clinic (File No. 20-006 DR/VAR/DEV/ADJ)

Gary Boyles <fmboyles.sandyfire@gmail.com>
To: emeharg@ci.sandy.or.us
Cc: Don Patty <d.patty3710@gmail.com>

Wed, Jun 3, 2020 at 12:32 PM

Hi Emily,

The only comment I have regarding this application is that the new fire department connection (FDC) be relocated to the Mt. Hood Highway side of the proposed fire vault and to be as close as possible to the existing fire hydrant located in that area as possible.

Thank you,

Gary Boyles
Fire Marshal
Sandy Fire District No. 72
PO Box 518
17460 SE Bruns Ave.
Sandy, Oregon 97055

Business line: 503-668-8093 Cell number: 503-891-7042

CONFIDENTIALITY NOTICE- This email, and any attachments may contain information that is privileged, confidential, or otherwise exempt from disclosure under applicable law. It is intended only for the use of the person(s) names above. If you are not the intended recipient, you are hereby notified that any review, dissemination, distribution, or duplication of this communication is strictly prohibited. If you are not the intended recipient, please contact me by reply email and delete the message and any attachments from your system.

REPLINGER & ASSOCIATES LLC

TRANSPORTATION ENGINEERING

June 8, 2020

Ms. Emily Meharg City of Sandy 39250 Pioneer Blvd. Sandy, OR 97055

SUBJECT: REVIEW OF TRANSPORTATION IMPACT ANALYSIS – SANDY HEALTH

CLINIC

Dear Emily:

In response to your request, I have reviewed materials submitted in support of the Sandy Health Clinic in the northeast quadrant of Highway 26 and Ten Eyck Road in the east part of Sandy. The Transportation Impact Analysis (TIA), dated March 12, 2020, was prepared under the direction of John Manix, PE of PBS.

The site, currently occupied by a warehouse, is proposed to have a 9600-square foot health clinic. Access will be on Pleasant Street.

Overall

I find the TIA addresses the city's requirements and provides an adequate basis to evaluate impacts of the proposed development.

Comments

- 1. Study Area. The study addresses the appropriate intersections. It includes analyses of:
 - Highway 26 at SE Ten Eyck Road;
 - Ten Eyck Road at Pleasant Street.
- 2. Traffic Counts. The AM and PM peak hour traffic counts were conducted during February 2020. The engineer adjusted the traffic counts to account for seasonal variations. The engineer adjusted the February counts by 28 percent to estimate the 30th highest hour traffic volumes. The methodology appears consistent with the procedures defined by the Oregon Department of Transportation (ODOT). The adjusted counts appear reasonable.

- 3. Trip Generation. The TIA uses trip generation for a medical clinic and for a warehouse (land use code 630 and 150, respectively) from the Institute of Transportation Engineers' (ITE) Trip Generation Manual. The warehouse calculation was used to calculate traffic from the existing use. After accounting for the warehouse, the engineer calculates that the medical clinic would produce 34 net new AM peak hour trips; 30 net new PM peak hour trips; and 335 net new daily trips. The calculation of trips generated by the development appears reasonable.
- 4. Trip Distribution. The TIA provided information about trip distribution from the site. Among other resources, the engineer consulted with county medical staff about clients. The engineer assumed 90 percent of the traffic would travel to and from the west on US 26 and 10 percent would travel to and from the east on US 26. The trip distribution seems reasonable.
- 5. Traffic Growth. The TIA uses a 2.0 percent annual increase for Highway 26 based on projected volumes from the Transportation System Plan. No adjustments were made for in process developments. The future year background traffic volumes appear reasonable.
- 6. Analysis. Traffic volumes were calculated for the intersections cited in #1, above. Intersection level-of-service (LOS) and the volume-to-capacity (v/c) ratio were provided. The intersection of US 26 with SE Ten Eyck Road is signalized; the intersection of Ten Eyck Road and Pleasant Street is stop-controlled. The analyses were conducted for existing 2020 conditions, 2022 background conditions, 2022 with the development, 2029 background conditions, and 2029 with the development.

The engineer calculated that the intersection of Highway 26 and Ten Eyck Road would operate at LOS B or better and a v/c ratio of 0.66 or better during the AM peak hour. For the PM peak hour, he calculated the intersection would operate at LOS C or better and a v/c ratio of 0.84 or better under all conditions. This meets ODOT's performance standard.

The engineer did not report the LOS or v/c ratio for the intersection of Ten Eyck Road with Pleasant Street. Both the east leg and west leg approaches of Pleasant Street with Ten Eyck Road were analyzed in a simulation that showed the anticipated queues and blockage time. Due to the low traffic volumes and short predicted queues on Pleasant Street, it is apparent that operations of the intersection will be good even with the proposed development. My own calculations using Synchro indicated the intersection will operate at LOS A, meeting city operational standards.

The engineer provides a thorough discussion of queuing issues using traffic volumes for 2029. During the PM peak hour, eastbound left-turn and eastbound right-turn queues are calculated to exceed available storage both with and without the development. In addition, southbound queues on Ten Eyck Road are expected to block nearby driveways and intersections both with and without the development. The engineer notes that the addition of a southbound left-turn lane may shorten queues. He recommended tracking volumes and queues over time to assess queuing storage needs.

The engineer also evaluated the effect of a westbound right-turn lane on Highway 26 at the intersection with Ten Eyck Road. He determined the performance of the intersection is not significantly different with a turn lane and meets v/c standards without it. He recommends against a westbound right-turn lane. He recommends retaining the existing configuration that features a slip lane.

7. Crash Information. The TIA provides information on crashes for the most recent available five-year period covering 2014 through 2018.

At the intersection of US 26 and SE Ten Eyck Road, there were eleven reported crashes. Rear-end crashes were the most common type. This is typical of signalized intersections in an urban area. The intersection has a relatively low crash rate of 0.26 crashes per million entering vehicles. The engineer concluded that no further investigation or mitigation is required. I concur.

- 8. Site Plan and Access. The site plan provides for a single access on Pleasant Street near the parcel's east boundary. The TIA indicates safety will be improved by the elimination of two existing driveways serving the site, including one on Ten Eyck Road. The site access is an improvement relative to existing conditions.
- Sight Distance. The engineer analyzed sight distance at the proposed access and concludes stopping sight distance is met. He recommends maintaining 200 feet of sight distance at the access.
- 10. Conclusions and Recommendations. The engineer concludes that the intersections will meet ODOT and city operational standards for the study area intersections either with or without the development. He also indicates that queuing is not significantly different with or without the development, but that queue storage will be exceeded by 2029 for some movements.

He found crash rates at the intersection of Highway 26 and Ten Eyck Road to be low and did not recommend further investigation. He concluded that a right-turn lane for Ms. Emily Meharg June 8, 2020 Page 4

Highway 26 westbound was not warranted and recommended retaining the existing slip lane.

He concluded the reduction in accesses to the site, including the elimination of a driveway to Ten Eyck Road, would be beneficial and improve safety.

He recommended monitoring traffic volumes and queuing at the Highway 26 and Ten Eyck Road intersection and reevaluating the intersection in connection with a future Transportation System Plan update.

I concur with the engineer's conclusions.

Conclusion and Recommendations

Based on the information provided by the applicant, I find the TIA meets city requirements. The engineer used appropriate methods and documents his procedures and conclusions.

The intersections of Highway 26 and Ten Eyck Road and Ten Eyck Road and Pleasant Street are calculated to meet ODOT and city performance standards. I do not find a need for mitigation measures to address traffic impacts of the development or to address safety issues.

To the extent that the developer may be required to implement projects or participate in projects involving facilities under the jurisdiction of ODOT, conditions of approval should be included requiring that the development comply with the requirements standards and procedures specified by ODOT. I recommend that that ODOT requirements and standards associated with frontage improvements where the development abuts Highway 26 be made conditions of approval for the development.

If you have any questions or need any further information concerning this review, please contact me at replinger-associates@comcast.net.

Sincerely,

John Replinger, PE

John Keplinger

Principal

SandyMedicalTIS060820

EXHIBIT Q



Department of Transportation

Region 1 Headquarters 123 NW Flanders Street Portland, Oregon 97209 (503) 731.8200 FAX (503) 731.8259

June 17, 2020 ODOT #10415

Updated ODOT Response

Project Name: Sandy Health Clinic	Applicant: Steve Kelly
Jurisdiction: City of Sandy	Jurisdiction Case #: 20-006 DR/VAR/DEV/ADJ
Site Address: 39831 US Hwy 26, Sandy, OR 97055	Legal Description: 02S 04E 13ad Tax Lot(s): 01000
State Highway: US 26	

The site of this proposed land use action is adjacent to US 26. ODOT has permitting authority for this facility and an interest in ensuring that this proposed land use is compatible with its safe and efficient operation. ODOT has reviewed the Traffic Impact Analysis for the proposed medical clinic development and determined that a westbound right turn lane at the US 26/SE Ten Eyck Rd intersection is not warranted.

ODOT has determined there will be no significant impacts to state highway facilities and no additional state review is required.

Please send a copy of the Notice of Decision including conditions of approval to:

ODOT Region 1 Planning Development Review 123 NW Flanders St Portland, OR 97209

ODOT_R1_DevRev@odot.state.or.us

Development Review Planner: Marah Danielson	503.731.8258,
	marah.b.danielson@odot.state.or.us

MEMORANDUM

TO: EMILY MEHARG, ASSOCIATE PLANNER

FROM: MIKE WALKER, PUBLIC WORKS DIRECTOR RE: FILE 20-006 CLACKAMAS COUNTY HEALTH CLINIC

DATE: JUNE 18, 2020

The following are Public Works' comments on the above-referenced application:

Transportation

The applicant shall improve the US 26 frontage of the site in compliance with ODOT requirements including modifying the existing slip/right-turn lane to reduce the curb radius at the corner to accommodate east-west and north-south ADA compliant ramps if required by ODOT. This may require right-of-way dedication at the NE corner of US 26 and Ten Eyck Rd.

The existing driveway approach onto Ten Eyck Rd. from the site does not meet the minimum spacing standards in 17.98.80(A) of the Sandy Municipal Code (SMC). The applicant shall abandon the existing driveway approach and improve the Ten Eyck Road frontage of the site including but not limited to: curbs, sidewalks, storm drainage, streetlighting, street trees per the requirements in sections 15.20 and 17.84.30 of the SMC. This section of Ten Eyck Rd. is under the jurisdiction of Clackamas County. The applicant shall coordinate with Clackamas County DTD to determine the required section for Ten Eyck. This may include relocating the existing fire hydrant at the intersection of Ten Eyck Rd. and Pleasant Ave. to install ADA compliant access ramps. Ten Eyck Road is a minor arterial street. Both Clackamas County and City of Sandy require minimum 6 ft. wide sidewalks on arterial streets. The County standard and the proposed ultimate section for Ten Eyck Road will only permit a curb tight sidewalk in the available right-of-way.

The City recently designed a pedestrian improvement project on Ten Eyck Rd. at the subject site. The Clackamas County DTD plan review fee has been paid and the plans have been approved by DTD. The applicant will be responsible for these improvements and is welcome to use the approved planset for this work.

The applicant shall dedicate sufficient right-of-way at the SW corner of the site to accommodate the required street section and pedestrian improvements including ADA-compliant ramp(s) at the intersection with US 26. The exact dedication area shall be determined during construction plan review. The applicant shall be responsible for providing legal descriptions and sketch maps of the dedication area, dedicating the right-of-way using the City's standard documents, and pay all recording costs.

The applicant shall remove the existing west driveway approach onto Pleasant St. The existing driveway approach doesn't to meet the minimum spacing standard in 17.98.80(A) SMC or the maneuvering standard in 17.98.70(B). The applicant shall

improve the Pleasant St. frontage of the site including but not limited to: curbs, sidewalks, storm drainage, streetlighting, street trees per the requirements in sections 15.20 and 17.84.30 of the SMC. The sidewalk shall be curb-tight, minimum 8 ft. in width with street trees specified by the City in tree wells on XX foot centers. The sidewalk shall be five feet wide separated from the curb with a five foot wide planter strip including street trees specified by the City on XX foot centers.

Street tree and landscaping placement shall conform to the sight distance recommendations in the traffic impact analysis submitted by the Applicant.

Utilities

The site is served by the existing 16" water main in US 26 and the existing 8" sanitary sewer main in Pleasant St. The applicant is proposing a drywell for stormwater disposal. Typically, the soils in Sandy do not permit treatment and discharge of stormwater in this manner. Stormwater management shall conform to the requirements in the City of Portland Stormwater Management Manual and the requirements in section 13.18 and 13.20 SMC.

Utility and right-of-way improvement plans are submitted with the land use application solely for conformance with the submittal requirements in Section 17.100.60(D). Land use approval does note connote approval of public improvement plans.

Please let me know if you have any questions or need more information.





Emily Meharg <emeharg@ci.sandy.or.us>

Incompleteness Letter: 20-006 DR/VAR/DEV/ADJ

Scott Soukup <scotts@ankrommoisan.com>

Wed, Apr 1, 2020 at 9:21 AM

To: Emily Meharg <emeharg@ci.sandy.or.us>

Cc: Marisol Martinez <mmartinez@ci.sandy.or.us>, "Kelly O'Neill Jr." <koneill@ci.sandy.or.us>, "Kelly, Steve" <SteveKel@clackamas.us>, Lori Kellow <lorik@ankrommoisan.com>

Hi Emily,

Here is the credit card authorization form.

For the vertical Nichiha siding, Section 17.90.110(B.3.d) allows composite-wood (concrete fiberboard, panels or shingles). The vertical ribbed Nichiha product is a panelized fiber cement product with 1 5/8" vertical slats and 3/8" reveals between each slat which add depth and rustic texture to the facade. The product is available in custom colors that can match any selected Miller or Sherwin Williams paint. The ribbed fiber cement is not the same as board-andbatten siding or T1-11 sheet siding.

The product can be installed either vertically or horizontally. In terms of design, the vertical siding is a darker earth tone and is the bulk of the siding. The vertical orientation was selected to distinguish it from the horizontal redwood Nichiha material pops of warm color at the bumpouts and recesses in the facade. Both siding products are Nichiha so all the siding can come from a single source manufacturer. This will make the construction process smoother and simplify the detailing. The vertical siding has been selected as the main siding, because the vertical orientation is better for cleaning and maintenance over time.

[Quoted text hidden]

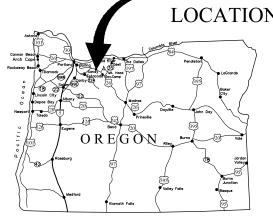


Credit Card Authorization Form signed 4.1.2020.pdf 337K

SE TEN EYCK ROAD & PLEASANT STREET CURB & SIDEWALK IMPROVEMENTS



CLACKAMAS COUNTY, OREGON **DECEMBER 2018**



CITY OF SANDY

HONORABLE BILL KING **MAYOR COUNCILOR** JEREMY PIETZOLD COUNCILOR JOHN HAMBLIN **COUNCILOR** SCOTT HORSFALL JAN LEE COUNCILOR **CARL EXNER COUNCILOR COUNCILOR** JEAN CUBIC CITY MANAGER KIM YAMASHITA DIRECTOR OF PUBLIC WORKS MIKE WALKER

SHEET INDEX

C1 COVER SHEET AND INDEX

C2 SE TEN EYCK ROAD & PLEASANT STREET **CURB & SIDEWALK IMPROVEMENTS**

C3 CLACKAMAS COUNTY CONSTRUCTION DETAILS

C4 CITY OF SANDY CONSTRUCTION DETAILS

PROJECT US HWY 26 MEINIG PARK

CALL BEFORE YOU DIG

OREGON LAW REOUIRES YOU TO FOLLOW RULES ADOPTED BY THE OREGON UTILITY NOTIFICATION CENTER. THOSE RULES ARE SET FORTH IN OAR 952-001-0010 THROUGH OAR (NOTE: THE TELEPHONE NUMBER FOR THE OREGON UTILITY NOTIFICATION CENTER IS (503) 232-1987) OR 811 OR 1-800-332-2344

> ALL UTILITY CROSSINGS ARE APPROXIMATE, CONTRACTOR TO POTHOLE AND FIELD DEPTH VERIFY PRIOR TO CONSTRUCTION AND CONSULT WITH THE ENGINEER REGARDING ANY CONFLICTS

CONTRACTOR TO PROTECT EXISTING POWER, TELEPHONE/TELECOMMUNICATION LINES & COORDINATE RELOCATION OF ANY LINES THAT ARE IN CONFLICT WITH THE CONSTRUCTION WITH APPROPRIATE AGENCY

LEGEND



LOCATION MAP

/ \	REV:#	
BAR IS ONE INCH ON	REV:#	
ORIGINAL DRAWING.	REV:#	
ONIONAL BRANCO	REV:#	
ADJUST SCALE	REV:#	
AS SHOWN	REV:#	
ACCORDINGLY.	REV:#	
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REVISIONS



CURRAN-McLEOD, INC. CONSULTING ENGINEERS

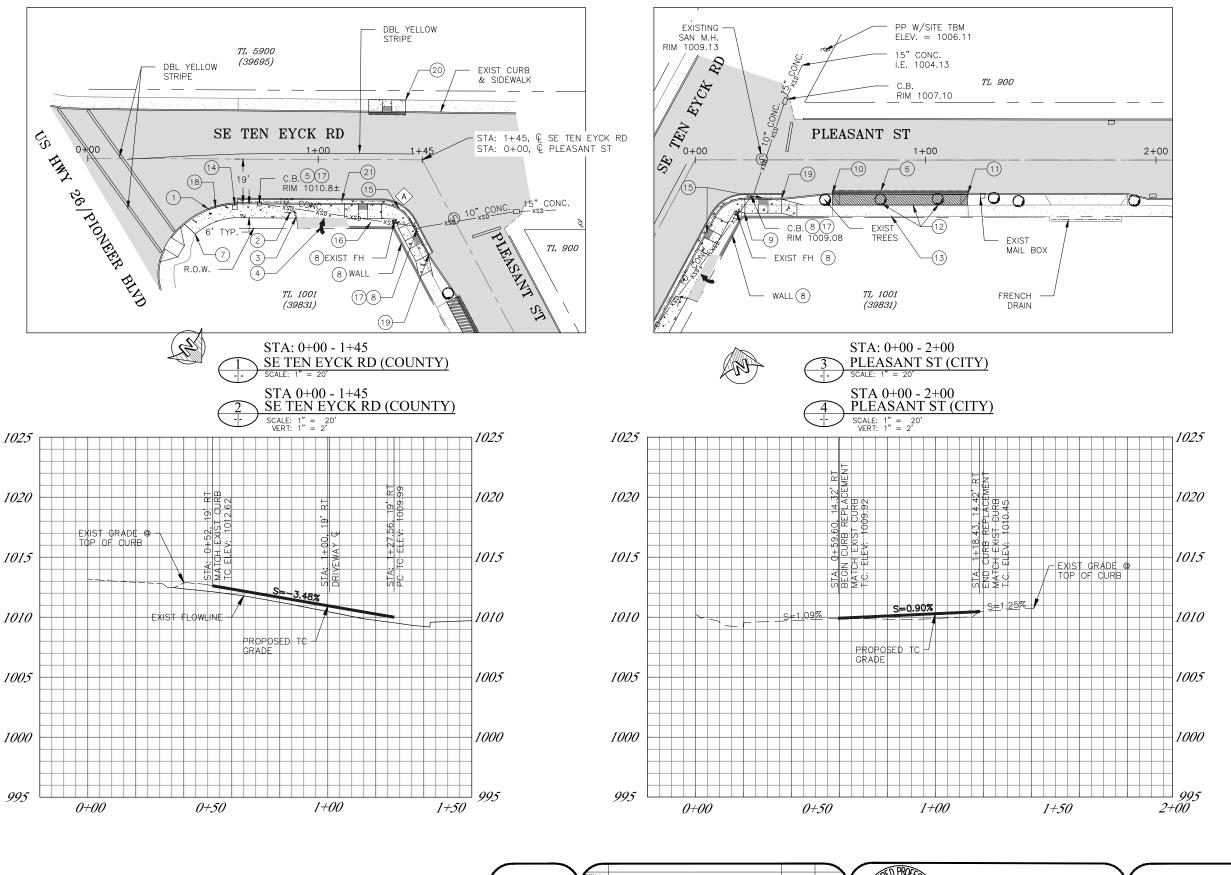
> PORTLAND OREGON 97223 PHONE (503) 684-3478

CITY OF SANDY

COVER SHEET AND INDEX

SE TEN EYCK ROAD / PLEASANT STREET CLACKAMAS COUNTY, OREGON

1723 JVB OF 1723-1



BAR IS ONE INCH OI ORIGINAL DRAWING.

AS SHOWN

ACCORDINGLY.

REVISIONS

CONSTRUCTION NOTES:

- 1 STA: 0+52, 19' RT BEGIN NEW CURB & GUTTER, SAWCUT & MATCH EXIST. SEE DETAIL S150 SHEET C3.
- (2) REMOVE EXIST TRAFFIC SIGN AND SALVAGE TO CITY.
- (3) REMOVE 3.25'± OF EXIST CURB, TAPER TO MATCH NEW SIDEWALK.
- (4) REMOVE EXIST. ARROW.
- (5) REMOVE EXIST CB GRATE AND INSTALL CURB INLET TOP, SEE DETAIL \$350 SHEET C3.
- 6 SAWCUT 1'± INTO EXIST PAVEMENT & MATCH EXIST AC
- (7) MATCH EXIST CURB & SIDEWALK.
- (8) PROTECT EXIST. FIRE HYDRANT, CATCH BASIN AND RETAINING WALL, MAINTAIN 48" MIN. CLEAR PATH.
- (9) REMOVE 24 LF \pm OF SIDEWALK, MEANDER AROUND EXIST FIRE HYDRANT.
- (1) STA: 0+59.60, 14.32' RT BEGIN NEW TYPE 'C' CURB, SAWCUT & MATCH EXIST. SEE DETAIL 5 SHEET C4.
- (11) STA: 1+18.43, 14.42' RT END NEW TYPE 'C' CURB SAWCUT, MATCH EXIST. SEE DETAIL 5 SHEET C4.
- (12) REMOVE EXIST 59'± CURB & 274 SF± OF DRIVEWAY, MAINTAIN EXIST SIDEWALK, FILL PLANTER STRIP W/12" CLEAN TOPSOIL, TWO STREET TREES (BY CITY).
- (13) PROTECT EXIST SIDEWALK.
- (14) PROTECT EXIST WATER METER, ADJUST BOX TO NEW SIDEWALK GRADE.
- (15) CONSTRUCT DUAL ADA RAMP, SEE DETAIL 1 ON SHEET C4.
- (16) RESTORE DAMAGED LANDSCAPE TO ORIGINAL CONDITION OR BETTER.
- (17) INSTALL INLET PROTECTION.
- (18) SAWCUT & REMOVE 13 LF± OF EXIST CURB.
- (9) STA: 0+37.57, 16.56' RT END NEW CURB & GUTTER & MATCH EXIST. SEE DETAIL S150 SHEET C3.
- (20) INSTALL MIDBLOCK CROSSING. SEE DETAIL 2 SHEET C4.
- (2) SAWCUT 2.5'± INTO EXIST PAVEMENT & MATCH EXIST AC DEPTH.

0.	RADIUS	Δ	LENGTH	CL
$\langle A \rangle$	15.00'	61°37'11"	16.13'	15.37'
0.	STATION	OFFSET	T.C. EL	
A	1+27.56 PC SE TEN EYCK RD	19.00' RT	1009.99	
	1⁄2∆		1009.79	
	1+40.74 PT SE TEN EYCK RD	26.86' RT	1009.59	

HALDON OREGON

EXPIRES: 6/30/2019

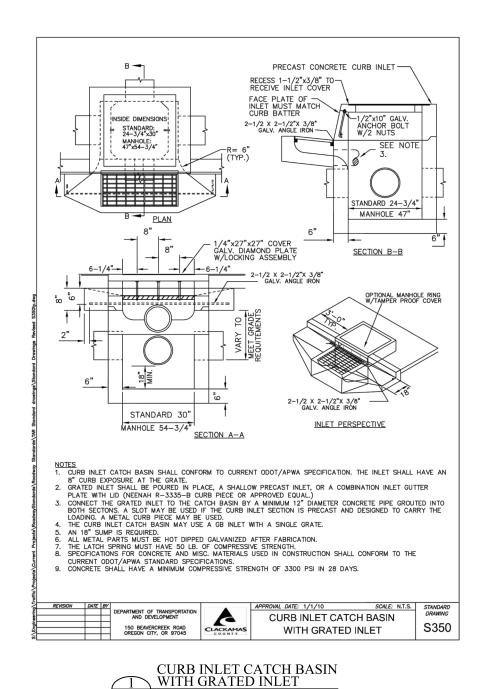
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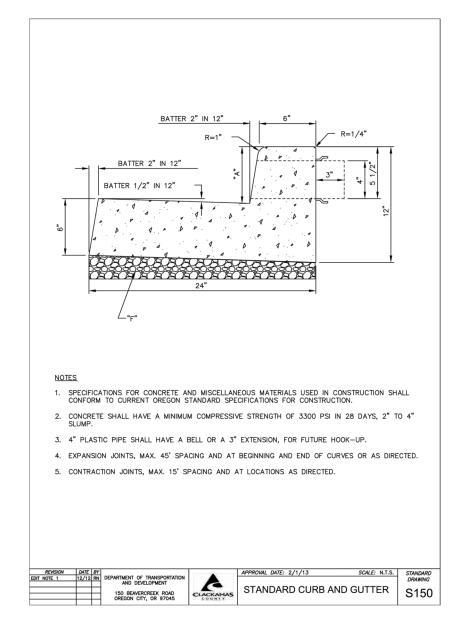
6655 S.W. HAMPTON ST., SUITE 210 PORTLAND, OREGON 97223 PHONE (503) 684-3478 CITY OF SANDY

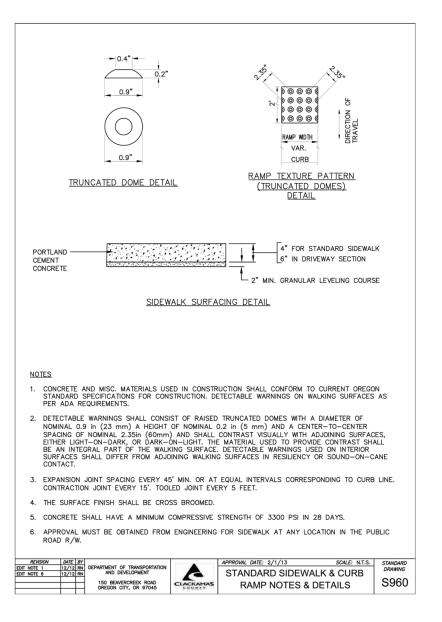
SE TEN EYCK ROAD & PLEASANT ST CURB & SIDEWALK IMPROVEMENTS

> SE TEN EYCK ROAD / PLEASANT STREET CLACKAMAS COUNTY, OREGON

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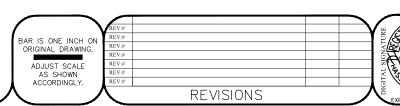














CURRAN-McLEOD, INC. CONSULTING ENGINEERS

> 6655 S.W. HAMPTON ST., SUITE 210 PORTLAND, OREGON 97223 PHONE (503) 684-3478

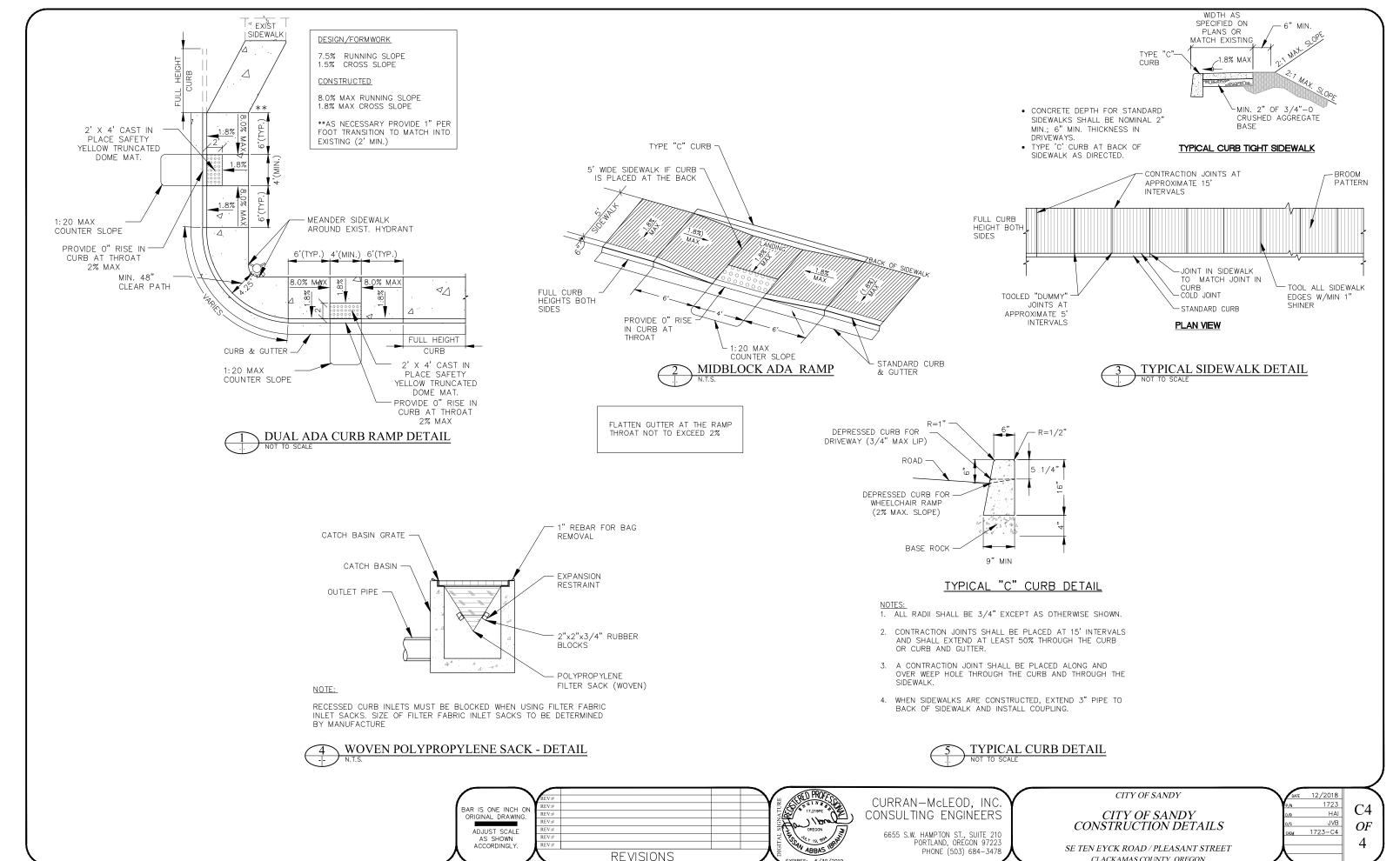
CITY OF SANDY

CLACKAMAS COUNTY CONSTRUCTION DETAILS

SE TEN EYCK ROAD / PLEASANT STREET CLACKAMAS COUNTY, OREGON

12/2018 1723 HAI JVB 1723-1

OF



CLACKAMAS COUNTY, OREGON