## EXHIBIT K

# Johnson RV Traffic Impact Study 

SANDY, OREGON



DIGITALLY SIGNED


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## ExECUTIVE Summary

1. A property located on the east side of SE $362^{\text {nd }}$ Avenue immediately south of Industrial Way in Sandy, Oregon is proposed for development with an RV refurbishing business that will be operated by Johnson RV. The site will take access via an existing driveway on SE $362^{\text {nd }}$ Avenue and a proposed new site access driveway on Industrial Way at the northeast corner of the site.
2. Upon completion of the proposed improvements within the subject property, the site is projected to accommodate 18 site trips during the morning peak hour, 22 trips during the evening peak hour, and 108 daily site trips.
3. Based on the operational analysis, the study intersections are currently operating acceptably per City of Sandy and ODOT standards. Under year 2023 traffic conditions the intersections are projected to continue to operate acceptably either with or without the addition of site trips from the proposed use. No operational mitigations are necessary or recommended.
4. Based on the queueing analysis, the projected northbound queues on SE $362^{\text {nd }}$ Avenue are projected to extend beyond the proposed driveway location during a portion of the peak hours. However, average queue lengths even during the peak hours will not obstruct the driveway, and the proposed driveway re-alignment will provide 50 feet of added access spacing as compared to existing conditions, and the driveway will be aligned directly opposite an existing driveway on the west side of SE $362^{\text {nd }}$ Avenue.
5. Based on the crash data, the study intersections are currently operating acceptably with respect to safety. No specific safety improvements are recommended in conjunction with the proposed site use.
6. Based on the warrant analysis, no new turn lanes or traffic signals are recommended in conjunction with the proposed site use.
7. The proposed re-aligned site access on SE $362^{\text {nd }}$ Avenue is projected to have adequate sight distance for safe and efficient operation. The proposed new site access on Industrial Way is projected to have adequate sight distance to the west upon clearing of vegetation within the site frontage allowing a clear line of sight to SE $362^{\text {nd }}$ Avenue. Sight distance to the east is restricted by an existing concrete block which supports a fire department standpipe connection that serves the property immediately east of the Johnson RV site. Although sight lines to the east are restricted, the available intersection sight distance is sufficient for safe operation of the access, and operational impacts associated with the limited sight distance are negligible. Accordingly, the proposed site access on Industrial Way can also operate safely and efficiently.

## Project Description \& Location

## INTRODUCTION

A property located on the east side of SE $362^{\text {nd }}$ Avenue immediately south of Industrial Way is currently developed with two buildings, a 20,000 square foot main building and a two-story 3,850 square foot office building. The site takes access via a driveway on SE $362^{\text {nd }}$ Avenue centered 100 feet south of the west leg of Industrial Way.

Under the proposed development plan, a 7,375 square foot shed roof will be added to cover the bus wash facility within the site. Additionally, a new access driveway intersecting Industrial Way near the northeast corner of the site is proposed.

This report addresses the impacts of the proposed development on the surrounding street system. An operational and safety analysis was conducted for the intersections of:

- Highway 26 at SE 362 ${ }^{\text {nd }}$ Avenue;
- SE $362^{\text {nd }}$ Avenue at Industrial Way (east);
- SE $362^{\text {nd }}$ Avenue at Industrial Way (west);
- SE $362^{\text {nd }}$ Avenue at Johnson RV Site Access; and
- Industrial Way at the proposed new site access.

The purpose of this analysis is to determine whether the surrounding transportation system is capable of safely and efficiently supporting the proposed use and to identify any necessary improvements and mitigations.

## Site Location and Study area Description

The project site has an area of approximately 3.4 acres, and was previously used for trailer and equipment sales, rental, and maintenance. Johnson RV purchased the site to serve as a maintenance facility which supplements their existing sales facility located at 41777 US Highway 26 at the east end of the City of Sandy.

The property is surrounded primarily by commercial and industrial uses, including the Fred Meyer store located immediately to the northwest. There are also residential homes south of the site on the far side of a school bus barn.

US Highway 26 (Mt. Hood Highway) is classified by the Oregon Department of Transportation as a Statewide Highway and a Freight Route. It has two through lanes in each direction and added turn lanes at intersections. It has a posted speed limit of 45 in the vicinity of SE $362^{\text {nd }}$ Avenue. Bike lanes are in place along both sides of the highway in the site vicinity, and sidewalks are in place along the south side of the highway in the vicinity of SE $362^{\text {nd }}$ Avenue.

SE $362^{\text {nd }}$ Avenue generally has one through travel lane for motor vehicles in each direction plus bike lanes and sidewalks on both sides of the roadway. North of Industrial Way it has a center two-way
left-turn lane. It has a posted speed limit of 35 mph and is classified by the City of Sandy as a Minor Arterial.

Industrial Way accommodates one travel lane in each direction with no centerline striping. It has a posted speed limit of 25 mph and has sufficient width for on-street parking (although parking is restricted in the immediate vicinity of SE $362^{\text {nd }}$ Avenue). It is classified by the City of Sandy as a Local Street. Existing sidewalks are in place on both sides of the roadway west of SE $362^{\text {nd }}$ Avenue. Partial sidewalks are in place along the north side of Industrial Way immediately east of SE $362^{\text {nd }}$ Avenue, while none are currently provided along the south side of the roadway east of SE $362^{\text {nd }}$ Avenue.

## Existing Conditions

The intersection of US Highway 26 at SE $362^{\text {nd }}$ Avenue is a T-intersection controlled by a traffic signal. The northbound approach has two left-turn lanes, a right-turn lane, and a bike lane to the right of the motor vehicle travel lanes. The westbound approach has a left-turn lane operating with protected signal phasing, two through lanes, and a bike lane to the right of the motor vehicle travel lanes. The eastbound approach has two through lanes, a bike lane, and a right-turn lane on the right side of the bike lane.

The intersection of SE $362^{\text {nd }}$ Avenue at Industrial Way (east) is a T-intersection controlled by a stop sign on the westbound Industrial Way approach. Through traffic traveling along SE $362^{\text {nd }}$ Avenue does not stop. The southbound approach has a left-turn lane and a through lane. The northbound and westbound approaches each have a single shared lane for all turning movements.

The intersection of SE $362^{\text {nd }}$ Avenue at Industrial Way (west) is a T-intersection operating under allway stop control. Each approach has a single, shared lane for all turning movements.

A vicinity map displaying the project site, vicinity streets, and the study intersections including lane configurations is provided in Figure 1 on page 6.


## Traffic Count Data

Traffic counts were conducted at the study area intersections on Thursday August 11, 2022 from 7:00 to 9:00 AM and from 4:00 to 6:00 PM. Data was used from the highest-volume hour for each study intersection during each analysis period.

Since the count data was not collected during the peak month of the year, the observed traffic volumes on Highway 26 were adjusted to account for seasonal traffic variations. In accordance with the Oregon Department of Transportation's Analysis Procedures Manual, this allows us to analyze operations based on traffic patterns that occur during the $30^{\text {th }}$-highest hour of the year.

US Highway 26 serves local and commuter traffic as well as trips to and from Mt. Hood and beyond. These trip types would be expected to exhibit vastly different seasonal variations in travel demands over the course of the year, since local and commuter traffic volumes are relatively stable regardless of season, while travel volumes to and from Mt. Hood vary significantly based on the season.

In order to determine the portion of traffic attributable to each of the two primary travel types, data from ODOT's 2017-2021 ATR station trend data was utilized. Specifically, the data used was collected at ODOT's Automatic Count Data station 03-006, located 0.30 miles east of Camp Creek Road in Rhododendron, Oregon. This site is located on Highway 26 approximately 24 miles east of SE $362^{\text {nd }}$ Avenue. Although the distance to the ATR station means the data cannot be used directly, the ATR data provides useful information regarding the variation in traffic volumes traveling to Mt. Hood and beyond during the time of the count data collection as well as during the peak season of the year. Accordingly, this data allows determination of the portion of highway traffic that falls into each of the two seasonal variation categories ("commuter" and "recreational summer/winter"), as well as providing information regarding the most appropriate seasonal adjustment factor for the recreational summer/winter traffic.

Based on the five years of ATR data and excluding the highest and lowest variations (i.e., averaging the three other data points), 13,374 vehicles per day (approximately 1,337 per hour during the peak hour) travel along Highway 26 to and from Mt. Hood at the Rhododendron permanent count station location during the month of August. This volume represents 50.5 percent of the through traffic volumes measured on Highway 26 east of Oregon Highway 211, since the August turning movement counts showed 2,643 vehicles on Highway 26 east of SE $362^{\text {nd }}$ Avenue during the evening peak hour. Accordingly, no more than 50.5 percent of the trips traveling along Highway 26 at that location can be traveling to and from destinations beyond the Rhododendron count station. Since the remaining 49.5 percent of through traffic volumes on Highway 26 at Highway 211 never reach Mt. Hood, it was assumed that these traffic volumes represent more typical commuter and local trips.

The ODOT data also showed that 13,969 vehicles were measured per day (approximately 1,397 per hour during the peak hour) during the peak-season month of July at the ATR station near Rhododendron. This indicates that the seasonal recreational traffic volumes along the Highway 26 corridor increased by 595 vehicles per day ( 13,969 vehicles per day in July - 13,374 vehicles per day in August). This equates to roughly 60 additional vehicles per hour during the peak hour of the peak recreational season. Accounting for directionality of trips, this equates to approximately 33 westbound vehicles and 27 eastbound vehicles during the evening peak hour.


In addition to the calculated seasonal adjustment for trips to and from Mt. Hood and beyond, a commuter seasonal adjustment was applied to the traffic volumes that do not reach the ATR station in Rhododendron, Oregon. Based on data from ODOT's Seasonal Trend Table, the seasonal adjustment for commuter traffic was calculated to be 2.2 percent. This adjustment was applied to the portion of the through traffic volumes on Highway 26 that represent commuter and local trips. Accordingly, the total adjustment was calculated to be 84 additional vehicles during the PM peak hour (an increase of 4.0 percent to the through traffic volumes on the highway). This 4.0 percent seasonal adjustment was also applied to the through volumes on Highway 26 for the AM count period.

Figure 2 on page 9 shows the resulting seasonally adjusted existing year $202230^{\text {th }}$-highest hour traffic volumes for the morning and evening peak hours at the study intersections.


## OPERATIONAL ANALYSIS

An operational analysis was conducted for the study intersections using Synchro 10 software, with outputs calculated based on the HIGHWAY CAPACITY MANUAL, $6^{\text {th }}$ Edition. The analysis was conducted for the weekday morning and evening peak hours.

The purpose of the existing conditions analysis is to establish how the study area intersections operate currently and allow for calibration of the operational analysis if required.

The results of the operational analysis are reported based on delay, Level of Service (LOS), and volume-to-capacity ratio ( $\mathrm{v} / \mathrm{c}$ ). Delays are reported in seconds. Level of service is reported as a letter grade and can range from A to F, with level of service A representing free-flow conditions and level of service F representing high delays and severe congestion. A report of level of service D generally indicates moderately high but tolerable delays, and typically occurs prior to reaching intersection capacity. For unsignalized intersections, the $\mathrm{v} / \mathrm{c}$ represents the portion of the available intersection capacity that is being utilized on the worst intersection approach. For signalized intersections, it indicates the portion of the overall intersection's capacity that is being used. A v/c ratio of 1.0 would indicate that the intersection is operating at capacity.

The Oregon Department of Transportation requires that the signalized intersection of Highway 26 at SE $362^{\text {nd }}$ Avenue operate with a $\mathrm{v} / \mathrm{c}$ ratio of 0.80 or less during the peak hours.

Intersections operating under the jurisdiction of the City of Sandy are required to operate at level of service D or better. This operational standard applies to the intersections of SE $362^{\text {nd }}$ Avenue at the north and south intersections with Industrial Way, as well as the site access intersections.

A summary of the existing conditions operational analysis is provided in Table 1 on the following page. For the unsignalized intersections the reported delays and levels-of-service represent the approach lane which experiences the highest delays. The reported $\mathrm{v} / \mathrm{c}$ ratios represent the highest ratio for the major-street and minor-street movements. For the signalized intersection of Highway 26 at SE $362^{\text {nd }}$ Avenue, the reported delays, levels-of-service and $v / \mathrm{c}$ ratios represent the operation of the overall intersection.

Based on the analysis, the intersections are currently operating acceptably per the respective ODOT and City of Sandy standards. Detailed capacity analysis worksheets are provided in the technical appendix.

Table 1 - Operational Analysis Summary: Year 2022 30th-Highest Hour Conditions

| Intersection | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Delay | LOS | v/c | Delay | LOS | v/c |
| Highway 26 at SE 362nd Ave. | 13.1 | B | 0.48 | 22.6 | C | 0.68 |
| SE 362nd Ave. at Industrial Way (N) | 12.8 | B | 0.09 | 15.0 | C | 0.21 |
| SE 362nd Ave. at Industrial Way (S) | 11.5 | B | 0.48 | 23.5 | C | 0.76 |
| SE 362nd Ave. at Existing Site Access | 10.8 | B | 0.01 | 13.0 | B | 0.01 |

## Site Trips

## PROPOSED DEVELOPMENT

The subject property currently contains an existing 20,000 square foot industrial main building and a two-story 3,850 square foot office building. The proposed redevelopment plan will also include constructing a new 7,375 square foot shed roof to cover the bus wash area within the site. To estimate the number of trips that will be generated at the site trip rates from the TRIP GENERATION MANUAL, $10^{\text {th }}$ EDITION were used. Data from land-use code 180, Specialty Trade Contractor, were used.

Since the floor area of the existing and proposed facilities is well in excess of the largest comparable facilities within the data set, the trip estimates are based on the number of employees at the site. It is anticipated that 20 to 30 employees will work within the site. To maintain a conservative analysis, the larger estimate of 30 employees was used to assess trip generation for the site.

A summary of the trip generation calculations is provided in Table 2 below. A detailed trip generation worksheet is also included in the technical appendix.

Table 2 - Proposed Development Trip Generation Summary

|  | AM Peak Hour |  |  | PM Peak Hour |  |  | Daily |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In | Out | Total | In | Out | Total |  |
| 30 Employee Specialty Contractor | 13 | 5 | 18 | 7 | 15 | 22 | 108 |

## TRIP DIStRIBUTION

The directional distribution of site trips to and from the project site was estimated based the existing travel patterns in the site vicinity, as well as the locations of likely trip destinations and major transportation routes. Overall, 40 percent of the anticipated site trips are projected to travel to and from the northwest on Highway 26, 45 percent are projected to travel to and from the southeast on Highway 26, and the remaining 15 percent of site trips are projected to travel to and from the west on Dubarko Road.

The trip distribution percentages and trip assignment for the proposed development are shown in Figure 3 on page 12.


## Future Conditions Analysis

## BACKGROUND VOLUMES

In order to determine the expected impact of site trips on the study area intersections, it is necessary to compare traffic conditions both with and without the addition of the projected traffic from the proposed development. This comparison is made for future traffic conditions at the time of project completion. It is anticipated that the proposed use will be completed and occupied within one year. Accordingly, the analysis was conducted for year 2023 traffic conditions.

Prior to adding the projected site trips to the study intersections, the existing traffic volumes were adjusted to account for background traffic growth over time. Based on data from ODOT's 2040 Future Volume Table, the growth rate for traffic volumes on Highway 26 in the site vicinity was calculated to be 1.92 percent per year (linear). This growth rate was applied to the through traffic volumes on Highway 26. All other turning movements had a growth factor of 2 percent per year (exponential) applied.

In addition to the background growth, future site trips associated with other anticipated developments within the City of Sandy were added to the background traffic volumes. These projects included the Mt. Hood Senior Living, The Pad, Cedar Heights Views, Shaylee Meadows, Trimble PD, Bornstedt Views, Cascade Creek Multifamily, Tickle Creek Village, Double Creek Condos, Jewelberry Ridge, Jewelberry Meadows, Sandy Plaza Apartments, FreeUp Storage, and a mixed-use development at 38015 Highway 26. The projected site trips for these residential developments are shown in Figure 6 in the attached technical appendix.

Figure 4 on page 14 shows the projected year 2023 background traffic volumes at the study intersections during the morning and evening peak hours.

## BaCKGRound Volumes plus Site Trips

Peak hour trips calculated to be generated by the proposed development were added to the projected year 2023 background traffic volumes to obtain the year 2023 total traffic volumes following completion of the proposed development.

Figure 5 on page 15 shows the projected year 2023 peak hour volumes including background growth, and site trips from the proposed development for the morning and evening peak hours.
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## OPERATIONAL ANALYSIS

The operational analysis for future traffic conditions was again conducted using Synchro analysis software, with outputs based on the analysis methodologies contained in the HIGHWAY CAPACITY $M A N U A L$. The analysis was prepared for the intersections' morning and evening peak hours.

The results of the operational analysis are summarized in Table 4 below. Detailed analysis worksheets are also included in the technical appendix.

Table 4 - Operational Analysis Summary: Year 2023 Future Conditions

| Intersection | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Delay | LOS | v/c | Delay | LOS | v/c |
| Highway 26 at SE 362nd Ave. |  |  |  |  |  |  |
| 2023 Background Conditions | 13.3 | B | 0.50 | 23.3 | C | 0.72 |
| 2023 Background plus Site | 13.3 | B | 0.50 | 23.4 | C | 0.72 |
| SE 362nd Ave. at Industrial Way (N) |  |  |  |  |  |  |
| 2023 Background Conditions | 13.1 | B | 0.10 | 15.6 | C | 0.22 |
| 2023 Background plus Site | 13.2 | B | 0.10 | 15.8 | C | 0.23 |
| SE 362nd Ave. at Industrial Way (S) |  |  |  |  |  |  |
| 2023 Background Conditions | 12.0 | B | 0.50 | 27.0 | D | 0.81 |
| 2023 Background plus Site | 12.1 | B | 0.51 | 27.7 | D | 0.81 |
| SE 362nd Ave. at Existing Site Access |  |  |  |  |  |  |
| 2023 Background Conditions | 10.9 | B | 0.01 | 13.3 | B | 0.01 |
| 2023 Background plus Site | 11.7 | B | 0.01 | 13.4 | B | 0.02 |
| Industrial Way at Proposed Site Access |  |  |  |  |  |  |
| 2023 Background plus Site | 9.7 | A | 0.01 | 9.4 | A | 0.01 |

Upon completion of the proposed development, all study intersections are projected to operate acceptably per the appropriate jurisdictional standards.

## QUEUING ANALYSIS

A queuing analysis was conducted using SimTraffic software to determine whether standing queues on the major streets will impact operation of the site access driveways. The SE $362^{\text {nd }}$ Avenue northbound approach toward Industrial Way (South) has projected $95^{\text {th }}$ percentile queue lengths of 103 feet and 115 feet during the morning and evening peak hours, respectively. The existing site access is planned to be moved 50 feet south of its existing alignment in conjunction with the proposed development, resulting in an access spacing of 93 feet between the northbound stop bar and the near side of the driveway. Although the proposed access location is within the 95 th percentile queue lengths it is less than the average queue lengths during the peak hours ( 67 feet and 73 feet during the AM and PM peak hours, respectively) and will align directly opposite an existing driveway on the west side of SE $362^{\text {nd }}$ Avenue. This represents an improvement in access spacing as compared to existing conditions.

## Safety Analysis

## CRASH Data ANALYSIS

Using data obtained from the Oregon Department of Transportation, a review of the five most recent years of available crash history (from January 2016 through December 2020) was performed for the study intersections. The crash data was evaluated based on the number, type, and severity of collisions, as well as the intersection crash rate. Crash rates allow comparison of relative safety risks at intersections with different lane configurations, volumes, and traffic control devices by accounting for both the number of crashes that occur during the study period and the number of vehicles that traveled through the intersection during that period. Crash rates are calculated using the standard assumption that evening peak hour volumes are approximately 10 percent of the average daily traffic volume at an intersection. The crash rates were compared to statewide crash rates for similar intersection types to identify any locations with crash rates in excess of the $90^{\text {th }}$ percentile.

The intersection of Highway 26 at SE $362^{\text {nd }}$ Avenue had 22 reported collisions during the five-year analysis period. These included 15 rear-end collisions, 6 turning-movement collisions, and one pedestrian collision. The pedestrian collision occurred when a pedestrian crossed Highway 26 without a walk signal in the dark and was struck by a driver making a northbound right turn from SE $362^{\text {nd }}$ Avenue onto Highway 26. The crash resulted in a "possible injury/complaint of pain" from the pedestrian. The crashes resulted in no incapacitating injuries or fatalities, two non-incapacitating injuries, and 18 reports of a "possible injury/complaint of pain". The crash rate for the intersection was calculated to be 0.362 crashes per million entering vehicles. This is well below the $90^{\text {th }}$ percentile crash rate of 0.509 crashes per million entering vehicles for signalized, three-way urban intersections in Oregon.

The intersections of SE $362^{\text {nd }}$ Avenue at Industrial Way had four total reported collisions during the five-year analysis period. These included three read-end collisions and one turning-movement collision. The crashes resulted in four reports of a "possible injury/complaint of pain." No serious injuries or fatalities were reported. Conservatively assuming that all reported crashes occurred at the same intersection, the crash rate for the intersection would be 0.203 crashes per million entering vehicles, which is still below the $90^{\text {th }}$ percentile crash rate of 0.293 crashes per million entering vehicles for stop-controlled, three-way urban intersections in Oregon.

Based on the crash data, the study intersections are currently operating acceptably with respect to safety. No specific safety improvements are recommended for the study area intersections.

## Traffic Signal Warrant analysis

Traffic signal warrants were examined for the unsignalized study intersections. Based on the projected traffic volumes, traffic signal warrants are not projected to be met for any of the unsignalized study intersections under any of the analysis scenarios.

## TURN LANE WARRANT ANALYSIS

Turn lane warrants were also examined for the major-street approaches to the unsignalized study intersections. Left-turn lane warrants are intended to evaluate whether a meaningful safety benefit may be expected if the turning vehicles are provided with a turn lane within the street, allowing leftturning drivers to move out of the through travel lane so that following vehicles may pass without conflicts. Similarly, right-turn lane warrants are intended to evaluate whether a meaningful safety benefit may be expected if a right-turn lane is provided, allowing right-turning vehicles to move out of the through travel lane while decelerating and making turns.

The intersection of SE $362^{\text {nd }}$ Avenue at Industrial Way (North) already has a southbound left-turn lane in place. Right-turn lane warrants are not projected to be met at this intersection.

Turn lane warrants are not directly applicable at the intersection of SE $362^{\text {nd }}$ Avenue and Industrial Way (South), since the intersection operates under all-way stop control. All vehicles must stop prior to entering the intersection and providing a separate turn lane would not allow through vehicles to traverse the intersection without slowing and stopping. The need for turn lanes at all-way stop control intersections is based on operational rather than safety benefits. In this instance, the intersection operates acceptably without the addition of left and right turn lanes. Therefore, no new turn lanes are recommended at this intersection in conjunction with the proposed development.

The intersections of SE $362^{\text {nd }}$ Avenue at the site access and Industrial Way at the proposed site access are not projected to meet turn lane warrants under any analysis scenarios.

## Intersection Sight Distance Analysis

Intersection sight distance was examined for the proposed re-aligned site access intersections on SE $362^{\text {nd }}$ Avenue and for the proposed new site access on Industrial Way.

## SE $362^{\text {nd }}$ Avenue at Re-Aligned Site Access

The existing site access on SE $362^{\text {nd }}$ Avenue is proposed to be re-aligned to a position 50 feet south of the existing driveway alignment. The proposed new alignment increases the access spacing between the driveway and the nearby all-way stop controlled intersection at Industrial Way. It also aligns the proposed access directly opposite another existing driveway on the west side of the roadway.

SE $362^{\text {nd }}$ Avenue has a posted speed limit of 35 mph , typically requiring a minimum of 390 feet of intersection sight distance in each direction. However, the actual $85^{\text {th }}$ percentile approach speeds were used in lieu of the posted speed limit to evaluate sight distance in both directions.

For southbound traffic approaching the proposed re-aligned site access on SE $362^{\text {nd }}$ Avenue, all approaching vehicles must stop prior to entering the intersection. Intersection sight distance was measured to be continuous beyond the stop-controlled intersection at Industrial Way. The effective
approach speed from the intersection is thus zero miles per hour, and adequate intersection sight distance for safe and efficient operation is available.

Intersection sight distance was measured to be 324 feet to the south from the proposed re-aligned site access. For northbound traffic approaching the proposed re-aligned site access on SE $362^{\text {nd }}$ Avenue, the measured $85^{\text {th }}$ percentile speed at the limits of sight distance was 37 mph . For this design speed, a minimum of 410 feet of intersection sight distance would typically be desired. However, this intersection sight distance requirement is predicated on the idea of allowing sufficient sight lines such that through traffic will not need to slow to avoid conflicts at the studied intersection. In this instance, all northbound traffic must slow when approaching the site access since it is in close proximity to the northbound stop bar at Industrial Way, so the assumptions underlying the typical intersection sight distance requirements are not directly applicable.

The required stopping sight distance for an approach speed of 37 mph was calculated to be 270 feet. Since the available intersection sight distance to the south is in excess of 270 feet, northbound vehicles approaching the site access have sufficient sight lines to see vehicles entering the roadway at the proposed site access location and slow or stop to avoid collisions. As such, the site access can operate safely. Since all northbound vehicles must slow (and stop) prior to reaching Industrial Way, the potential induced delays to northbound through traffic are not projected to materially impact operation of SE $362^{\text {nd }}$ Avenue either at the proposed re-aligned site access location or at Industrial Way.

Based on the detailed analysis, sight lines at the proposed re-aligned site access location are sufficient to allow for safe and efficient operation of the site access. Since the proposed re-alignment also results in increased access spacing and direct alignment opposite an existing driveway, the proposed re-aligned access will operate better than the existing site access and is expected to represent the optimal location for the driveway within the site frontage.

## Industrial Way at Proposed Site Access

The proposed new site access is centered approximately 40 feet west of the site's east property line on Industrial Way. Industrial Way has a posted speed limit of 25 mph . The desired intersection sight distance for this approach speed is 280 feet in each direction.

Intersection sight distance to the west from the proposed access location on Industrial Way is currently obstructed by vegetation within the site frontage. However, with clearing of the vegetation continuous sight lines to SE $362^{\text {nd }}$ Avenue can be provided to the west. The proposed access will be located 230 feet east of the traveled way on SE $362^{\text {nd }}$ Avenue, indicating that a minimum of 230 feet of intersection sight distance will be provided in this direction. Vehicles approaching from beyond the intersection at SE $362^{\text {nd }}$ Avenue will need to make a 90 -degree turn onto Industrial Way. Typical turning speeds are in the range of 9 to 19 mph , while the available intersection sight distance to the west will be sufficient for turning speeds of up to 20 mph . The available intersection sight distance to the west is also projected to provide adequate stopping sight distance for approach speeds up to 33 mph . Based on the analysis, adequate sight lines for safe and efficient operation can be attained to the west of the proposed access location upon clearing of vegetation within the site frontage.

Intersection sight distance to the east from the proposed access location on Industrial Way was measured to be 248 feet, as limited by a large concrete block which provides a fire department standpipe connection that serves the property immediately east of the Johnson RV site.

For westbound traffic approaching the proposed site access on Industrial Way, the measured $85^{\text {th }}$ percentile speed at the limits of sight distance was 33 mph . This design speed requires a minimum of 230 feet of stopping sight distance for safety. Since the available intersection sight distance is in excess of 230 feet, the intersection has adequate sight lines for through vehicles to anticipate and avoid collisions at the site access. However, interruptions to the flow of through traffic along Industrial Way may be expected when vehicles pull out from the proposed access driveway.

In order to assess the anticipated delays which would be induced by operation of the proposed driveway on Industrial Way, a detailed delay analysis was conducted.

For vehicles traveling at speeds of up to 33 mph , the available intersection sight distance of 248 feet accommodates approximately 5.1 seconds of travel time. Typically, intersections are designed to accommodate 7.5 seconds of travel time at the design speed in order to avoid undue delays to through traffic. Accordingly, vehicles entering Industrial Way from the proposed site access have the potential to add as much as 2.4 seconds of additional delay to through traffic per vehicle exiting from the proposed driveway. Assuming random arrivals, the average added delay per affected vehicle would be 1.2 seconds (half the maximum value).

A conservative estimate of the likelihood of conflicts resulting in any induced delay can be calculated based on the volume of westbound traffic traveling on Industrial Way during the highestvolume hour. In this instance, the highest westbound volumes occur during the evening peak hour when 91 westbound through vehicles are projected at the site access. Conservatively assuming that each approaching vehicle has a 2.4 -second window during which a vehicle exiting the site would require the westbound driver to slow, each vehicle making a left turn from the site access onto Industrial Way would have a 6 percent chance of experiencing a conflict with westbound through traffic which induces a delay. Since approximately 10 vehicles per day are projected to make this turning movement, the average induced delay was calculated to be 0.72 seconds per day ( 10 vehicles per day * $6 \%$ chance of conflict * 1.2 seconds average delay per conflict). This equates to approximately 4.4 minutes of induced delay per year. The economic impact of these cumulative delays would be $\$ 2.19$ per year assuming a time value of $\$ 30$ per hour. Based on the minimal economic impact, any meaningful mitigation would result in costs well in excess of the actual impacts of the proposed site access.

Based on the analysis, adequate intersection sight distance is available in each direction for safe operation of the proposed site access on Industrial Way. Since sight lines are limited to the east by a large concrete block which provides a fire department standpipe connection that serves the property immediately east of the Johnson RV site, some induced delays are expected since westbound through vehicles may need to slow or stop to avoid collisions at the site access. The overall impact of these delays is negligible, however. Accordingly, operation of the proposed site access is not projected to result in any significant operational or safety concerns.

## Conclusions

Based on the operational analysis, the study intersections are currently operating acceptably per City of Sandy and ODOT standards. Under year 2023 traffic conditions the intersections are projected to continue to operate acceptably either with or without the addition of site trips from the proposed use. No operational mitigations are necessary or recommended.

Based on the queueing analysis, the projected northbound queues on SE $362^{\text {nd }}$ Avenue are projected to extend beyond the proposed driveway location during a portion of the peak hours. However, average queue lengths even during the peak hours will not obstruct the driveway, and the proposed driveway re-alignment will provide 50 feet of added access spacing as compared to existing conditions, and the driveway will be aligned directly opposite an existing driveway on the west side of SE $362^{\text {nd }}$ Avenue.

Based on the crash data, the study intersections are currently operating acceptably with respect to safety. No specific safety improvements are recommended in conjunction with the proposed site use.

Based on the warrant analysis, no new turn lanes or traffic signals are recommended in conjunction with the proposed site use.

The proposed re-aligned site access on SE $362^{\text {nd }}$ Avenue is projected to have adequate sight distance for safe and efficient operation. The proposed new site access on Industrial Way is projected to have adequate sight distance to the west upon clearing of vegetation within the site frontage allowing a clear line of sight to SE $362^{\text {nd }}$ Avenue. Sight distance to the east is restricted by an existing concrete block which supports a fire department standpipe connection that serves the property immediately east of the Johnson RV site. Although sight lines to the east are restricted, the available intersection sight distance is sufficient for safe operation of the access, and operational impacts associated with the limited sight distance are negligible. Accordingly, the proposed site access on Industrial Way can also operate safely and efficiently.


## APPENDIX




Note: Total study counts contained in parentheses.

|  | HV\% | PHF |
| :--- | :---: | :---: |
| EB | $9.8 \%$ | 0.84 |
| WB | $4.4 \%$ | 0.94 |
| NB | $4.5 \%$ | 0.92 |
| SB | $0.0 \%$ | 0.00 |
| All | $6.5 \%$ | 0.93 |

Traffic Counts - Motorized Vehicles

| Interval | HWY 26 <br> Eastbound |  |  |  | HWY 26 <br> Westbound |  |  |  | SE 362ND DR Northbound |  |  |  | SE 362ND DR Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 7:00 AM | 0 | 0 | 60 | 7 | 0 | 4 | 69 | 0 | 0 | 21 | 0 | 1 | 0 | 0 | 0 | 0 | 162 | 2,185 |
| 7:05 AM | 0 | 0 | 37 | 9 | 0 | 8 | 82 | 0 | 0 | 22 | 0 | 5 | 0 | 0 | 0 | 0 | 163 | 2,202 |
| 7:10 AM | 0 | 0 | 40 | 8 | 0 | 7 | 68 | 0 | 0 | 26 | 0 | 3 | 0 | 0 | 0 | 0 | 152 | 2,181 |
| 7:15 AM | 0 | 0 | 50 | 6 | 0 | 3 | 89 | 0 | 0 | 30 | 0 | 3 | 0 | 0 | 0 | 0 | 181 | 2,203 |
| 7:20 AM | 0 | 0 | 45 | 8 | 0 | 3 | 90 | 0 | 0 | 22 | 0 | 7 | 0 | 0 | 0 | 0 | 175 | 2,192 |
| 7:25 AM | 0 | 0 | 78 | 16 | 0 | 4 | 76 | 0 | 0 | 21 | 0 | 4 | 0 | 0 | 0 | 0 | 199 | 2,184 |
| 7:30 AM | 0 | 0 | 65 | 16 | 0 | 7 | 71 | 0 | 0 | 26 | 0 | 8 | 0 | 0 | 0 | 0 | 193 | 2,148 |
| 7:35 AM | 0 | 0 | 52 | 6 | 0 | 8 | 80 | 0 | 0 | 26 | 0 | 7 | 0 | 0 | 0 | 0 | 179 | 2,109 |
| 7:40 AM | 0 | 0 | 71 | 9 | 0 | 11 | 71 | 0 | 0 | 22 | 0 | 9 | 0 | 0 | 0 | 0 | 193 | 2,143 |
| 7:45 AM | 0 | 0 | 49 | 11 | 0 | 7 | 73 | 0 | 0 | 19 | 0 | 13 | 0 | 0 | 0 | 0 | 172 | 2,139 |
| 7:50 AM | 0 | 0 | 85 | 13 | 0 | 11 | 67 | 0 | 0 | 21 | 0 | 5 | 0 | 0 | 0 | 0 | 202 | 2,147 |
| 7:55 AM | 0 | 0 | 71 | 21 | 0 | 9 | 78 | 0 | 0 | 23 | 0 | 12 | 0 | 0 | 0 | 0 | 214 | 2,133 |
| 8:00 AM | 0 | 0 | 71 | 8 | 0 | 7 | 67 | 0 | 0 | 18 | 0 | 8 | 0 | 0 | 0 | 0 | 179 | 2,107 |
| 8:05 AM | 0 | 0 | 41 | 9 | 0 | 8 | 60 | 0 | 0 | 17 | 0 | 7 | 0 | 0 | 0 | 0 | 142 |  |
| 8:10 AM | 0 | 0 | 51 | 9 | 0 | 10 | 77 | 0 | 0 | 16 | 0 | 11 | 0 | 0 | 0 | 0 | 174 |  |
| 8:15 AM | 0 | 0 | 71 | 17 | 0 | 4 | 58 | 0 | 0 | 10 | 0 | 10 | 0 | 0 | 0 | 0 | 170 |  |
| 8:20 AM | 0 | 0 | 52 | 8 | 0 | 10 | 57 | 0 | 0 | 26 | 0 | 14 | 0 | 0 | 0 | 0 | 167 |  |
| 8:25 AM | 0 | 0 | 59 | 7 | 0 | 7 | 68 | 0 | 0 | 12 | 0 | 10 | 0 | 0 | 0 | 0 | 163 |  |
| 8:30 AM | 0 | 0 | 57 | 5 | 0 | 7 | 52 | 0 | 0 | 19 | 0 | 14 | 0 | 0 | 0 | 0 | 154 |  |
| 8:35 AM | 0 | 0 | 58 | 5 | 0 | 12 | 101 | 0 | 0 | 25 | 0 | 12 | 0 | 0 | 0 | 0 | 213 |  |
| 8:40 AM | 0 | 0 | 68 | 10 | 0 | 9 | 69 | 0 | 0 | 19 | 0 | 14 | 0 | 0 | 0 | 0 | 189 |  |
| 8:45 AM | 0 | 0 | 77 | 8 | 0 | 10 | 55 | 0 | 0 | 18 | 0 | 12 | 0 | 0 | 0 | 0 | 180 |  |
| 8:50 AM | 0 | 0 | 76 | 9 | 0 | 11 | 65 | 0 | 0 | 18 | 0 | 9 | 0 | 0 | 0 | 0 | 188 |  |
| 8:55 AM | 0 | 0 | 78 | 14 | 0 | 16 | 62 | 0 | 0 | 9 | 0 | 9 | 0 | 0 | 0 | 0 | 188 |  |
| Count Total | 0 | 0 | 1,462 | 239 | 0 | 193 | 1,705 | 0 | 0 | 486 | 0 | 207 | 0 | 0 | 0 | 0 | 4,292 |  |
| Peak Hour | 0 | 0 | 729 | 132 | 0 | 88 | 899 | 0 | 0 | 261 | 0 | 94 | 0 | 0 | 0 | 0 | 2,203 |  |

Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles on Crosswalk

| Interval | Heavy Vehicles |  |  |  |  |  | Interval Start Time | Bicycles on Roadway |  |  |  |  |  | Interval <br> Start Time | Pedestrians/Bicycles on Crosswalk |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | EB | NB | WB | SB |  | Total |  | EB |  | NB | WB | SB | Total |  | EB |  | NB | WB | SB | Total |
| 7:00 AM | 12 | 0 | 4 |  | 0 | 16 | 7:00 AM |  | 0 | 0 | 0 | 0 | 0 | 7:00 AM |  | 0 | 0 | 0 | 0 | 0 |
| 7:05 AM | 7 | 0 | 6 |  | 0 | 13 | 7:05 AM |  | 0 | 0 | 0 | 0 | 0 | 7:05 AM |  | 0 | 0 | 0 | 0 | 0 |
| 7:10 AM | 3 | 2 | 1 |  | 0 | 6 | 7:10 AM |  | 0 | 0 | 0 | 0 | 0 | 7:10 AM |  | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 11 | 2 | 1 |  | 0 | 14 | 7:15 AM |  | 0 | 0 | 0 | 0 | 0 | 7:15 AM |  | 0 | 0 | 0 | 0 | 0 |
| 7:20 AM | 6 | 0 | 1 |  | 0 | 7 | 7:20 AM |  | 0 | 0 | 0 | 0 | 0 | 7:20 AM |  | 0 | 0 | 0 | 0 | 0 |
| 7:25 AM | 9 | 0 | 1 |  | 0 | 10 | 7:25 AM |  | 0 | 0 | 1 | 0 | 1 | 7:25 AM |  | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 10 | 2 | 3 |  | 0 | 15 | 7:30 AM |  | 0 | 0 | 0 | 0 | 0 | 7:30 AM |  | 0 | 0 | 0 | 0 | 0 |
| 7:35 AM | 3 | 1 | 2 |  | 0 | 6 | 7:35 AM |  | 0 | 0 | 0 | 0 | 0 | 7:35 AM |  | 0 | 0 | 0 | 0 | 0 |
| 7:40 AM | 6 | 0 | 5 |  | 0 | 11 | 7:40 AM |  | 0 | 0 | 0 | 0 | 0 | 7:40 AM |  | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 5 | 1 | 5 |  | 0 | 11 | 7:45 AM |  | 0 | 0 | 0 | 0 | 0 | 7:45 AM |  | 0 | 0 | 0 | 0 | 0 |
| 7:50 AM | 11 | 1 | 5 |  | 0 | 17 | 7:50 AM |  | 0 | 0 | 0 | 0 | 0 | 7:50 AM |  | 0 | 0 | 0 | 0 | 0 |
| 7:55 AM | 10 | 4 | 6 |  | 0 | 20 | 7:55 AM |  | 0 | 0 | 0 | 0 | 0 | 7:55 AM |  | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 2 | 1 | 5 |  | 0 | 8 | 8:00 AM |  | 0 | 0 | 0 | 0 | 0 | 8:00 AM |  | 0 | 0 | 0 | 0 | 0 |
| 8:05 AM | 4 | 0 | 5 |  | 0 | 9 | 8:05 AM |  | 0 | 0 | 0 | 0 | 0 | 8:05 AM |  | 0 | 0 | 0 | 0 | 0 |
| 8:10 AM | 7 | 4 | 4 |  | 0 | 15 | 8:10 AM |  | 0 | 0 | 0 | 0 | 0 | 8:10 AM |  | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 16 | 1 | 3 |  | 0 | 20 | 8:15 AM |  | 0 | 0 | 0 | 0 | 0 | 8:15 AM |  | 0 | 0 | 1 | 1 | 2 |
| 8:20 AM | 3 | 3 | 2 |  | 0 | 8 | 8:20 AM |  | 0 | 0 | 0 | 0 | 0 | 8:20 AM |  | 0 | 0 | 0 | 0 | 0 |
| 8:25 AM | 8 | 2 | 7 |  | 0 | 17 | 8:25 AM |  | 0 | 0 | 0 | 0 | 0 | 8:25 AM |  | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 6 | 1 | 9 |  | 0 | 16 | 8:30 AM |  | 0 | 0 | 0 | 0 | 0 | 8:30 AM |  | 0 | 0 | 0 | 0 | 0 |
| 8:35 AM | 7 | 2 | 6 |  | 0 | 15 | 8:35 AM |  | 0 | 0 | 0 | 0 | 0 | 8:35 AM |  | 0 | 0 | 0 | 0 | 0 |
| 8:40 AM | 7 | 1 | 7 |  | 0 | 15 | 8:40 AM |  | 0 | 0 | 0 | 0 | 0 | 8:40 AM |  | 0 | 1 | 0 | 0 | 1 |
| 8:45 AM | 12 | 2 | 4 |  | 0 | 18 | 8:45 AM |  | 0 | 0 | 0 | 0 | 0 | 8:45 AM |  | 0 | 0 | 0 | 0 | 0 |
| 8:50 AM | 11 | 1 | 9 |  | 0 | 21 | 8:50 AM |  | 0 | 0 | 0 | 0 | 0 | 8:50 AM |  | 0 | 0 | 0 | 0 | 0 |
| 8:55 AM | 5 | 1 | 5 |  | 0 | 11 | 8:55 AM |  | 0 | 0 | 0 | 0 | 0 | 8:55 AM |  | 0 | 0 | 0 | 0 | 0 |
| Count Total | 181 | 32 | 106 |  | 0 | 319 | Count Total |  | 0 | 0 | 1 | 0 | 1 | Count Total |  | 0 | 1 | 1 | 1 | 3 |
| Peak Hour | 84 | 16 | 43 |  | 0 | 143 | Peak Hour |  | 0 | 0 | 1 | 0 | 1 | Peak Hour |  | 0 | 0 | 0 | 0 | 0 |



Note: Total study counts contained in parentheses.

|  | HV\% | PHF |
| :---: | :---: | :---: |
| EB | $0.0 \%$ | 0.00 |
| WB | $14.6 \%$ | 0.80 |
| NB | $6.2 \%$ | 0.89 |
| SB | $6.4 \%$ | 0.82 |
| All | $6.9 \%$ | 0.90 |

Traffic Counts - Motorized Vehicles

| Interval | INDUSTRIAL WAY EAST Eastbound |  |  |  | INDUSTRIAL WAY EAST <br> Westbound |  |  |  | SE 362ND DR Northbound |  |  |  | SE 362ND DR Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 21 | 3 | 0 | 3 | 4 | 0 | 31 | 520 |
| 7:05 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 25 | 1 | 0 | 2 | 8 | 0 | 37 | 528 |
| 7:10 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 29 | 5 | 0 | 5 | 6 | 0 | 45 | 529 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 2 | 0 | 2 | 6 | 0 | 35 | 521 |
| 7:20 AM | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 28 | 4 | 0 | 1 | 9 | 0 | 47 | 536 |
| 7:25 AM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 24 | 2 | 0 | 5 | 8 | 0 | 42 | 529 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 36 | 5 | 0 | 7 | 10 | 0 | 60 | 523 |
| 7:35 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 21 | 3 | 0 | 1 | 7 | 0 | 35 | 515 |
| 7:40 AM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 26 | 1 | 0 | 2 | 10 | 0 | 43 | 525 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 26 | 3 | 0 | 3 | 18 | 0 | 51 | 527 |
| 7:50 AM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 25 | 7 | 0 | 3 | 7 | 0 | 45 | 517 |
| 7:55 AM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 24 | 4 | 0 | 3 | 15 | 0 | 49 | 506 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 20 | 7 | 0 | 4 | 3 | 0 | 39 | 503 |
| 8:05 AM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 22 | 3 | 0 | 1 | 9 | 0 | 38 |  |
| 8:10 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 19 | 3 | 0 | 3 | 10 | 0 | 37 |  |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 2 | 0 | 0 | 22 | 3 | 0 | 3 | 15 | 0 | 50 |  |
| 8:20 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 24 | 3 | 0 | 2 | 8 | 0 | 40 |  |
| 8:25 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 18 | 0 | 0 | 2 | 12 | 0 | 36 |  |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 28 | 4 | 0 | 1 | 17 | 0 | 52 |  |
| 8:35 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 30 | 3 | 0 | 0 | 8 | 0 | 45 |  |
| 8:40 AM | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 27 | 1 | 0 | 2 | 11 | 0 | 45 |  |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 27 | 3 | 0 | 1 | 9 | 0 | 41 |  |
| 8:50 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 15 | 3 | 0 | 1 | 11 | 0 | 34 |  |
| 8:55 AM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 4 | 0 | 0 | 20 | 3 | 0 | 1 | 16 | 0 | 46 |  |
| Count Total | 0 | 0 | 0 | 0 | 0 | 37 | 0 | 33 | 0 | 0 | 582 | 76 | 0 | 58 | 237 | 0 | 1,023 |  |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 26 | 0 | 15 | 0 | 0 | 293 | 45 | 0 | 36 | 121 | 0 | 536 |  |

Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles on Crosswalk



Note: Total study counts contained in parentheses.

|  | HV\% | PHF |
| :--- | :---: | :---: |
| EB | $13.8 \%$ | 0.78 |
| WB | $0.0 \%$ | 0.00 |
| NB | $5.2 \%$ | 0.89 |
| SB | $8.7 \%$ | 0.84 |
| All | $7.4 \%$ | 0.90 |

Traffic Counts - Motorized Vehicles

| Interval Start Time | INDUSTRIAL WAY WEST Eastbound |  |  |  | INDUSTRIAL WAY WEST <br> Westbound |  |  |  | SE 362ND DR Northbound |  |  |  | SE 362ND DR Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 7:00 AM | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 21 | 0 | 0 | 0 | 4 | 2 | 37 | 561 |
| 7:05 AM | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 18 | 0 | 0 | 0 | 4 | 2 | 35 | 565 |
| 7:10 AM | 0 | 3 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 2 | 29 | 0 | 0 | 0 | 4 | 3 | 45 | 570 |
| 7:15 AM | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 12 | 26 | 0 | 0 | 0 | 4 | 2 | 48 | 568 |
| 7:20 AM | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 4 | 25 | 0 | 0 | 0 | 5 | 4 | 46 | 558 |
| 7:25 AM | 0 | 9 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 5 | 22 | 0 | 0 | 0 | 7 | 4 | 50 | 568 |
| 7:30 AM | 0 | 6 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 6 | 23 | 0 | 0 | 0 | 10 | 0 | 48 | 553 |
| 7:35 AM | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 2 | 34 | 0 | 0 | 0 | 8 | 3 | 53 | 558 |
| 7:40 AM | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 5 | 23 | 0 | 0 | 0 | 4 | 4 | 40 | 551 |
| 7:45 AM | 0 | 4 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 7 | 21 | 0 | 0 | 0 | 11 | 4 | 49 | 560 |
| 7:50 AM | 0 | 5 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 2 | 32 | 0 | 0 | 0 | 10 | 4 | 59 | 564 |
| 7:55 AM | 0 | 10 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 20 | 0 | 0 | 0 | 13 | 4 | 51 | 548 |
| 8:00 AM | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 16 | 0 | 0 | 0 | 10 | 2 | 41 | 537 |
| 8:05 AM | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 5 | 22 | 0 | 0 | 0 | 4 | 3 | 40 |  |
| 8:10 AM | 0 | 5 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 22 | 0 | 0 | 0 | 8 | 4 | 43 |  |
| 8:15 AM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 20 | 0 | 0 | 0 | 11 | 2 | 38 |  |
| 8:20 AM | 0 | 3 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 5 | 28 | 0 | 0 | 0 | 9 | 7 | 56 |  |
| 8:25 AM | 0 | 5 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 4 | 9 | 0 | 0 | 0 | 9 | 2 | 35 |  |
| 8:30 AM | 0 | 8 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 2 | 23 | 0 | 0 | 0 | 12 | 4 | 53 |  |
| 8:35 AM | 0 | 7 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 22 | 0 | 0 | 0 | 10 | 3 | 46 |  |
| 8:40 AM | 0 | 6 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 6 | 23 | 0 | 0 | 0 | 8 | 1 | 49 |  |
| 8:45 AM | 0 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 4 | 33 | 0 | 0 | 0 | 7 | 4 | 53 |  |
| 8:50 AM | 0 | 6 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 6 | 15 | 0 | 0 | 0 | 12 | 1 | 43 |  |
| 8:55 AM | 0 | 6 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 2 | 13 | 0 | 0 | 0 | 12 | 4 | 40 |  |
| Count Total | 0 | 119 | 0 | 69 | 0 | 0 | 0 | 0 | 0 | 101 | 540 | 0 | 0 | 0 | 196 | 73 | 1,098 |  |
| Peak Hour | 0 | 58 | 0 | 36 | 0 | 0 | 0 | 0 | 0 | 56 | 293 | 0 | 0 | 0 | 90 | 37 | 570 |  |

Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles on Crosswalk

| Interval | Heavy Vehicles |  |  |  |  | Interval Start Time | Bicycles on Roadway |  |  |  |  | Interval <br> Start Time | Pedestrians/Bicycles on Crosswalk |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |
| 7:00 AM | 0 | 0 | 0 | 2 | 2 | 7:00 AM | 0 | 0 | 0 | 0 | 0 | 7:00 AM | 0 | 0 | 0 | 0 | 0 |
| 7:05 AM | 1 | 1 | 0 | 3 | 5 | 7:05 AM | 0 | 0 | 0 | 0 | 0 | 7:05 AM | 0 | 0 | 0 | 0 | 0 |
| 7:10 AM | 0 | 1 | 0 | 1 | 2 | 7:10 AM | 0 | 0 | 0 | 0 | 0 | 7:10 AM | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 1 | 2 | 0 | 0 | 3 | 7:15 AM | 0 | 0 | 0 | 0 | 0 | 7:15 AM | 0 | 0 | 0 | 0 | 0 |
| 7:20 AM | 3 | 0 | 0 | 1 | 4 | 7:20 AM | 0 | 0 | 0 | 0 | 0 | 7:20 AM | 0 | 0 | 0 | 0 | 0 |
| 7:25 AM | 1 | 1 | 0 | 2 | 4 | 7:25 AM | 0 | 0 | 0 | 0 | 0 | 7:25 AM | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 1 | 2 | 0 | 0 | 3 | 7:30 AM | 0 | 0 | 0 | 0 | 0 | 7:30 AM | 0 | 0 | 0 | 0 | 0 |
| 7:35 AM | 2 | 2 | 0 | 0 | 4 | 7:35 AM | 0 | 0 | 0 | 0 | 0 | 7:35 AM | 0 | 0 | 0 | 0 | 0 |
| 7:40 AM | 0 | 2 | 0 | 0 | 2 | 7:40 AM | 0 | 0 | 0 | 0 | 0 | 7:40 AM | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 2 | 0 | 1 | 3 | 7:45 AM | 0 | 0 | 0 | 0 | 0 | 7:45 AM | 2 | 2 | 0 | 0 | 4 |
| 7:50 AM | 2 | 2 | 0 | 2 | 6 | 7:50 AM | 0 | 0 | 0 | 0 | 0 | 7:50 AM | 0 | 0 | 1 | 1 | 2 |
| 7:55 AM | 2 | 1 | 0 | 1 | 4 | 7:55 AM | 0 | 0 | 0 | 0 | 0 | 7:55 AM | 0 | 0 | 1 | 1 | 2 |
| 8:00 AM | 0 | 2 | 0 | 3 | 5 | 8:00 AM | 0 | 0 | 0 | 0 | 0 | 8:00 AM | 0 | 0 | 0 | 0 | 0 |
| 8:05 AM | 1 | 1 | 0 | 0 | 2 | 8:05 AM | 0 | 0 | 0 | 0 | 0 | 8:05 AM | 0 | 0 | 0 | 0 | 0 |
| 8:10 AM | 4 | 3 | 0 | 2 | 9 | 8:10 AM | 0 | 0 | 0 | 0 | 0 | 8:10 AM | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 1 | 4 | 0 | 3 | 8 | 8:15 AM | 0 | 0 | 0 | 0 | 0 | 8:15 AM | 0 | 0 | 1 | 0 | 1 |
| 8:20 AM | 1 | 3 | 0 | 2 | 6 | 8:20 AM | 0 | 0 | 0 | 0 | 0 | 8:20 AM | 0 | 0 | 0 | 0 | 0 |
| 8:25 AM | 1 | 1 | 0 | 1 | 3 | 8:25 AM | 0 | 0 | 0 | 0 | 0 | 8:25 AM | 0 | 0 | 2 | 2 | 4 |
| 8:30 AM | 1 | 1 | 0 | 2 | 4 | 8:30 AM | 0 | 0 | 0 | 0 | 0 | 8:30 AM | 0 | 0 | 0 | 0 | 0 |
| 8:35 AM | 1 | 0 | 0 | 0 | 1 | 8:35 AM | 0 | 0 | 0 | 0 | 0 | 8:35 AM | 0 | 0 | 0 | 0 | 0 |
| 8:40 AM | 1 | 3 | 0 | 2 | 6 | 8:40 AM | 0 | 0 | 0 | 0 | 0 | 8:40 AM | 0 | 0 | 1 | 1 | 2 |
| 8:45 AM | 1 | 0 | 0 | 2 | 3 | 8:45 AM | 0 | 0 | 0 | 0 | 0 | 8:45 AM | 0 | 0 | 0 | 0 | 0 |
| 8:50 AM | 0 | 1 | 0 | 3 | 4 | 8:50 AM | 0 | 0 | 0 | 0 | 0 | 8:50 AM | 1 | 1 | 0 | 0 | 2 |
| 8:55 AM | 0 | 2 | 0 | 1 | 3 | 8:55 AM | 0 | 0 | 0 | 0 | 0 | 8:55 AM | 0 | 0 | 0 | 0 | 0 |
| Count Total | 25 | 37 | 0 | 34 | 96 | Count Total | 0 | 0 | 0 | 0 | 0 | Count Total | 3 | 3 | 6 | 5 | 17 |
| Peak Hour | 13 | 18 | 0 | 11 | 42 | Peak Hour | 0 | 0 | 0 | 0 | 0 | Peak Hour | 2 | 2 | 2 | 2 | 8 |



Note: Total study counts contained in parentheses.

|  | HV\% | PHF |
| :--- | :---: | :---: |
| EB | $3.5 \%$ | 0.95 |
| WB | $4.3 \%$ | 0.95 |
| NB | $1.3 \%$ | 0.95 |
| SB | $0.0 \%$ | 0.00 |
| All | $3.4 \%$ | 0.96 |

Traffic Counts - Motorized Vehicles

| Interval Start Time | HWY 26 <br> Eastbound |  |  |  | HWY 26 <br> Westbound |  |  |  | SE 362ND DR Northbound |  |  |  | SE 362ND DR Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 4:00 PM | 0 | 0 | 60 | 6 | 0 | 22 | 84 | 0 | 0 | 20 | 0 | 15 | 0 | 0 | 0 | 0 | 207 | 2,742 |
| 4:05 PM | 0 | 0 | 40 | 9 | 0 | 21 | 75 | 0 | 0 | 44 | 0 | 19 | 0 | 0 | 0 | 0 | 208 | 2,828 |
| 4:10 PM | 0 | 0 | 41 | 8 | 0 | 24 | 89 | 0 | 0 | 13 | 0 | 17 | 0 | 0 | 0 | 0 | 192 | 2,888 |
| 4:15 PM | 0 | 0 | 49 | 6 | 0 | 16 | 115 | 0 | 0 | 22 | 0 | 25 | 0 | 0 | 0 | 0 | 233 | 2,961 |
| 4:20 PM | 0 | 0 | 44 | 8 | 0 | 19 | 84 | 0 | 0 | 28 | 0 | 30 | 0 | 0 | 0 | 0 | 213 | 3,016 |
| 4:25 PM | 0 | 0 | 76 | 15 | 0 | 28 | 94 | 0 | 0 | 27 | 0 | 13 | 0 | 0 | 0 | 0 | 253 | 3,079 |
| 4:30 PM | 0 | 0 | 67 | 16 | 0 | 19 | 92 | 0 | 0 | 30 | 0 | 20 | 0 | 0 | 0 | 0 | 244 | 3,090 |
| 4:35 PM | 0 | 0 | 52 | 6 | 0 | 24 | 101 | 0 | 0 | 30 | 0 | 20 | 0 | 0 | 0 | 0 | 233 | 3,113 |
| 4:40 PM | 0 | 0 | 70 | 9 | 0 | 28 | 98 | 0 | 0 | 14 | 0 | 23 | 0 | 0 | 0 | 0 | 242 | 3,148 |
| 4:45 PM | 0 | 0 | 53 | 11 | 0 | 10 | 80 | 0 | 0 | 22 | 0 | 20 | 0 | 0 | 0 | 0 | 196 | 3,158 |
| 4:50 PM | 0 | 0 | 84 | 12 | 0 | 15 | 91 | 0 | 0 | 20 | 0 | 26 | 0 | 0 | 0 | 0 | 248 | 3,207 |
| 4:55 PM | 0 | 0 | 73 | 22 | 0 | 29 | 97 | 0 | 0 | 22 | 0 | 30 | 0 | 0 | 0 | 0 | 273 | 3,196 |
| 5:00 PM | 0 | 0 | 105 | 28 | 0 | 21 | 98 | 0 | 0 | 21 | 0 | 20 | 0 | 0 | 0 | 0 | 293 | 3,177 |
| 5:05 PM | 0 | 0 | 94 | 30 | 0 | 18 | 83 | 0 | 0 | 22 | 0 | 21 | 0 | 0 | 0 | 0 | 268 |  |
| 5:10 PM | 0 | 0 | 71 | 29 | 0 | 17 | 81 | 0 | 0 | 33 | 0 | 34 | 0 | 0 | 0 | 0 | 265 |  |
| 5:15 PM | 0 | 0 | 104 | 22 | 0 | 23 | 101 | 0 | 0 | 15 | 0 | 23 | 0 | 0 | 0 | 0 | 288 |  |
| 5:20 PM | 0 | 0 | 113 | 37 | 0 | 13 | 71 | 0 | 0 | 18 | 0 | 24 | 0 | 0 | 0 | 0 | 276 |  |
| 5:25 PM | 0 | 0 | 99 | 25 | 0 | 19 | 75 | 0 | 0 | 21 | 0 | 25 | 0 | 0 | 0 | 0 | 264 |  |
| 5:30 PM | 0 | 0 | 92 | 33 | 0 | 14 | 83 | 0 | 0 | 23 | 0 | 22 | 0 | 0 | 0 | 0 | 267 |  |
| 5:35 PM | 0 | 0 | 109 | 25 | 0 | 24 | 74 | 0 | 0 | 11 | 0 | 25 | 0 | 0 | 0 | 0 | 268 |  |
| 5:40 PM | 0 | 0 | 103 | 26 | 0 | 12 | 56 | 0 | 0 | 25 | 0 | 30 | 0 | 0 | 0 | 0 | 252 |  |
| 5:45 PM | 0 | 0 | 96 | 24 | 0 | 22 | 65 | 0 | 0 | 20 | 0 | 18 | 0 | 0 | 0 | 0 | 245 |  |
| 5:50 PM | 0 | 0 | 102 | 20 | 0 | 18 | 60 | 0 | 0 | 18 | 0 | 19 | 0 | 0 | 0 | 0 | 237 |  |
| 5:55 PM | 1 | 0 | 107 | 18 | 0 | 14 | 70 | 0 | 0 | 14 | 0 | 30 | 0 | 0 | 0 | 0 | 254 |  |
| Count Total | 1 | 0 | 1,904 | 445 | 0 | 470 | 2,017 | 0 | 0 | 533 | 0 | 549 | 0 | 0 | 0 | 0 | 5,919 |  |
| Peak Hour | 0 | 0 | 1,143 | 313 | 0 | 227 | 975 | 0 | 0 | 251 | 0 | 298 | 0 | 0 | 0 | 0 | 3,207 |  |

## Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles on Crosswalk

| Interval | Heavy Vehicles |  |  |  |  | Interval Start Time | Bicycles on Roadway |  |  |  |  | Interval <br> Start Time | Pedestrians/Bicycles on Crosswalk |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |
| 4:00 PM | 11 | 2 | 8 | 0 | 21 | 4:00 PM | 0 | 0 | 0 | 0 | 0 | 4:00 PM | 0 | 0 | 0 | 0 | 0 |
| 4:05 PM | 7 | 2 | 6 | 0 | 15 | 4:05 PM | 0 | 0 | 0 | 0 | 0 | 4:05 PM | 0 | 0 | 0 | 0 | 0 |
| 4:10 PM | 4 | 0 | 4 | 0 | 8 | 4:10 PM | 0 | 0 | 0 | 0 | 0 | 4:10 PM | 0 | 0 | 1 | 0 | 1 |
| 4:15 PM | 10 | 1 | 6 | 0 | 17 | 4:15 PM | 0 | 0 | 0 | 0 | 0 | 4:15 PM | 0 | 0 | 0 | 0 | 0 |
| 4:20 PM | 6 | 0 | 5 | 0 | 11 | 4:20 PM | 0 | 0 | 0 | 0 | 0 | 4:20 PM | 0 | 0 | 1 | 0 | 1 |
| 4:25 PM | 9 | 1 | 3 | 0 | 13 | 4:25 PM | 0 | 0 | 0 | 0 | 0 | 4:25 PM | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 10 | 0 | 2 | 0 | 12 | 4:30 PM | 0 | 0 | 0 | 0 | 0 | 4:30 PM | 0 | 0 | 0 | 0 | 0 |
| 4:35 PM | 3 | 2 | 4 | 0 | 9 | 4:35 PM | 0 | 0 | 0 | 0 | 0 | 4:35 PM | 0 | 0 | 0 | 0 | 0 |
| 4:40 PM | 8 | 0 | 4 | 0 | 12 | 4:40 PM | 0 | 0 | 1 | 0 | 1 | 4:40 PM | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 7 | 0 | 5 | 0 | 12 | 4:45 PM | 0 | 0 | 0 | 0 | 0 | 4:45 PM | 0 | 0 | 0 | 0 | 0 |
| 4:50 PM | 10 | 0 | 3 | 0 | 13 | 4:50 PM | 0 | 0 | 0 | 0 | 0 | 4:50 PM | 0 | 0 | 0 | 0 | 0 |
| 4:55 PM | 7 | 0 | 5 | 0 | 12 | 4:55 PM | 0 | 0 | 1 | 0 | 1 | 4:55 PM | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 5 | 1 | 5 | 0 | 11 | 5:00 PM | 0 | 0 | 0 | 0 | 0 | 5:00 PM | 0 | 0 | 0 | 0 | 0 |
| 5:05 PM | 3 | 1 | 3 | 0 | 7 | 5:05 PM | 0 | 0 | 0 | 0 | 0 | 5:05 PM | 0 | 0 | 0 | 0 | 0 |
| 5:10 PM | 4 | 0 | 5 | 0 | 9 | 5:10 PM | 0 | 0 | 0 | 0 | 0 | 5:10 PM | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 5 | 0 | 9 | 0 | 14 | 5:15 PM | 0 | 0 | 0 | 0 | 0 | 5:15 PM | 0 | 0 | 0 | 0 | 0 |
| 5:20 PM | 2 | 1 | 4 | 0 | 7 | 5:20 PM | 0 | 0 | 0 | 0 | 0 | 5:20 PM | 0 | 0 | 0 | 0 | 0 |
| 5:25 PM | 4 | 1 | 4 | 0 | 9 | 5:25 PM | 0 | 0 | 0 | 0 | 0 | 5:25 PM | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 4 | 1 | 9 | 0 | 14 | 5:30 PM | 0 | 0 | 0 | 0 | 0 | 5:30 PM | 0 | 0 | 0 | 0 | 0 |
| 5:35 PM | 2 | 0 | 1 | 0 | 3 | 5:35 PM | 0 | 0 | 0 | 0 | 0 | 5:35 PM | 0 | 0 | 0 | 0 | 0 |
| 5:40 PM | 2 | 1 | 0 | 0 | 3 | 5:40 PM | 0 | 0 | 0 | 0 | 0 | 5:40 PM | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 3 | 1 | 4 | 0 | 8 | 5:45 PM | 0 | 0 | 0 | 0 | 0 | 5:45 PM | 0 | 0 | 0 | 0 | 0 |
| 5:50 PM | 7 | 1 | 3 | 0 | 11 | 5:50 PM | 0 | 0 | 0 | 0 | 0 | 5:50 PM | 0 | 0 | 0 | 0 | 0 |
| 5:55 PM | 1 | 0 | 1 | 0 | 2 | 5:55 PM | 0 | 0 | 0 | 0 | 0 | 5:55 PM | 0 | 0 | 0 | 0 | 0 |
| Count Total | 134 | 16 | 103 | 0 | 253 | Count Total | 0 | 0 | 2 | 0 | 2 | Count Total | 0 | 0 | 2 | 0 | 2 |
| Peak Hour | 51 | 7 | 52 | 0 | 110 | Peak Hour | 0 | 0 | 1 | 0 | 1 | Peak Hour | 0 | 0 | 0 | 0 | 0 |



Note: Total study counts contained in parentheses.

|  | HV\% | PHF |
| :---: | :---: | :---: |
| EB | $0.0 \%$ | 0.00 |
| WB | $2.2 \%$ | 0.77 |
| NB | $1.6 \%$ | 0.92 |
| SB | $1.7 \%$ | 0.92 |
| All | $1.7 \%$ | 0.94 |

Traffic Counts - Motorized Vehicles

| Interval Start Time | INDUSTRIAL WAY EAST Eastbound |  |  |  | INDUSTRIAL WAY EAST <br> Westbound |  |  |  | SE 362ND DR <br> Northbound |  |  |  | SE 362ND DR Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 7 | 0 | 0 | 42 | 2 | 0 | 1 | 38 | 0 | 93 | 933 |
| 4:05 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 5 | 0 | 0 | 30 | 2 | 0 | 5 | 30 | 0 | 74 | 929 |
| 4:10 PM | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 5 | 0 | 0 | 21 | 1 | 0 | 1 | 38 | 0 | 69 | 933 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 35 | 3 | 0 | 2 | 43 | 0 | 93 | 929 |
| 4:20 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 26 | 4 | 0 | 0 | 41 | 0 | 72 | 898 |
| 4:25 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 4 | 0 | 0 | 19 | 2 | 0 | 1 | 26 | 0 | 54 | 896 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 11 | 0 | 0 | 34 | 1 | 0 | 2 | 44 | 0 | 97 | 902 |
| 4:35 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 5 | 0 | 0 | 21 | 6 | 0 | 2 | 45 | 0 | 81 | 876 |
| 4:40 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 4 | 0 | 0 | 31 | 2 | 0 | 1 | 30 | 0 | 70 | 862 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 5 | 0 | 0 | 34 | 3 | 0 | 5 | 29 | 0 | 80 | 863 |
| 4:50 PM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 2 | 0 | 0 | 25 | 0 | 0 | 1 | 36 | 0 | 69 | 854 |
| 4:55 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 28 | 3 | 0 | 2 | 46 | 0 | 81 | 847 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 4 | 0 | 0 | 44 | 2 | 0 | 0 | 38 | 0 | 89 | 831 |
| 5:05 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 27 | 3 | 0 | 0 | 44 | 0 | 78 |  |
| 5:10 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 22 | 1 | 0 | 2 | 36 | 0 | 65 |  |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 28 | 2 | 0 | 1 | 28 | 0 | 62 |  |
| 5:20 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 25 | 1 | 0 | 1 | 40 | 0 | 70 |  |
| 5:25 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 17 | 1 | 0 | 0 | 39 | 0 | 60 |  |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 33 | 1 | 0 | 0 | 33 | 0 | 71 |  |
| 5:35 PM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 29 | 2 | 0 | 1 | 30 | 0 | 67 |  |
| 5:40 PM | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 24 | 2 | 0 | 1 | 40 | 0 | 71 |  |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 27 | 2 | 0 | 1 | 37 | 0 | 71 |  |
| 5:50 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 30 | 3 | 0 | 0 | 28 | 0 | 62 |  |
| 5:55 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 26 | 5 | 0 | 0 | 33 | 0 | 65 |  |
| Count Total | 0 | 0 | 0 | 0 | 0 | 56 | 0 | 74 | 0 | 0 | 678 | 54 | 0 | 30 | 872 | 0 | 1,764 |  |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 34 | 0 | 55 | 0 | 0 | 346 | 29 | 0 | 23 | 446 | 0 | 933 |  |

## Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles on Crosswalk

| Interval | Heavy Vehicles |  |  |  |  | Interval Start Time | Bicycles on Roadway |  |  |  |  | Interval <br> Start Time | Pedestrians/Bicycles on Crosswalk |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |
| 4:00 PM | 0 | 3 | 0 | 2 | 5 | 4:00 PM | 0 | 0 | 0 | 0 | 0 | 4:00 PM | 0 | 0 | 1 | 0 | 1 |
| 4:05 PM | 0 | 1 | 0 | 0 | 1 | 4:05 PM | 0 | 0 | 0 | 0 | 0 | 4:05 PM | 0 | 0 | 0 | 0 | 0 |
| 4:10 PM | 0 | 1 | 0 | 0 | 1 | 4:10 PM | 0 | 0 | 0 | 0 | 0 | 4:10 PM | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 1 | 0 | 1 | 2 | 4:15 PM | 0 | 0 | 0 | 0 | 0 | 4:15 PM | 0 | 0 | 0 | 0 | 0 |
| 4:20 PM | 0 | 0 | 0 | 1 | 1 | 4:20 PM | 0 | 0 | 0 | 0 | 0 | 4:20 PM | 0 | 0 | 0 | 0 | 0 |
| 4:25 PM | 0 | 0 | 1 | 0 | 1 | 4:25 PM | 0 | 0 | 0 | 0 | 0 | 4:25 PM | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 1 | 1 | 2 | 4:30 PM | 0 | 0 | 0 | 0 | 0 | 4:30 PM | 0 | 0 | 0 | 0 | 0 |
| 4:35 PM | 0 | 0 | 0 | 0 | 0 | 4:35 PM | 0 | 0 | 0 | 0 | 0 | 4:35 PM | 0 | 0 | 0 | 0 | 0 |
| 4:40 PM | 0 | 0 | 0 | 0 | 0 | 4:40 PM | 0 | 0 | 0 | 0 | 0 | 4:40 PM | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 2 | 2 | 4:45 PM | 0 | 0 | 0 | 0 | 0 | 4:45 PM | 0 | 0 | 0 | 0 | 0 |
| 4:50 PM | 0 | 0 | 0 | 1 | 1 | 4:50 PM | 0 | 0 | 0 | 0 | 0 | 4:50 PM | 0 | 0 | 0 | 0 | 0 |
| 4:55 PM | 0 | 0 | 0 | 0 | 0 | 4:55 PM | 0 | 0 | 0 | 0 | 0 | 4:55 PM | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 2 | 0 | 0 | 2 | 5:00 PM | 0 | 0 | 0 | 0 | 0 | 5:00 PM | 0 | 0 | 0 | 0 | 0 |
| 5:05 PM | 0 | 0 | 0 | 1 | 1 | 5:05 PM | 0 | 0 | 0 | 0 | 0 | 5:05 PM | 0 | 0 | 0 | 0 | 0 |
| 5:10 PM | 0 | 0 | 0 | 2 | 2 | 5:10 PM | 0 | 0 | 0 | 0 | 0 | 5:10 PM | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 5:15 PM | 0 | 0 | 0 | 0 | 0 | 5:15 PM | 0 | 0 | 0 | 0 | 0 |
| 5:20 PM | 0 | 0 | 1 | 0 | 1 | 5:20 PM | 0 | 0 | 0 | 0 | 0 | 5:20 PM | 0 | 0 | 0 | 0 | 0 |
| 5:25 PM | 0 | 1 | 0 | 0 | 1 | 5:25 PM | 0 | 0 | 0 | 0 | 0 | 5:25 PM | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 1 | 1 | 5:30 PM | 0 | 0 | 0 | 0 | 0 | 5:30 PM | 0 | 0 | 0 | 0 | 0 |
| 5:35 PM | 0 | 0 | 0 | 0 | 0 | 5:35 PM | 0 | 0 | 0 | 0 | 0 | 5:35 PM | 0 | 0 | 0 | 0 | 0 |
| 5:40 PM | 0 | 0 | 0 | 0 | 0 | 5:40 PM | 0 | 0 | 0 | 0 | 0 | 5:40 PM | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 2 | 0 | 0 | 2 | 5:45 PM | 0 | 0 | 0 | 0 | 0 | 5:45 PM | 0 | 0 | 0 | 0 | 0 |
| 5:50 PM | 0 | 0 | 0 | 1 | 1 | 5:50 PM | 0 | 0 | 0 | 0 | 0 | 5:50 PM | 0 | 0 | 0 | 0 | 0 |
| 5:55 PM | 0 | 1 | 0 | 1 | 2 | 5:55 PM | 0 | 0 | 0 | 0 | 0 | 5:55 PM | 0 | 0 | 0 | 0 | 0 |
| Count Total | 0 | 12 | 3 | 14 | 29 | Count Total | 0 | 0 | 0 | 0 | 0 | Count Total | 0 | 0 | 1 | 0 | 1 |
| Peak Hour | 0 | 6 | 2 | 8 | 16 | Peak Hour | 0 | 0 | 0 | 0 | 0 | Peak Hour | 0 | 0 | 1 | 0 | 1 |



Note: Total study counts contained in parentheses.

|  | HV\% | PHF |
| :--- | :---: | :---: |
| EB | $0.9 \%$ | 0.85 |
| WB | $0.0 \%$ | 0.00 |
| NB | $1.7 \%$ | 0.92 |
| SB | $2.7 \%$ | 0.94 |
| All | $2.0 \%$ | 0.92 |

Traffic Counts - Motorized Vehicles

| Interval Start Time | INDUSTRIAL WAY WEST <br> Eastbound |  |  |  | INDUSTRIAL WAY WESTWestbound |  |  |  | SE 362ND DR Northbound |  |  |  | SE 362ND DR Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 4:00 PM | 0 | 15 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 8 | 25 | 0 | 0 | 0 | 31 | 4 | 94 | 1,029 |
| 4:05 PM | 0 | 14 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 8 | 27 | 0 | 0 | 0 | 39 | 2 | 104 | 1,033 |
| 4:10 PM | 0 | 6 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 3 | 11 | 0 | 0 | 0 | 34 | 3 | 65 | 1,020 |
| 4:15 PM | 0 | 14 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 1 | 24 | 0 | 0 | 0 | 35 | 4 | 92 | 1,053 |
| 4:20 PM | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 5 | 26 | 0 | 0 | 0 | 45 | 3 | 87 | 1,033 |
| 4:25 PM | 0 | 4 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 4 | 24 | 0 | 0 | 0 | 36 | 2 | 81 | 1,036 |
| 4:30 PM | 0 | 8 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 3 | 24 | 0 | 0 | 0 | 32 | 1 | 79 | 1,025 |
| 4:35 PM | 0 | 8 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 3 | 20 | 0 | 0 | 0 | 42 | 6 | 91 | 1,037 |
| 4:40 PM | 0 | 4 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 7 | 25 | 0 | 0 | 0 | 34 | 4 | 86 | 1,026 |
| 4:45 PM | 0 | 10 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 3 | 27 | 0 | 0 | 0 | 31 | 1 | 80 | 1,024 |
| 4:50 PM | 0 | 7 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 5 | 22 | 0 | 0 | 0 | 42 | 3 | 88 | 1,027 |
| 4:55 PM | 0 | 6 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 4 | 24 | 0 | 0 | 0 | 32 | 5 | 82 | 1,016 |
| 5:00 PM | 0 | 11 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 4 | 29 | 0 | 0 | 0 | 40 | 2 | 98 | 1,015 |
| 5:05 PM | 0 | 6 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 7 | 24 | 0 | 0 | 0 | 42 | 1 | 91 |  |
| 5:10 PM | 0 | 10 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 8 | 21 | 0 | 0 | 0 | 44 | 1 | 98 |  |
| 5:15 PM | 0 | 5 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 4 | 19 | 0 | 0 | 0 | 30 | 0 | 72 |  |
| 5:20 PM | 0 | 6 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | 5 | 21 | 0 | 0 | 0 | 37 | 3 | 90 |  |
| 5:25 PM | 0 | 5 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 4 | 18 | 0 | 0 | 0 | 36 | 3 | 70 |  |
| 5:30 PM | 0 | 6 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 5 | 27 | 0 | 0 | 0 | 39 | 0 | 91 |  |
| 5:35 PM | 0 | 7 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 6 | 17 | 0 | 0 | 0 | 35 | 1 | 80 |  |
| 5:40 PM | 0 | 5 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 5 | 28 | 0 | 0 | 0 | 34 | 1 | 84 |  |
| 5:45 PM | 0 | 9 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 5 | 17 | 0 | 0 | 0 | 44 | 0 | 83 |  |
| 5:50 PM | 0 | 4 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 3 | 25 | 0 | 0 | 0 | 33 | 2 | 77 |  |
| 5:55 PM | 0 | 8 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 6 | 25 | 0 | 0 | 0 | 30 | 3 | 81 |  |
| Count Total | 0 | 182 | 0 | 264 | 0 | 0 | 0 | 0 | 0 | 116 | 550 | 0 | 0 | 0 | 877 | 55 | 2,044 |  |
| Peak Hour | 0 | 92 | 0 | 129 | 0 | 0 | 0 | 0 | 0 | 54 | 290 | 0 | 0 | 0 | 455 | 33 | 1,053 |  |

## Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles on Crosswalk

| Interval | Heavy Vehicles |  |  |  |  | Interval Start Time | Bicycles on Roadway |  |  |  |  | Interval <br> Start Time | Pedestrians/Bicycles on Crosswalk |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |
| 4:00 PM | 0 | 3 | 0 | 2 | 5 | 4:00 PM | 0 | 0 | 0 | 0 | 0 | 4:00 PM | 0 | 0 | 2 | 0 | 2 |
| 4:05 PM | 1 | 0 | 0 | 3 | 4 | 4:05 PM | 0 | 0 | 0 | 0 | 0 | 4:05 PM | 0 | 0 | 2 | 1 | 3 |
| 4:10 PM | 0 | 0 | 0 | 0 | 0 | 4:10 PM | 0 | 0 | 0 | 0 | 0 | 4:10 PM | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 2 | 0 | 0 | 2 | 4:15 PM | 0 | 1 | 0 | 0 | 1 | 4:15 PM | 0 | 0 | 0 | 0 | 0 |
| 4:20 PM | 0 | 0 | 0 | 2 | 2 | 4:20 PM | 0 | 0 | 0 | 0 | 0 | 4:20 PM | 0 | 0 | 5 | 0 | 5 |
| 4:25 PM | 0 | 0 | 0 | 3 | 3 | 4:25 PM | 0 | 0 | 0 | 0 | 0 | 4:25 PM | 0 | 0 | 2 | 0 | 2 |
| 4:30 PM | 0 | 0 | 0 | 1 | 1 | 4:30 PM | 1 | 0 | 0 | 0 | 1 | 4:30 PM | 0 | 0 | 0 | 0 | 0 |
| 4:35 PM | 1 | 1 | 0 | 1 | 3 | 4:35 PM | 0 | 0 | 0 | 0 | 0 | 4:35 PM | 0 | 0 | 0 | 0 | 0 |
| 4:40 PM | 1 | 0 | 0 | 1 | 2 | 4:40 PM | 0 | 0 | 0 | 0 | 0 | 4:40 PM | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 1 | 1 | 4:45 PM | 0 | 0 | 0 | 0 | 0 | 4:45 PM | 0 | 0 | 0 | 0 | 0 |
| 4:50 PM | 0 | 1 | 0 | 0 | 1 | 4:50 PM | 0 | 0 | 0 | 0 | 0 | 4:50 PM | 0 | 0 | 0 | 0 | 0 |
| 4:55 PM | 0 | 0 | 0 | 0 | 0 | 4:55 PM | 0 | 0 | 0 | 0 | 0 | 4:55 PM | 0 | 0 | 1 | 0 | 1 |
| 5:00 PM | 0 | 1 | 0 | 1 | 2 | 5:00 PM | 0 | 0 | 0 | 0 | 0 | 5:00 PM | 0 | 0 | 0 | 0 | 0 |
| 5:05 PM | 0 | 1 | 0 | 1 | 2 | 5:05 PM | 0 | 0 | 0 | 0 | 0 | 5:05 PM | 0 | 0 | 1 | 0 | 1 |
| 5:10 PM | 0 | 0 | 0 | 2 | 2 | 5:10 PM | 0 | 0 | 0 | 0 | 0 | 5:10 PM | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 1 | 0 | 0 | 1 | 5:15 PM | 0 | 0 | 0 | 0 | 0 | 5:15 PM | 0 | 0 | 1 | 0 | 1 |
| 5:20 PM | 1 | 0 | 0 | 0 | 1 | 5:20 PM | 0 | 0 | 0 | 0 | 0 | 5:20 PM | 0 | 0 | 0 | 0 | 0 |
| 5:25 PM | 0 | 0 | 0 | 0 | 0 | 5:25 PM | 0 | 0 | 0 | 0 | 0 | 5:25 PM | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 2 | 0 | 2 | 4 | 5:30 PM | 0 | 0 | 0 | 0 | 0 | 5:30 PM | 0 | 0 | 0 | 0 | 0 |
| 5:35 PM | 1 | 0 | 0 | 0 | 1 | 5:35 PM | 1 | 0 | 0 | 0 | 1 | 5:35 PM | 0 | 0 | 0 | 0 | 0 |
| 5:40 PM | 0 | 1 | 0 | 2 | 3 | 5:40 PM | 0 | 0 | 0 | 0 | 0 | 5:40 PM | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 1 | 0 | 0 | 1 | 5:45 PM | 0 | 0 | 0 | 0 | 0 | 5:45 PM | 0 | 0 | 0 | 0 | 0 |
| 5:50 PM | 0 | 1 | 0 | 1 | 2 | 5:50 PM | 0 | 0 | 0 | 0 | 0 | 5:50 PM | 0 | 0 | 2 | 0 | 2 |
| 5:55 PM | 1 | 0 | 0 | 2 | 3 | 5:55 PM | 0 | 0 | 0 | 0 | 0 | 5:55 PM | 0 | 0 | 2 | 0 | 2 |
| Count Total | 6 | 15 | 0 | 25 | 46 | Count Total | 2 | 1 | 0 | 0 | 3 | Count Total | 0 | 0 | 18 | 1 | 19 |
| Peak Hour | 2 | 6 | 0 | 13 | 21 | Peak Hour | 1 | 1 | 0 | 0 | 2 | Peak Hour | 0 | 0 | 9 | 0 | 9 |

ODOT ADT Volumes at Permanent Count Station 03-006 (Rhododendron)

| Year | August | July | Adjust | High/Low |
| :---: | :---: | :---: | :---: | :---: |
| 2021 | 12988 | 14387 | 1.107715 | High |
| 2020 | 13411 | 14166 | 1.056297 |  |
| 2019 | 13497 | 13605 | 1.008002 | Low |
| 2018 | 13089 | 13868 | 1.059516 |  |
| 2017 | 13623 | 13874 | 1.018425 |  |
|  |  |  |  |  |
| Sum of 3 | 40123 | 41908 | 1.044488 |  |
| Average of 3 | 13374.33 | 13969.33 |  |  |

## Calculated Adjustment 595 vehicles per day

| SEASONAL TREND TABLE (Updated: 7/20/2021) ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Seasonal TrendPeak PeriodFactor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TREND | 1-Jan | 15-Jan | 1-Jun | 15-Jun | 1-Jul | 15-Jul | 1-Aug | 15-Aug | 1-Sep | 15-Sep | 1-Oct | 15-Oct | 1-Nov | 15-Nov | 1-Dec | 15-Dec |  |
| INTERSTATE URBANIZED | 1.0672 | 1.0684 | 0.9615 | 0.9463 | 0.9517 | 0.9571 | 0.9551 | 0.9531 | 0.9674 | 0.9816 | 0.9850 | 0.9884 | 1.0045 | 1.0206 | 1.0322 | 1.043 | 0.9463 |
| INTERSTATE NONURBANIZED | 1.2426 | 1.2883 | 0.9005 | 0.8506 | 0.8322 | 0.8139 | 0.8221 | 0.8302 | 0.8719 | 0.9135 | 0.9441 | 0.9747 | 1.0178 | 1.0608 | 1.1123 | 1.163 | 0.8139 |
| COMMUTER | 1.0850 | 1.0875 | 0.9503 | 0.9355 | 0.9470 | 0.9585 | 0.9509 | 0.9433 | 0.9528 | 0.9623 | 0.9614 | 0.9604 | 0.9938 | 1.0272 | 1.0474 | 1.0676 | 0.9355 |
| COASTAL DESTINATION | 1.1885 | 1.1712 | 0.9347 | 0.8972 | 0.8612 | 0.8252 | 0.8205 | 0.8159 | 0.8686 | 0.9214 | 0.9689 | 1.0164 | 1.0660 | 1.1156 | 1.1580 | 1.2005 | 0.8159 |
| COASTAL DESTINATION ROUTE | 1.3445 | 1.3248 | 0.8941 | 0.8409 | 0.7820 | 0.7231 | 0.7218 | 0.7205 | 0.8016 | 0.8827 | 0.9669 | 1.0511 | 1.1133 | 1.1754 | 1.2480 | 1.3206 | 0.7205 |
| AGRICULTURE | 1.4583 | 1.4827 | 0.8579 | 0.8146 | 0.8058 | 0.7970 | 0.7922 | 0.7873 | 0.7772 | 0.7670 | 0.8288 | 0.8905 | 0.9947 | 1.0989 | 1.2462 | 1.3934 | 0.7670 |
| RECREATIONAL SUMMER | 1.5848 | 1.6474 | 0.8256 | 0.7484 | 0.7018 | 0.6552 | 0.6708 | 0.6864 | 0.7393 | 0.7922 | 0.8898 | 0.9874 | 1.1242 | 1.2610 | 1.3965 | 1.5320 | 0.6552 |
| RECREATIONAL SUMMER WINTER | 0.8736 | 0.8525 | 0.9760 | 0.8821 | 0.8005 | 0.7190 | 0.7305 | 0.7420 | 0.8897 | 1.0374 | 1.2010 | 1.3645 | 1.5212 | 1.6778 | 1.3812 | 1.0847 | 0.7190 |
| RECREATIONAL WINTER | 0.6997 | 0.6389 | 1.2832 | 1.1625 | 0.9985 | 0.8344 | 0.8600 | 0.8857 | 1.0560 | 1.2262 | 1.4100 | 1.5937 | 1.8758 | 2.1580 | 1.5328 | 0.9076 | 0.6389 |
| SUMMER | 1.2151 | 1.2357 | 0.8976 | 0.8615 | 0.8457 | 0.8299 | 0.8354 | 0.8410 | 0.8743 | 0.9077 | 0.9357 | 0.9638 | 1.0273 | 1.0908 | 1.1322 | 1.1737 | 0.8299 |
| SUMMER < 2500 | 1.3035 | 1.3186 | 0.8720 | 0.8387 | 0.8237 | 0.8086 | 0.8229 | 0.8373 | 0.8616 | 0.8859 | 0.9233 | 0.9607 | 1.0428 | 1.1249 | 1.2016 | 1.2783 | 0.8086 |

[^0]${ }^{1}$ Seasonal Trend Table: The 2020 table is based on 2019 values due to the irregularity caused by the Covid epidemic shutdown during the 2020 count year.
-0.00543 (Change per day)
$=$ August 11 value / June 15 peak value



## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.5 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  | 1 | 个 |
| Traffic Vol, veh/h | 26 | 15 | 293 | 45 | 36 | 121 |
| Future Vol, veh/h | 26 | 15 | 293 | 45 | 36 | 121 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 150 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 15 | 15 | 6 | 6 | 6 | 6 |
| Mvmt Flow | 29 | 17 | 326 | 50 | 40 | 134 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 565 | 351 | 0 | 0 | 376 | 0 |
| Stage 1 | 351 | - | - | - | - | - |
| Stage 2 | 214 | - | - | - | - | - |
| Critical Hdwy | 6.55 | 6.35 | - | - | 4.16 | - |
| Critical Hdwy Stg 1 | 5.55 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.55 | - | - | - | - | - |
| Follow-up Hdwy | 3.635 | 3.435 | - | - | 2.254 | - |
| Pot Cap-1 Maneuver | 465 | 664 | - | - | 1161 | - |
| Stage 1 | 685 | - | - | - | - | - |
| Stage 2 | 792 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 449 | 664 | - | - | 1161 | - |
| Mov Cap-2 Maneuver | 449 | - | - | - | - | - |
| Stage 1 | 685 | - | - | - | - | - |
| Stage 2 | 765 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 12.8 |  | 0 |  | 1.9 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 509 | 1161 | - |
| HCM Lane V/C Ratio |  | - | - | 0.09 | 0.034 | - |
| HCM Control Delay (s) |  | - | - | 12.8 | 8.2 | - |
| HCM Lane LOS |  | - | - | B | A | - |
| HCM 95th \%tile Q(veh) |  | - | - | 0.3 | 0.1 | - |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh $\quad 10.5$ |  |
| Intersection LOS | B |


| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | M |  |  | $\uparrow$ | $\hat{1}$ |  |
| Traffic Vol, veh/h | 58 | 36 | 56 | 293 | 90 | 37 |
| Future Vol, veh/h | 58 | 36 | 56 | 293 | 90 | 37 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles, \% | 14 | 14 | 5 | 5 | 9 | 9 |
| Mvmt Flow | 64 | 40 | 62 | 326 | 100 | 41 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 0 |
| Approach | EB |  | NB |  | SB |  |
| Opposing Approach |  |  | SB |  | NB |  |
| Opposing Lanes | 0 |  | 1 |  | 1 |  |
| Conflicting Approach Left | SB |  | EB |  |  |  |
| Conflicting Lanes Left | 1 |  | 1 |  | 0 |  |
| Conflicting Approach Right | NB |  |  |  | EB |  |
| Conflicting Lanes Right | 1 |  | 0 |  | 1 |  |
| HCM Control Delay | 9.2 |  | 11.5 |  | 8.6 |  |
| HCM LOS | A |  | B |  | A |  |


| Lane | NBLn1 | EBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: |
| Vol Left, \% | $16 \%$ | $62 \%$ | $0 \%$ |
| Vol Thru, \% | $84 \%$ | $0 \%$ | $71 \%$ |
| Vol Right, \% | $0 \%$ | $38 \%$ | $29 \%$ |
| Sign Control | Stop | Stop | Stop |
| Traffic Vol by Lane | 349 | 94 | 127 |
| LT Vol | 56 | 58 | 0 |
| Through Vol | 293 | 0 | 90 |
| RT Vol | 0 | 36 | 37 |
| Lane Flow Rate | 388 | 104 | 141 |
| Geometry Grp | 1 | 1 | 1 |
| Degree of Util (X) | 0.48 | 0.151 | 0.179 |
| Departure Headway (Hd) | 4.452 | 5.219 | 4.575 |
| Convergence, Y/N | Yes | Yes | Yes |
| Cap | 810 | 686 | 783 |
| Service Time | 2.476 | 3.261 | 2.606 |
| HCM Lane V/C Ratio | 0.479 | 0.152 | 0.18 |
| HCM Control Delay | 11.5 | 9.2 | 8.6 |
| HCM Lane LOS | B | A | A |
| HCM 95th-tile Q | 2.6 | 0.5 | 0.6 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 0 | 1 | 348 | 0 | 3 | 123 |
| Future Vol, veh/h | 0 | 1 | 348 | 0 | 3 | 123 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 20 | 20 | 5 | 5 | 9 | 9 |
| Mvmt Flow | 0 | 1 | 387 | 0 | 3 | 137 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 530 | 387 | 0 | 0 | 387 | 0 |
| Stage 1 | 387 | - | - | - | - | - |
| Stage 2 | 143 | - | - | - | - | - |
| Critical Hdwy | 6.6 | 6.4 | - | - | 4.19 | - |
| Critical Hdwy Stg 1 | 5.6 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.6 | - | - | - | - | - |
| Follow-up Hdwy | 3.68 | 3.48 | - | - | 2.281 | - |
| Pot Cap-1 Maneuver | 480 | 623 | - | - | 1134 | - |
| Stage 1 | 649 | - | - | - | - | - |
| Stage 2 | 842 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 479 | 623 | - | - | 1134 | - |
| Mov Cap-2 Maneuver | 479 | - | - | - | - | - |
| Stage 1 | 649 | - | - | - | - | - |
| Stage 2 | 839 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 10.8 |  | 0 |  | 0.2 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 623 | 1134 | - |
| HCM Lane V/C Ratio |  | - | - | 0.002 | 0.003 | - |
| HCM Control Delay (s) |  | - | - | 10.8 | 8.2 | 0 |
| HCM Lane LOS |  | - | - | B | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0 | 0 | - |

[^1] MTA



## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.6 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  | 7 | 4 |
| Traffic Vol, veh/h | 34 | 55 | 346 | 29 | 23 | 446 |
| Future Vol, veh/h | 34 | 55 | 346 | 29 | 23 | 446 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 150 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 36 | 59 | 368 | 31 | 24 | 474 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 906 | 384 | 0 | 0 | 399 | 0 |
| Stage 1 | 384 | - | - | - | - | - |
| Stage 2 | 522 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 307 | 664 | - | - | 1160 | - |
| Stage 1 | 688 | - | - | - | - | - |
| Stage 2 | 595 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 301 | 664 | - | - | 1160 | - |
| Mov Cap-2 Maneuver | 301 | - | - | - | - | - |
| Stage 1 | 688 | - | - | - | - | - |
| Stage 2 | 583 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 15 |  | 0 |  | 0.4 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 455 | 1160 | - |
| HCM Lane V/C Ratio |  | - | - | 0.208 | 0.021 | - |
| HCM Control Delay (s) |  | - | - | 15 | 8.2 | - |
| HCM Lane LOS |  | - | - | C | A | - |
| HCM 95th \%tile Q(veh) |  | - | - | 0.8 | 0.1 | - |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh $\quad 18.6$ |  |
| Intersection LOS | C |


| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | 9 |  |  | $\uparrow$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 92 | 129 | 54 | 290 | 455 | 33 |
| Future Vol, veh/h | 92 | 129 | 54 | 290 | 455 | 33 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 3 | 3 |
| Mvmt Flow | 100 | 140 | 59 | 315 | 495 | 36 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 0 |
| Approach | EB |  | NB |  | SB |  |
| Opposing Approach |  |  | SB | NB |  |  |
| Opposing Lanes | 0 |  | 1 | 1 |  |  |
| Conflicting Approach Left | SB |  | EB |  |  |  |
| Conflicting Lanes Left | 1 |  | 1 |  | 0 |  |
| Conflicting Approach Right | NB |  |  |  | EB |  |
| Conflicting Lanes Right | 1 | 0 | 1 |  |  |  |
| HCM Control Delay | 12.8 | 15.5 | 23.5 |  |  |  |
| HCM LOS | B | C |  | C |  |  |


| Lane | NBLn1 | EBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: |
| Vol Left, \% | $16 \%$ | $42 \%$ | $0 \%$ |
| Vol Thru, \% | $84 \%$ | $0 \%$ | $93 \%$ |
| Vol Right, \% | $0 \%$ | $58 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop |
| Traffic Vol by Lane | 544 | 221 | 488 |
| LT Vol | 54 | 92 | 0 |
| Through Vol | 090 | 0 | 455 |
| RT Vol | 0 | 129 | 33 |
| Lane Flow Rate | 374 | 240 | 530 |
| Geometry Grp | 1 | 1 | 1 |
| Degree of Util (X) | 0.568 | 0.395 | 0.769 |
| Departure Headway (Hd) | 5.467 | 5.919 | 5.216 |
| Convergence, Y/N | Yes | Yes | Yes |
| Cap | 658 | 605 | 695 |
| Service Time | 3.515 | 3.975 | 3.258 |
| HCM Lane V/C Ratio | 0.568 | 0.397 | 0.763 |
| HCM Control Delay | 15.5 | 12.8 | 23.5 |
| HCM Lane LOS | C | B | C |
| HCM 95th-tile Q | 3.6 | 1.9 | 7.3 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | M |  | F |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 1 | 3 | 341 | 0 | 2 | 582 |
| Future Vol, veh/h | 1 | 3 | 341 | 0 | 2 | 582 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 20 | 20 | 2 | 20 | 20 | 3 |
| Mvmt Flow | 1 | 3 | 371 | 0 | 2 | 633 |



## Trip Generation Calculation Worksheet

Land Use Description: Specialty Trade Contractor
ITE Land Use Code: 180
Independent Variable: Gross Floor Area
Quantity: 30 Employees

## Summary of ITE Trip Generation Data

AM Peak Hour of Adjacent Street Traffic
Trip Rate: $\quad 0.61$ trips per ksf
Directional Distribution: 74\% Entering 26\% Exiting

PM Peak Hour of Adjacent Street Traffic
Trip Rate: $\quad 0.72$ trips per ksf
Directional Distribution: 32\% Entering 68\% Exiting

Total Weekday Traffic
$\begin{array}{lrl}\text { Trip Rate: } \quad 3.63 \text { trips per ksf } & \\ \text { Directional Distribution: } & 50 \% \text { Entering } & 50 \% \text { Exiting }\end{array}$

## Site Trip Generation Calculations

30 Employee Specialty Trade Contractor

|  | Entering | Exiting | Total |
| :--- | :---: | :---: | :---: |
| AM Peak Hour | 13 | 5 | 18 |
| PM Peak Hour | 7 | 15 | 22 |
| Weekday | 54 | 54 | 108 |

** Future Volume calculated based on 2017-2019 counts due to covid.

| Site id | HWY | MP | DIR | HS | Description | 2017 | 2018 | 2019 | 2020 | 2040** | RSQ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 26003 | 026 | 14.36 | 1 |  | Southeast of Powell Valley Rd [0.18 mile] \{Gresham ATR, Sta. 26-003\} |  | 33400 |  |  | 43300 | MODEL |
| 1774 | 026 | 14.80 | 1 |  | mile] |  | 28500 |  |  | 36500 | MODEL |
| 1775 | 026 | 18.30 | 1 |  | Northwest of S.E. Haley Road [0.05 mile] |  | 25600 |  |  | 37600 | MODEL |
| 1776 | 026 | 19.24 | 1 |  | Northwest of Clackamas Boring Highway (OR212) [0.30 mile] |  | 25500 |  |  | 37400 | MODEL |
| 22590 | 026 | 20.60 | 1 |  | Northwest of S.E. Kelso Road [0.50 mile] |  | 30300 |  |  | 44000 | MODEL |
| 1777 | 026 | 21.40 | 1 |  | Southeast of Southeast Kelso Road [0.30 mile] |  | 30300 |  |  | 43000 | MODEL |
| 1778 | 026 | 22.72 | 1 |  | Northwest of S.E. 362nd Drive, west city limits Sandy [ 0.02 mile] |  | 33700 |  |  | 47900 | MODEL |
| 1779 | 026 | 23.85 | 1 |  | West of Bluff Road [0.02 mile] |  | 33300 |  |  | 47700 | MODEL |
| 1780 | 026 | 23.89 | 1 |  | East of Bluff Road [0.02 mile] |  | 15700 |  |  | 22700 | MODEL |
| 1781 | 026 | 24.02 | 1 |  | West of Beers Avenue [0.02 mile] |  | 16200 |  |  | 23500 | MODEL |
| 1782 | 026 | 24.35 | 1 |  | West of Meining Ave (OR211) [0.05 mile] |  | 16000 |  |  | 23700 | MODEL |
| 1783 | 026 | 24.42 | 1 |  | East of Meining Ave (OR211) [0.02 mile] |  | 12400 |  |  | 17900 | MODEL |
| 1784 | 026 | 24.59 | 1 |  | West of Ten Eyck Road [0.02 mile] |  | 12500 |  |  | 18100 | MODEL |
| 1785 | 026 | 23.89 | 2 |  | East of Bluff Road [0.02 mile] |  | 16600 |  |  | 23600 | MODEL |
| 1786 | 026 | 24.04 | 2 |  | West of Beers Avenue [0.02 mile] |  | 18300 |  |  | 26000 | MODEL |
| 1787 | 026 | 24.36 | 2 |  | West of Meining Ave (OR211) [0.02 mile] |  | 15900 |  |  | 23000 | MODEL |
| 1788 | 026 | 24.40 | 2 |  | East of Meining Ave (OR211) [0.02 mile] |  | 13700 |  |  | 19400 | MODEL |
| 1789 | 026 | 24.61 | 2 |  | West of Ten Eyck Road [0.02 mile] |  | 12600 |  |  | 17900 | MODEL |
| 1790 | 026 | 25.10 | 1 |  | West of Langensand Road [0.02 mile] |  | 20700 |  |  | 29600 | MODEL |
| 1791 | 026 | 25.66 | 1 |  | East of Vista Loop Drive [0.10 mile] |  | 23500 |  |  | 33300 | MODEL |
| 1792 | 026 | 26.76 | 1 |  | West of S.E. Firwood Road [0.10 mile] |  | 19000 |  |  | 26900 | MODEL |
| 1793 | 026 | 26.93 | 1 |  | East of S.E. Firwood Road [0.07 mile] |  | 17800 |  |  | 25600 | MODEL |
| 1794 | 026 | 29.66 | 1 |  | West of Wagoneer Loop Drive (East Jct.) [0.23 mile] |  | 16500 |  |  | 23700 | MODEL |
| 1795 | 026 | 34.87 | 1 |  | West of E. Sleepy Hollow Drive [0.10 mile] |  | 15000 |  |  | 21800 | MODEL |




## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.5 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  | 1 | 4 |
| Traffic Vol, veh/h | 27 | 15 | 307 | 46 | 37 | 130 |
| Future Vol, veh/h | 27 | 15 | 307 | 46 | 37 | 130 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 150 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 15 | 15 | 6 | 6 | 6 | 6 |
| Mvmt Flow | 30 | 17 | 341 | 51 | 41 | 144 |


| Major/Minor | Minor1 | Major1 |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 593 | 367 |  | 0 | 392 | 0 |
| Stage 1 | 367 |  | - | - | - |  |
| Stage 2 | 226 |  | - | - | - |  |
| Critical Hdwy | 6.55 | 6.35 | - | - | 4.16 |  |
| Critical Hdwy Stg 1 | 5.55 | - | - | - | - |  |
| Critical Hdwy Stg 2 | 5.55 | - | - | - | - |  |
| Follow-up Hdwy | 3.635 | 3.435 | - |  | 2.254 |  |
| Pot Cap-1 Maneuver | 447 | 650 | - | - | 1145 |  |
| Stage 1 | 673 | - | - | - | - |  |
| Stage 2 | 782 | - | - | - | - |  |
| Platoon blocked, \% |  |  | - | - |  |  |
| Mov Cap-1 Maneuver | 431 | 650 | - | - | 1145 |  |
| Mov Cap-2 Maneuver | 431 | - | - | - | - |  |
| Stage 1 | 673 |  | - | - | - |  |
| Stage 2 | 754 | - | - | - | - |  |


| Approach | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 13.1 | 0 | 1.8 |
| HCM LOS | B |  |  |


| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
| :--- | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | - | -490 | 1145 | - |
| HCM Lane V/C Ratio | - | -0.095 | 0.036 | - |
| HCM Control Delay (s) | - | -13.1 | 8.3 | - |
| HCM Lane LOS | - | - | $B$ | A |
| HCM 95th \%tile Q(veh) | - | - | 0.3 | 0.1 |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh | 10.8 |
| Intersection LOS | B |


| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | M |  |  | $\uparrow$ | $\hat{1}$ |  |
| Traffic Vol, veh/h | 59 | 38 | 58 | 307 | 98 | 39 |
| Future Vol, veh/h | 59 | 38 | 58 | 307 | 98 | 39 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles, \% | 14 | 14 | 5 | 5 | 9 | 9 |
| Mvmt Flow | 66 | 42 | 64 | 341 | 109 | 43 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 0 |
| Approach | EB |  | NB |  | SB |  |
| Opposing Approach |  |  | SB |  | NB |  |
| Opposing Lanes | 0 |  | 1 |  | 1 |  |
| Conflicting Approach Left | SB |  | EB |  |  |  |
| Conflicting Lanes Left | 1 |  | 1 |  | 0 |  |
| Conflicting Approach Right | NB |  |  |  | EB |  |
| Conflicting Lanes Right | 1 |  | 0 |  | 1 |  |
| HCM Control Delay | 9.3 |  | 12 |  | 8.8 |  |
| HCM LOS | A |  | B |  | A |  |


| Lane | NBLn1 | EBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: |
| Vol Left, \% | $16 \%$ | $61 \%$ | $0 \%$ |
| Vol Thru, \% | $84 \%$ | $0 \%$ | $72 \%$ |
| Vol Right, \% | $0 \%$ | $39 \%$ | $28 \%$ |
| Sign Control | Stop | Stop | Stop |
| Traffic Vol by Lane | 565 | 97 | 137 |
| LT Vol | 58 | 59 | 0 |
| Through Vol | 0 | 0 | 98 |
| RT Vol | 0. | 38 | 39 |
| Lane Flow Rate | 1 | 108 | 152 |
| Geometry Grp | 1 | 1 |  |
| Degree of Util (X) | 0.504 | 0.158 | 0.195 |
| Departure Headway (Hd) | 4.475 | 5.277 | 4.61 |
| Convergence, Y/N | Yes | Yes | Yes |
| Cap | 807 | 678 | 776 |
| Service Time | 2.504 | 3.324 | 2.647 |
| HCM Lane V/C Ratio | 0.503 | 0.159 | 0.196 |
| HCM Control Delay | 12 | 9.3 | 8.8 |
| HCM Lane LOS | B | A | A |
| HCM 95th-tile Q | 2.9 | 0.6 | 0.7 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 0 | 1 | 364 | 0 | 3 | 133 |
| Future Vol, veh/h | 0 | 1 | 364 | 0 | 3 | 133 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 20 | 20 | 5 | 5 | 9 | 9 |
| Mvmt Flow | 0 | 1 | 404 | 0 | 3 | 148 |





Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.7 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  | 1 | 4 |
| Traffic Vol, veh/h | 35 | 56 | 359 | 30 | 23 | 465 |
| Future Vol, veh/h | 35 | 56 | 359 | 30 | 23 | 465 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 150 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 37 | 60 | 382 | 32 | 24 | 495 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 941 | 398 | 0 | 0 | 414 | 0 |
| Stage 1 | 398 | - | - | - | - | - |
| Stage 2 | 543 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 292 | 652 | - | - | 1145 | - |
| Stage 1 | 678 | - | - | - | - | - |
| Stage 2 | 582 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 286 | 652 | - | - | 1145 | - |
| Mov Cap-2 Maneuver | 286 | - | - | - | - | - |
| Stage 1 | 678 | - | - | - | - | - |
| Stage 2 | 570 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 15.6 |  | 0 |  | 0.4 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 437 | 1145 | - |
| HCM Lane V/C Ratio |  | - | - | 0.222 | 0.021 | - |
| HCM Control Delay (s) |  | - | - | 15.6 | 8.2 | - |
| HCM Lane LOS |  | - | - | C | A | - |
| HCM 95th \%tile Q(veh) |  | - | - | 0.8 | 0.1 | - |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh $\quad 20.8$ |  |
| Intersection LOS | C |


| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | M |  |  | $\uparrow$ | $\hat{1}$ |  |
| Traffic Vol, veh/h | 94 | 133 | 57 | 302 | 473 | 35 |
| Future Vol, veh/h | 94 | 133 | 57 | 302 | 473 | 35 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 3 | 3 |
| Mvmt Flow | 102 | 145 | 62 | 328 | 514 | 38 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 0 |
| Approach | EB |  | NB |  | SB |  |
| Opposing Approach |  |  | SB |  | NB |  |
| Opposing Lanes | 0 |  | 1 |  | 1 |  |
| Conflicting Approach Left | SB |  | EB |  |  |  |
| Conflicting Lanes Left | 1 |  | 1 |  | 0 |  |
| Conflicting Approach Right | NB |  |  |  | EB |  |
| Conflicting Lanes Right | 1 |  | 0 |  | 1 |  |
| HCM Control Delay | 13.3 |  | 16.7 |  | 27 |  |
| HCM LOS | B |  | C |  | D |  |


| Lane | NBLn1 | EBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: |
| Vol Left, \% | $16 \%$ | $41 \%$ | $0 \%$ |
| Vol Thru, \% | $84 \%$ | $0 \%$ | $93 \%$ |
| Vol Right, \% | $0 \%$ | $59 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop |
| Traffic Vol by Lane | 359 | 227 | 508 |
| LT Vol | 57 | 94 | 0 |
| Through Vol | 002 | 0 | 473 |
| RT Vol | 0 | 133 | 35 |
| Lane Flow Rate | 390 | 247 | 552 |
| Geometry Grp | 1 | 1 | 1 |
| Degree of Util (X) | 0.601 | 0.413 | 0.81 |
| Departure Headway (Hd) | 5.542 | 6.019 | 5.28 |
| Convergence, Y/N | Yes | Yes | Yes |
| Cap | 648 | 595 | 685 |
| Service Time | 3.598 | 4.083 | 3.331 |
| HCM Lane V/C Ratio | 0.602 | 0.415 | 0.806 |
| HCM Control Delay | 16.7 | 13.3 | 27 |
| HCM Lane LOS | C | B | D |
| HCM 95th-tile Q | 4 | 2 | 8.4 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\boldsymbol{F}$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 1 | 3 | 356 | 0 | 2 | 604 |
| Future Vol, veh/h | 1 | 3 | 356 | 0 | 2 | 604 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 20 | 20 | 2 | 20 | 20 | 3 |
| Mvmt Flow | 1 | 3 | 387 | 0 | 2 | 657 |





## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.6 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  | 1 | 4 |
| Traffic Vol, veh/h | 27 | 16 | 309 | 46 | 39 | 135 |
| Future Vol, veh/h | 27 | 16 | 309 | 46 | 39 | 135 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 150 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 15 | 15 | 6 | 6 | 6 | 6 |
| Mvmt Flow | 30 | 18 | 343 | 51 | 43 | 150 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 605 | 369 | 0 | 0 | 394 | 0 |
| Stage 1 | 369 | - | - | - | - | - |
| Stage 2 | 236 | - | - | - | - | - |
| Critical Hdwy | 6.55 | 6.35 | - | - | 4.16 | - |
| Critical Hdwy Stg 1 | 5.55 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.55 | - | - | - | - | - |
| Follow-up Hdwy | 3.635 | 3.435 | - | - | 2.254 | - |
| Pot Cap-1 Maneuver | 440 | 649 | - | - | 1143 | - |
| Stage 1 | 672 | - | - | - | - | - |
| Stage 2 | 774 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 423 | 649 | - | - | 1143 | - |
| Mov Cap-2 Maneuver | 423 | - | - | - | - | - |
| Stage 1 | 672 | - | - | - | - | - |
| Stage 2 | 745 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 13.2 |  | 0 |  | 1.9 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 486 | 1143 | - |
| HCM Lane V/C Ratio |  | - | - | 0.098 | 0.038 | - |
| HCM Control Delay (s) |  | - | - | 13.2 | 8.3 | - |
| HCM Lane LOS |  | - | - | B | A | - |
| HCM 95th \%tile Q(veh) |  | - | - | 0.3 | 0.1 | - |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh 10.9 |  |
| Intersection LOS | B |


| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | M |  |  | $\uparrow$ | $\hat{1}$ |  |
| Traffic Vol, veh/h | 59 | 38 | 58 | 309 | 103 | 39 |
| Future Vol, veh/h | 59 | 38 | 58 | 309 | 103 | 39 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles, \% | 14 | 14 | 5 | 5 | 9 | 9 |
| Mvmt Flow | 66 | 42 | 64 | 343 | 114 | 43 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 0 |
| Approach | EB |  | NB |  | SB |  |
| Opposing Approach |  |  | SB |  | NB |  |
| Opposing Lanes | 0 |  | 1 |  | 1 |  |
| Conflicting Approach Left | SB |  | EB |  |  |  |
| Conflicting Lanes Left | 1 |  | 1 |  | 0 |  |
| Conflicting Approach Right | NB |  |  |  | EB |  |
| Conflicting Lanes Right | 1 |  | 0 |  | 1 |  |
| HCM Control Delay | 9.4 |  | 12.1 |  | 8.8 |  |
| HCM LOS | A |  | B |  | A |  |


| Lane | NBLn1 | EBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: |
| Vol Left, \% | $16 \%$ | $61 \%$ | $0 \%$ |
| Vol Thru, \% | $84 \%$ | $0 \%$ | $73 \%$ |
| Vol Right, \% | $0 \%$ | $39 \%$ | $27 \%$ |
| Sign Control | Stop | Stop | Stop |
| Traffic Vol by Lane | 367 | 97 | 142 |
| LT Vol | 58 | 59 | 0 |
| Through Vol | 009 | 0 | 103 |
| RT Vol | 0 | 38 | 39 |
| Lane Flow Rate | 408 | 108 | 158 |
| Geometry Grp | 1 | 1 | 1 |
| Degree of Util (X) | 0.508 | 0.159 | 0.203 |
| Departure Headway (Hd) | 4.484 | 5.295 | 4.621 |
| Convergence, Y/N | Yes | Yes | Yes |
| Cap | 803 | 676 | 775 |
| Service Time | 2.514 | 3.344 | 2.659 |
| HCM Lane V/C Ratio | 0.508 | 0.16 | 0.204 |
| HCM Control Delay | 12.1 | 9.4 | 8.8 |
| HCM Lane LOS | B | A | A |
| HCM 95th-tile Q | 2.9 | 0.6 | 0.8 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 1 | 2 | 365 | 2 | 5 | 136 |
| Future Vol, veh/h | 1 | 2 | 365 | 2 | 5 | 136 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 20 | 20 | 5 | 5 | 9 | 9 |
| Mvmt Flow | 1 | 2 | 406 | 2 | 6 | 151 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 570 | 407 | 0 | 0 | 408 | 0 |
| Stage 1 | 407 | - | - | - | - | - |
| Stage 2 | 163 | - | - | - | - | - |
| Critical Hdwy | 6.6 | 6.4 | - | - | 4.19 | - |
| Critical Hdwy Stg 1 | 5.6 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.6 | - | - | - | - | - |
| Follow-up Hdwy | 3.68 | 3.48 | - | - | 2.281 | - |
| Pot Cap-1 Maneuver | 454 | 607 | - | - | 1114 | - |
| Stage 1 | 635 | - | - | - | - | - |
| Stage 2 | 824 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 451 | 607 | - | - | 1114 | - |
| Mov Cap-2 Maneuver | 451 | - | - | - | - | - |
| Stage 1 | 635 | - | - | - | - | - |
| Stage 2 | 819 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 11.7 |  | 0 |  | 0.3 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 544 | 1114 | - |
| HCM Lane V/C Ratio |  | - | - | 0.006 | 0.005 | - |
| HCM Control Delay (s) |  | - | - | 11.7 | 8.2 | 0 |
| HCM Lane LOS |  | - | - | B | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0 | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | -1 | Yr |  |
| Traffic Vol, veh/h | 83 | 2 | 4 | 42 | 1 | 1 |
| Future Vol, veh/h | 83 | 2 | 4 | 42 | 1 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 80 | 80 | 80 | 80 | 80 | 80 |
| Heavy Vehicles, \% | 6 | 6 | 15 | 15 | 50 | 50 |
| Mvmt Flow | 104 | 3 | 5 | 53 | 1 | 1 |





Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.7 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | $\mathbf{r}$ |  | $\uparrow$ |  | i | 个 |
| Traffic Vol, veh/h | 35 | 58 | 365 | 30 | 24 | 468 |
| Future Vol, veh/h | 35 | 58 | 365 | 30 | 24 | 468 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 150 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 37 | 62 | 388 | 32 | 26 | 498 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 954 | 404 | 0 | 0 | 420 | 0 |
| Stage 1 | 404 | - | - | - | - | - |
| Stage 2 | 550 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 287 | 647 | - | - | 1139 | - |
| Stage 1 | 674 | - | - | - | - | - |
| Stage 2 | 578 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 280 | 647 | - | - | 1139 | - |
| Mov Cap-2 Maneuver | 280 | - | - | - | - | - |
| Stage 1 | 674 | - | - | - | - | - |
| Stage 2 | 565 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 15.8 |  | 0 |  | 0.4 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 433 | 1139 | - |
| HCM Lane V/C Ratio |  | - | - | 0.228 | 0.022 | - |
| HCM Control Delay (s) |  | - | - | 15.8 | 8.2 | - |
| HCM Lane LOS |  | - | - | C | A | - |
| HCM 95th \%tile Q(veh) |  | - | - | 0.9 | 0.1 | - |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh $\quad 21.2$ |  |
| Intersection LOS | C |


| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | M |  |  | $\uparrow$ | $\hat{1}$ |  |
| Traffic Vol, veh/h | 94 | 133 | 57 | 308 | 476 | 35 |
| Future Vol, veh/h | 94 | 133 | 57 | 308 | 476 | 35 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 3 | 3 |
| Mvmt Flow | 102 | 145 | 62 | 335 | 517 | 38 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 0 |
| Approach | EB |  | NB |  | SB |  |
| Opposing Approach |  |  | SB |  | NB |  |
| Opposing Lanes | 0 |  | 1 |  | 1 |  |
| Conflicting Approach Left | SB |  | EB |  |  |  |
| Conflicting Lanes Left | 1 |  | 1 |  | 0 |  |
| Conflicting Approach Right | NB |  |  |  | EB |  |
| Conflicting Lanes Right | 1 |  | 0 |  | 1 |  |
| HCM Control Delay | 13.4 |  | 17 |  | 27.7 |  |
| HCM LOS | B |  | C |  | D |  |


| Lane | NBLn1 | EBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: |
| Vol Left, \% | $16 \%$ | $41 \%$ | $0 \%$ |
| Vol Thru, \% | $84 \%$ | $0 \%$ | $93 \%$ |
| Vol Right, \% | $0 \%$ | $59 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop |
| Traffic Vol by Lane | 365 | 227 | 511 |
| LT Vol | 57 | 94 | 0 |
| Through Vol | 308 | 0 | 476 |
| RT Vol | 0 | 133 | 35 |
| Lane Flow Rate | 397 | 247 | 555 |
| Geometry Grp | 1 | 1 | 1 |
| Degree of Util (X) | 0.612 | 0.414 | 0.817 |
| Departure Headway (Hd) | 5.553 | 6.046 | 5.296 |
| Convergence, Y/N | Yes | Yes | Yes |
| Cap | 647 | 592 | 683 |
| Service Time | 3.607 | 4.109 | 3.344 |
| HCM Lane V/C Ratio | 0.614 | 0.417 | 0.813 |
| HCM Control Delay | 17 | 13.4 | 27.7 |
| HCM Lane LOS | C | B | D |
| HCM 95th-tile Q | 4.2 | 2 | 8.6 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\mathbf{F}$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 2 | 6 | 359 | 1 | 3 | 606 |
| Future Vol, veh/h | 2 | 6 | 359 | 1 | 3 | 606 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 20 | 20 | 2 | 20 | 20 | 3 |
| Mvmt Flow | 2 | 7 | 390 | 1 | 3 | 659 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1056 | 391 | 0 | 0 | 391 | 0 |
| Stage 1 | 391 | - | - | - | - | - |
| Stage 2 | 665 | - | - | - | - | - |
| Critical Hdwy | 6.6 | 6.4 | - | - | 4.3 | - |
| Critical Hdwy Stg 1 | 5.6 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.6 | - | - | - | - | - |
| Follow-up Hdwy | 3.68 | 3.48 | - | - | 2.38 | - |
| Pot Cap-1 Maneuver | 231 | 620 | - | - | 1076 | - |
| Stage 1 | 646 | - | - | - | - | - |
| Stage 2 | 479 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 230 | 620 | - | - | 1076 | - |
| Mov Cap-2 Maneuver | 230 | - | - | - | - | - |
| Stage 1 | 646 | - | - | - | - | - |
| Stage 2 | 477 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 13.4 |  | 0 |  | 0 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 435 | 1076 | - |
| HCM Lane V/C Ratio |  | - | - | 0.02 | 0.003 | - |
| HCM Control Delay (s) |  | - | - | 13.4 | 8.4 | 0 |
| HCM Lane LOS |  | - | - | B | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.1 | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



## Intersection: 1: 362nd Avenue \& US Hwy 26

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | T | T | L | L | $R$ |
| Maximum Queue (ft) | 262 | 246 | 85 | 157 | 174 | 174 | 140 | 274 | 140 |
| Average Queue (ft) | 148 | 96 | 31 | 78 | 88 | 70 | 78 | 118 | 66 |
| 95th Queue (ft) | 248 | 199 | 65 | 146 | 154 | 138 | 141 | 215 | 137 |
| Link Distance (ft) | 890 | 890 |  |  | 1768 | 1768 |  | 648 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  | 115 |  |
| Storage Bay Dist (ft) |  | 0 |  | 500 |  |  | 1 | 7 | 115 |
| Storage Blk Time (\%) |  | 0 |  |  |  |  | 3 | 16 | 1 |
| Queuing Penalty (veh) |  | 0 |  |  |  |  |  |  |  |

Intersection: 2: 362nd Avenue \& Industrial Way

| Movement | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| Directions Served | LR | TR | L |
| Maximum Queue (ft) | 80 | 5 | 57 |
| Average Queue (ft) | 30 | 0 | 15 |
| 95th Queue (ft) | 62 | 4 | 45 |
| Link Distance (ft) | 373 | 164 |  |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |

Intersection: 3: 362nd Avenue \& Industrial Way

| Movement | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| Directions Served | LR | LT | TR |
| Maximum Queue (ft) | 89 | 120 | 89 |
| Average Queue (ft) | 44 | 67 | 44 |
| 95th Queue (ft) | 71 | 103 | 71 |
| Link Distance (ft) | 443 | 551 | 164 |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |

## Intersection: 4: 362nd Avenue \& Site Access

| Movement | WB | SB |
| :--- | ---: | ---: |
| Directions Served | LR | LT |
| Maximum Queue (ft) | 35 | 20 |
| Average Queue (ft) | 3 | 1 |
| 95th Queue (ft) | 19 | 10 |
| Link Distance (ft) | 365 | 551 |
| Upstream Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Bay Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |

Intersection: 5: Proposed Access \& Industrial Way

| Movement | WB | NB |
| :--- | ---: | ---: |
| Directions Served | LT | LR |
| Maximum Queue (ft) | 23 | 67 |
| Average Queue (ft) | 1 | 4 |
| 95th Queue (ft) | 10 | 30 |
| Link Distance (ft) | 306 | 173 |
| Upstream Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Baa Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Network Summary |  |  |
| Network wide Queuing Penalty: 22 |  |  |

## Intersection: 1: 362nd Avenue \& US Hwy 26

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | T | T | L | L | R |
| Maximum Queue (ft) | 513 | 502 | 275 | 323 | 180 | 184 | 140 | 556 | 140 |
| Average Queue (ft) | 330 | 288 | 133 | 196 | 95 | 79 | 108 | 343 | 134 |
| 95th Queue (ft) | 474 | 452 | 280 | 310 | 161 | 151 | 162 | 573 | 161 |
| Link Distance (ft) | 890 | 890 |  |  | 1768 | 1768 |  | 648 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  | 0 |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  | 1 |  |
| Storage Bay Dist (ft) |  |  | 250 | 500 |  |  | 115 |  | 115 |
| Storage Blk Time (\%) |  | 6 | 0 |  |  |  | 6 | 29 | 22 |
| Queuing Penalty (veh) |  | 19 | 3 |  |  |  | 27 | 127 | 59 |

Intersection: 2: 362nd Avenue \& Industrial Way

| Movement | WB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LR | TR | L | T |
| Maximum Queue (ft) | 180 | 26 | 63 | 189 |
| Average Queue (ft) | 58 | 1 | 9 | 27 |
| 95th Queue (ft) | 128 | 20 | 41 | 106 |
| Link Distance (ft) | 373 | 164 |  | 648 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  | 150 |  |
| Storage Bay Dist (ft) |  |  |  | 1 |
| Storage Blk Time (\%) |  |  |  | 0 |

Intersection: 3: 362nd Avenue \& Industrial Way

| Movement | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| Directions Served | LR | LT | TR |
| Maximum Queue (ft) | 121 | 129 | 176 |
| Average Queue (ft) | 61 | 73 | 126 |
| 95th Queue (ft) | 99 | 115 | 186 |
| Link Distance (ft) | 443 | 551 | 164 |
| Upstream Blk Time (\%) |  |  | 2 |
| Queuing Penalty (veh) |  |  | 9 |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |

## Intersection: 4: 362nd Avenue \& Site Access

| Movement | WB | SB |
| :--- | ---: | ---: |
| Directions Served | LR | LT |
| Maximum Queue (ft) | 57 | 20 |
| Average Queue (ft) | 9 | 1 |
| 95th Queue (ft) | 36 | 12 |
| Link Distance (ft) | 365 | 551 |
| Upstream Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Bay Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |

Intersection: 5: Proposed Access \& Industrial Way

| Movement | WB | NB |
| :--- | ---: | ---: |
| Directions Served | LT | LR |
| Maximum Queue (ft) | 7 | 71 |
| Average Queue (ft) | 0 | 10 |
| 95th Queue (ft) | 5 | 46 |
| Link Distance (ft) | 306 | 173 |
| Upstream Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Baa Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Network Summary |  |  |
| Network wide Queuing Penalty: 245 |  |  |








## Preliminary Traffic Signal Warrant Analysis

Project Name: Johnson RV
Intersection: 362nd at Industrial (North)
Scenario: 2023 Background plus Site Trips
Number of Major Street Lanes $\qquad$ PM Peak Hour Volume $\qquad$ (sum of both approaches)
Number of Minor Street Lanes 1 PM Peak Hour Volume 35 (highest-volume approach) ${ }^{\text {a }}$
Posted or 85th percentile speed $>40 \mathrm{mph}$ : No
Isolated Population Less than 10,000:
No

## Warrant 1, Eight-Hour Vehicular Volume

Condition A - Minimum Vehicular Volume

| Number of lanes for moving <br> traffic on each approach | Vehicles per hour on major street <br> (total of both approaches) |  |  | Vehicles per hour on minor street <br> (total of both approaches) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street | Minor Street | $100 \%$ | $80 \%$ | $70 \%$ | $56 \%$ | $100 \%$ | $80 \%$ | $70 \%$ | $56 \%$ |
| 1 | 1 | 500 | 400 | 350 | 280 | 150 | 120 | 105 | 84 |
| 2 or more | 1 | 600 | 480 | 420 | 336 | 150 | 120 | 105 | 84 |
| 2 or more | 2 or more | 600 | 480 | 420 | 336 | 200 | 160 | 140 | 112 |
| 1 | 2 or more | 500 | 400 | 350 | 280 | 200 | 160 | 140 | 112 |

Condition B - Interruption of Continuous Traffic

| Number of lanes for moving traffic on each approach |  | Vehicles per hour on major street (total of both approaches) |  |  |  | Vehicles per hour on minor street (total of both approaches) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street | Minor Street | 100\% | 80\% | 70\% | 56\% | 100\% | 80\% | 70\% | 56\% |
| 1 | 1 | 750 | 600 | 525 | 420 | 75 | 60 | 53 | 42 |
| 2 or more | 1 | 900 | 720 | 630 | 504 | 75 | 60 | 53 | 42 |
| 2 or more | 2 or more | 900 | 720 | 630 | 504 | 100 | 80 | 70 | 56 |
| 1 | 2 or more | 750 | 600 | 525 | 420 | 100 | 80 | 70 | 56 |
| Warrant Anaylsis Calculations |  |  |  | 8th Highest Hour ${ }^{\text {b }}$ |  | Minimum Volume |  | Warrant Satisfied? |  |
| Condition A - Minimum Vehicular Volume |  |  |  |  |  |  |  |  |  |
| Major Street Volume |  |  |  | 501 |  | 500 |  |  |  |
| Minor Street Volume |  |  |  | 20 |  | 150 |  | No |  |
| Condition B - Interruption of Continuous Traffic |  |  |  |  |  |  |  |  |  |
| Major Street Volume |  |  |  | 501 |  | 750 |  |  |  |
| Minor Street Volume |  |  |  | 20 |  | 75 |  | No |  |
| Combination Warrant ${ }^{\text {c }}$ |  |  |  |  |  |  |  |  |  |
| Major Street Volume |  |  |  | 501 |  | 600 |  |  |  |
| Minor Street Volume |  |  |  | 20 |  | 120 |  | No |  |
| ${ }^{\text {a }}$ Minor-Street right turn volumes are reduced to account for the impact of right-turns on red. |  |  |  |  |  |  |  |  |  |
| ${ }^{\mathrm{b}}$ Eighth-highest hour volumes are calculated as 5.65 percent of the expected daily traffic volume. |  |  |  |  |  |  |  |  |  |
| ${ }^{\text {c }}$ This warrant should be used only after adequate trial of other alternatives has failed to solve traffic problems. |  |  |  |  |  |  |  |  |  |

## Preliminary Traffic Signal Warrant Analysis

Project Name: Johnson RV
Intersection: 362nd at Industrial (South)
Scenario: 2023 Background plus Site Trips
Number of Major Street Lanes $\qquad$ 1
Number of Minor Street Lanes $\qquad$ 1 PM Peak Hour Volume $\qquad$ (sum of both approaches) PM Peak Hour Volume $\qquad$ (highest-volume approach) ${ }^{\text {a }}$
Posted or 85 th percentile speed $>40 \mathrm{mph}$ : No
Isolated Population Less than 10,000:
No

## Warrant 1, Eight-Hour Vehicular Volume

Condition A - Minimum Vehicular Volume

| Number of lanes for moving <br> traffic on each approach | Vehicles per hour on major street <br> (total of both approaches) |  |  | Vehicles per hour on minor street <br> (total of both approaches) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street | Minor Street | $100 \%$ | $80 \%$ | $70 \%$ | $56 \%$ | $100 \%$ | $80 \%$ | $70 \%$ | $56 \%$ |
| 1 | 1 | 500 | 400 | 350 | 280 | 150 | 120 | 105 | 84 |
| 2 or more | 1 | 600 | 480 | 420 | 336 | 150 | 120 | 105 | 84 |
| 2 or more | 2 or more | 600 | 480 | 420 | 336 | 200 | 160 | 140 | 112 |
| 1 | 2 or more | 500 | 400 | 350 | 280 | 200 | 160 | 140 | 112 |

Condition B - Interruption of Continuous Traffic

| Number of lanes for moving traffic on each approach |  | Vehicles per hour on major street (total of both approaches) |  |  |  | Vehicles per hour on minor street (total of both approaches) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street | Minor Street | 100\% | 80\% | 70\% | 56\% | 100\% | 80\% | 70\% | 56\% |
| 1 | 1 | 750 | 600 | 525 | 420 | 75 | 60 | 53 | 42 |
| 2 or more | 1 | 900 | 720 | 630 | 504 | 75 | 60 | 53 | 42 |
| 2 or more | 2 or more | 900 | 720 | 630 | 504 | 100 | 80 | 70 | 56 |
| 1 | 2 or more | 750 | 600 | 525 | 420 | 100 | 80 | 70 | 56 |
| Warrant Anaylsis Calculations |  |  |  | 8th Highest Hour ${ }^{\text {b }}$ |  | Minimum Volume |  | Warrant Satisfied? |  |
| Condition A - Minimum Vehicular Volume |  |  |  |  |  |  |  |  |  |
| Major Street Volume |  |  |  | 495 |  | 500 |  |  |  |
| Minor Street Volume |  |  |  | 53 |  | 150 |  | No |  |
| Condition B - Interruption of Continuous Traffic |  |  |  |  |  |  |  |  |  |
| Major Street Volume |  |  |  | 495 |  | 750 |  |  |  |
| Minor Street Volume |  |  |  | 53 |  | 75 |  | No |  |
| Combination Warrant ${ }^{\text {c }}$ |  |  |  |  |  |  |  |  |  |
| Major Street Volume |  |  |  | 495 |  | 600 |  |  |  |
| Minor Street Volume |  |  |  | 53 |  | 120 |  | No |  |
| ${ }^{\text {a }}$ Minor-Street right turn volumes are reduced to account for the impact of right-turns on red. |  |  |  |  |  |  |  |  |  |
| ${ }^{\mathrm{b}}$ Eighth-highest hour volumes are calculated as 5.65 percent of the expected daily traffic volume. |  |  |  |  |  |  |  |  |  |
| ${ }^{\text {c }}$ This warrant should be used only after adequate trial of other alternatives has failed to solve traffic problems. |  |  |  |  |  |  |  |  |  |

## Preliminary Traffic Signal Warrant Analysis

Project Name: Johnson RV
Intersection: 362nd at Site Access
Scenario: 2023 Background plus Site Trips
Number of Major Street Lanes: $\qquad$ PM Peak Hour Volume $\qquad$ 969 (sum of both approaches)
Number of Minor Street Lanes 1 PM Peak Hour Volume 2 (highest-volume approach) ${ }^{\text {a }}$
Posted or 85th percentile speed $>40 \mathrm{mph}$ : No
Isolated Population Less than 10,000:
No

## Warrant 1, Eight-Hour Vehicular Volume

Condition A - Minimum Vehicular Volume

| Number of lanes for moving <br> traffic on each approach | Vehicles per hour on major street <br> (total of both approaches) |  |  | Vehicles per hour on minor street <br> (total of both approaches) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street | Minor Street | $100 \%$ | $80 \%$ | $70 \%$ | $56 \%$ | $100 \%$ | $80 \%$ | $70 \%$ | $56 \%$ |
| 1 | 1 | 500 | 400 | 350 | 280 | 150 | 120 | 105 | 84 |
| 2 or more | 1 | 600 | 480 | 420 | 336 | 150 | 120 | 105 | 84 |
| 2 or more | 2 or more | 600 | 480 | 420 | 336 | 200 | 160 | 140 | 112 |
| 1 | 2 or more | 500 | 400 | 350 | 280 | 200 | 160 | 140 | 112 |

Condition B - Interruption of Continuous Traffic

| Number of lanes for moving traffic on each approach |  | Vehicles per hour on major street (total of both approaches) |  |  |  | Vehicles per hour on minor street (total of both approaches) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street | Minor Street | 100\% | 80\% | 70\% | 56\% | 100\% | 80\% | 70\% | 56\% |
| 1 | 1 | 750 | 600 | 525 | 420 | 75 | 60 | 53 | 42 |
| 2 or more | 1 | 900 | 720 | 630 | 504 | 75 | 60 | 53 | 42 |
| 2 or more | 2 or more | 900 | 720 | 630 | 504 | 100 | 80 | 70 | 56 |
| 1 | 2 or more | 750 | 600 | 525 | 420 | 100 | 80 | 70 | 56 |
| Warrant Anaylsis Calculations |  |  |  | 8th Highest Hour ${ }^{\text {b }}$ |  | Minimum Volume |  | Warrant Satisfied? |  |
| Condition A - Minimum Vehicular Volume |  |  |  |  |  |  |  |  |  |
| Major Street Volume |  |  |  | 547 |  | 500 |  |  |  |
| Minor Street Volume |  |  |  | 1 |  | 150 |  | No |  |
| Condition B - Interruption of Continuous Traffic |  |  |  |  |  |  |  |  |  |
| Major Street Volume |  |  |  | 547 |  | 750 |  |  |  |
| Minor Street Volume |  |  |  | 1 |  | 75 |  | No |  |
| Combination Warrant ${ }^{\text {c }}$ |  |  |  |  |  |  |  |  |  |
| Major Street Volume |  |  |  | 547 |  | 600 |  |  |  |
| Minor Street Volume |  |  |  | 1 |  | 120 |  | No |  |
| ${ }^{\text {a }}$ Minor-Street right turn volumes are reduced to account for the impact of right-turns on red. |  |  |  |  |  |  |  |  |  |
| ${ }^{\mathrm{b}}$ Eighth-highest hour volumes are calculated as 5.65 percent of the expected daily traffic volume. |  |  |  |  |  |  |  |  |  |
| ${ }^{\text {c }}$ This warrant should be used only after adequate trial of other alternatives has failed to solve traffic problems. |  |  |  |  |  |  |  |  |  |

## Preliminary Traffic Signal Warrant Analysis

Project Name: Johnson RV
Intersection: Industrial at Proposed Site Access
Scenario: 2023 Background plus Site Trips
Number of Major Street Lanes: 1
Number of Minor Street Lanes 1

PM Peak Hour Volume $\qquad$ 147 (sum of both approaches) PM Peak Hour Volume $\qquad$ (highest-volume approach) ${ }^{\text {a }}$

Posted or 85th percentile speed > 40 mph : No
Isolated Population Less than 10,000: No

## Warrant 1, Eight-Hour Vehicular Volume

Condition A - Minimum Vehicular Volume

| Number of lanes for moving <br> traffic on each approach | Vehicles per hour on major street <br> (total of both approaches) |  |  | Vehicles per hour on minor street <br> (total of both approaches) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street | Minor Street | $100 \%$ | $80 \%$ | $70 \%$ | $56 \%$ | $100 \%$ | $80 \%$ | $70 \%$ | $56 \%$ |
| 1 | 1 | 500 | 400 | 350 | 280 | 150 | 120 | 105 | 84 |
| 2 or more | 1 | 600 | 480 | 420 | 336 | 150 | 120 | 105 | 84 |
| 2 or more | 2 or more | 600 | 480 | 420 | 336 | 200 | 160 | 140 | 112 |
| 1 | 2 or more | 500 | 400 | 350 | 280 | 200 | 160 | 140 | 112 |

Condition B - Interruption of Continuous Traffic

| Number of lanes for moving traffic on each approach |  | Vehicles per hour on major street (total of both approaches) |  |  |  | Vehicles per hour on minor street (total of both approaches) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street | Minor Street | 100\% | 80\% | 70\% | 56\% | 100\% | 80\% | 70\% | 56\% |
| 1 | 1 | 750 | 600 | 525 | 420 | 75 | 60 | 53 | 42 |
| 2 or more | 1 | 900 | 720 | 630 | 504 | 75 | 60 | 53 | 42 |
| 2 or more | 2 or more | 900 | 720 | 630 | 504 | 100 | 80 | 70 | 56 |
| 1 | 2 or more | 750 | 600 | 525 | 420 | 100 | 80 | 70 | 56 |
| Warrant Anaylsis Calculations |  |  |  | 8th Highest Hour ${ }^{\text {b }}$ |  | Minimum Volume |  | Warrant Satisfied? |  |
| Condition A - Minimum Vehicular Volume |  |  |  |  |  |  |  |  |  |
| Major Street Volume |  |  |  | 83 |  | 500 |  |  |  |
| Minor Street Volume |  |  |  | 1 |  | 150 |  | No |  |
| Condition B - Interruption of Continuous Traffic |  |  |  |  |  |  |  |  |  |
| Major Street Volume |  |  |  | 83 |  | 750 |  |  |  |
| Minor Street Volume |  |  |  | 1 |  | 75 |  | No |  |
| Combination Warrant ${ }^{\text {c }}$ |  |  |  |  |  |  |  |  |  |
| Major Street Volume |  |  |  | 83 |  | 600 |  |  |  |
| Minor Street Volume |  |  |  | 1 |  | 120 |  | No |  |
| ${ }^{\text {a }}$ Minor-Street right turn volumes are reduced to account for the impact of right-turns on red. |  |  |  |  |  |  |  |  |  |
| ${ }^{\mathrm{b}}$ Eighth-highest hour volumes are calculated as 5.65 percent of the expected daily traffic volume. |  |  |  |  |  |  |  |  |  |
| ${ }^{\text {c }}$ This warrant should be used only after adequate trial of other alternatives has failed to solve traffic problems. |  |  |  |  |  |  |  |  |  |

## Left-Turn Lane Warrant Analysis (ODOT Methodology)

Project Name: Johnson RV
Approach: Northbound 362nd Avenue at Industrial (South)
Scenario: 2022 Existing Conditions

Number of Advancing Lanes: 1
Number of Opposing Lanes: 1
Major-Street Design Speed: 35 mph

|  | AM Volume | PM Volume |
| :--- | :---: | :---: |
| Advancing Volume for Design Hour: | 349 | 344 |
| Opposing Volume for Design Hour: | 127 | 488 |
| Design Hour Volume Per Lane: | 476 | 832 |
| Number of Left Turns per Hour: | 56 | 54 |
| Left-turn lane warrants satisfied? | YES | YES |

## Exhibit 7-1 Left Turn Lane Criterion (TTI)


*(Advancing Volume/Number of Advancing Through Lanes) + (Opposing Volume/Number of Opposing Through Lanes)

## Left-Turn Lane Warrant Analysis (ODOT Methodology)

Project Name: Johnson RV
Approach: Southbound 362nd Avenue at Site Access
Scenario: 2023 Background plus Site Trips

Number of Advancing Lanes: 1
Number of Opposing Lanes: 1
Major-Street Design Speed: 35 mph

|  | AM Volume | PM Volume |
| :--- | :---: | :---: |
| Advancing Volume for Design Hour: | 141 | 609 |
| Opposing Volume for Design Hour: | 367 | 360 |
| Design Hour Volume Per Lane: | 508 | 969 |
| Number of Left Turns per Hour: | 5 | 3 |
| Left-turn lane warrants satisfied? | NO | NO |

## Exhibit 7-1 Left Turn Lane Criterion (TTI)


*(Advancing Volume/Number of Advancing Through Lanes) + (Opposing Volume/Number of Opposing Through Lanes)

## Left-Turn Lane Warrant Analysis (ODOT Methodology)

Project Name: Johnson RV
Approach: Westbound Industrial at Proposed Site Access
Scenario: 2023 Background plus Site Trips

Number of Advancing Lanes: 1
Number of Opposing Lanes: 1
Major-Street Design Speed: 25 mph

|  | AM Volume | PM Volume |
| :--- | :---: | :---: |
| Advancing Volume for Design Hour: | 44 | 93 |
| Opposing Volume for Design Hour: | 85 | 54 |
| Design Hour Volume Per Lane: | 129 | 147 |
| Number of Left Turns per Hour: | 4 | 2 |
| Left-turn lane warrants satisfied? | NO | NO |

## Exhibit 7-1 Left Turn Lane Criterion (TTI)


*(Advancing Volume/Number of Advancing Through Lanes) + (Opposing Volume/Number of Opposing Through Lanes)

## Right-Turn Lane Warrant Analysis (ODOT Methodology)

Project Name: Johnson RV
Approach: Northbound 362nd at Industrial (North)
Scenario: 2023 Background plus Site Trips

Major-Street Design Speed: 35 mph

|  | AM Volume | PM Volume |
| :--- | :---: | :---: |
| Number of Right Turns per Hour: | 46 | 30 |
| Approaching DVH in Outside Lane: | 355 | 395 |
| Calculated Turn Volume Threshold: | 66 | 61 |
| Right Turn Volume Exceeds Threshold? | NO | NO |

## Criterion 1: Vehicular Volume

The vehicular volume criterion is intended for application where the volume of intersecting traffic is the principal reason for considering installation of a right turn lane. The vehicular volume criteria are determined using the curve in Exhibit 7-2.

## Exhibit 7-2 Right Turn Lane Criterion



Note: If there is no right turn lane, a shoulder needs to be provided. If this intersection is in a rural area and is a connection to a public street, a right turn lane is needed.

## Right-Turn Lane Warrant Analysis (ODOT Methodology)

Project Name: Johnson RV
Approach: Southbound 362nd at Industrial (South)
Scenario: 2023 Background plus Site Trips

Major-Street Design Speed: 35 mph

|  | AM Volume | PM Volume |
| :--- | :---: | :---: |
| Number of Right Turns per Hour: | 39 | 35 |
| Approaching DVH in Outside Lane: | 142 | 511 |
| Calculated Turn Volume Threshold: | 94 | 45 |
| Right Turn Volume Exceeds Threshold? | NO | NO |

## Criterion 1: Vehicular Volume

The vehicular volume criterion is intended for application where the volume of intersecting traffic is the principal reason for considering installation of a right turn lane. The vehicular volume criteria are determined using the curve in Exhibit 7-2.

## Exhibit 7-2 Right Turn Lane Criterion



Note: If there is no right turn lane, a shoulder needs to be provided. If this intersection is in a rural area and is a connection to a public street, a right turn lane is needed.

## Right-Turn Lane Warrant Analysis (ODOT Methodology)

Project Name: Johnson RV
Approach: Northbound 362nd at Site Access
Scenario: 2023 Background plus Site Trips

Major-Street Design Speed: 35 mph

|  | AM Volume | PM Volume |
| :--- | :---: | :---: |
| Number of Right Turns per Hour: | 2 | 1 |
| Approaching DVH in Outside Lane: | 367 | 360 |
| Calculated Turn Volume Threshold: | 64 | 65 |
| Right Turn Volume Exceeds Threshold? | NO | NO |

## Criterion 1: Vehicular Volume

The vehicular volume criterion is intended for application where the volume of intersecting traffic is the principal reason for considering installation of a right turn lane. The vehicular volume criteria are determined using the curve in Exhibit 7-2.

## Exhibit 7-2 Right Turn Lane Criterion



Note: If there is no right turn lane, a shoulder needs to be provided. If this intersection is in a rural area and is a connection to a public street, a right turn lane is needed.

## Right-Turn Lane Warrant Analysis (ODOT Methodology)

Project Name: Johnson RV
Approach: Eastbound Industrial at Proposed Site Access
Scenario: 2023 Background plus Site Trips

Major-Street Design Speed: 35 mph

|  | AM Volume | PM Volume |
| :--- | :---: | :---: |
| Number of Right Turns per Hour: | 2 | 1 |
| Approaching DVH in Outside Lane: | 85 | 54 |
| Calculated Turn Volume Threshold: | 102 | 106 |
| Right Turn Volume Exceeds Threshold? | NO | NO |

## Criterion 1: Vehicular Volume

The vehicular volume criterion is intended for application where the volume of intersecting traffic is the principal reason for considering installation of a right turn lane. The vehicular volume criteria are determined using the curve in Exhibit 7-2.

## Exhibit 7-2 Right Turn Lane Criterion



Note: If there is no right turn lane, a shoulder needs to be provided. If this intersection is in a rural area and is a connection to a public street, a right turn lane is needed.

## Speed Study Summary - Radar Data

Location: SE 362nd Avenue
Direction: Northbound


Date: August 31, 2022
Time: 3:00 PM
Weather: Clear/Dry
Notes: Occasional queues back up and impact through travel speeds. Data collecton was stopped during these incidents to capture free-flow speeds.

## 85th Percentile Speed

Average Speed:

37 mph
33 mph

Recorded Speeds:*

| 1 mph ------- 0 | $26 \mathrm{mph}------2$ | $51 \mathrm{mph}------0$ |
| :---: | :---: | :---: |
| 2 mph ------- 0 | $27 \mathrm{mph}------3$ | 52 mph ------- 0 |
| 3 mph ------- 0 | 28 mph ------- 4 | 53 mph ------- 0 |
| 4 mph ------- 0 | 29 mph ------- 3 | 54 mph ------- 0 |
| 5 mph ------- 0 | 30 mph ------- 5 | 55 mph ------- 0 |
| 6 mph ------- 0 | 31 mph ------- 14 | 56 mph ------- 0 |
| 7 mph ------- 0 | 32 mph ------- 13 | 57 mph ------- 0 |
| 8 mph ------- 0 | 33 mph ------- 8 | 58 mph ------- 0 |
| 9 mph ------- 0 | 34 mph ------- 12 | 59 mph ------- 0 |
| 10 mph ------- 0 | 35 mph ------- 7 | 60 mph ------- 0 |
| 11 mph ------- 0 | 36 mph ------- 10 | 61 mph ------- 0 |
| 12 mph ------- 0 | 37 mph ------- 5 | 62 mph ------- 0 |
| 13 mph ------- 0 | 38 mph ------- 4 | 63 mph ------- 0 |
| 14 mph ------- 0 | 39 mph ------- 2 | 64 mph ------- 0 |
| 15 mph ------- 0 | 40 mph ------- 1 | 65 mph ------- 0 |
| 16 mph ------- 0 | $41 \mathrm{mph}------0$ | 66 mph ------- 0 |
| $17 \mathrm{mph}------0$ | $42 \mathrm{mph}------2$ | $67 \mathrm{mph}------0$ |
| 18 mph ------- 0 | $43 \mathrm{mph}------0$ | 68 mph ------- 0 |
| 19 mph ------- 0 | 44 mph ------- 1 | 69 mph ------- 0 |
| 20 mph ------- 0 | 45 mph ------- 0 | 70 mph ------- 0 |
| 21 mph ------- 0 | 46 mph ------- 0 | 71 mph ------- 0 |
| 22 mph ------- 0 | 47 mph ------- 0 | 72 mph ------- 0 |
| 23 mph ------- 1 | 48 mph ------- 0 | $73 \mathrm{mph}------0$ |
| 24 mph ------- 1 | $49 \mathrm{mph}------1$ | 74 mph ------- 0 |
| 25 mph ------- 1 | 50 mph ------- 0 | 75+ mph ------- 0 |

[^2]
## Speed Study Summary - Radar Data

Location: Industrial Way (North)
Direction: Westbound
Date: 11/7/2022
Time: 2:00 PM
Weather: Overcast, showers
Notes: None

85th Percentile Speed:
Average Speed:

33 mph
29 mph

Recorded Speeds:*

| 1 mph ------- | 0 | 26 mph -------6 | $51 \mathrm{mph}------0$ |
| :---: | :---: | :---: | :---: |
| 2 mph ------- | 0 | 27 mph ------- 9 | 52 mph ------- 0 |
| 3 mph ------- | 0 | 28 mph ------- 10 | 53 mph ------- 0 |
| 4 mph ------- | 0 | 29 mph ------- 10 | 54 mph ------- 0 |
| 5 mph ------- | 0 | 30 mph ------- 4 | 55 mph ------- 0 |
| 6 mph ------- | 0 | 31 mph ------- 8 | 56 mph ------- 0 |
| 7 mph ------- | 0 | 32 mph ------- 7 | 57 mph ------- 0 |
| 8 mph ------- | 0 | 33 mph ------- 10 | 58 mph ------- 0 |
| 9 mph ------- | 0 | 34 mph ------- 2 | 59 mph ------- 0 |
| 10 mph ------- | 0 | 35 mph ------- 2 | 60 mph ------- 0 |
| 11 mph ------- | 0 | 36 mph ------- 0 | 61 mph ------- 0 |
| 12 mph ------- | 0 | 37 mph ------- 3 | 62 mph ------- 0 |
| 13 mph ------- | 0 | 38 mph -------1 | 63 mph ------- 0 |
| 14 mph ------- | 0 | 39 mph ------- 0 | 64 mph ------- 0 |
| 15 mph ------- | 0 | 40 mph ------- 1 | 65 mph ------- 0 |
| 16 mph ------- | 0 | 41 mph -------1 | 66 mph ------- 0 |
| 17 mph ------- | 1 | 42 mph ------- 0 | 67 mph ------- 0 |
| 18 mph ------- | 1 | 43 mph ------- 0 | 68 mph ------- 0 |
| 19 mph ------- | 0 | 44 mph -------1 | 69 mph ------- 0 |
| 20 mph ------- | 2 | 45 mph ------- 0 | 70 mph ------- 0 |
| 21 mph ------- | 3 | 46 mph ------- 0 | 71 mph ------- 0 |
| 22 mph ------- | 4 | 47 mph ------- 0 | 72 mph ------- 0 |
| 23 mph ------- | 1 | 48 mph ------- 0 | 73 mph ------- 0 |
| 24 mph ------- | 7 | 49 mph ------- 0 | 74 mph ------- 0 |
| 25 mph ------- | 6 | 50 mph ------- 0 | 75+ mph ------- 0 |

[^3]
[^0]:    *Seasonal Trend Table factors are based on previous year ATR data. The table is updated yearly

    * Grey shading indicates months were seasonal factor is greater than or less than $30 \%$
    *February 2019 snow event causing lower seasonal factors

[^1]:    Scenario 1 Johnson RV 1:41 pm 08/26/2022 2022 Existing AM Peak Hour

[^2]:    * Speed data observations include free-flowing traffic only (i.e. no following vehicles)

[^3]:    * Speed data observations include free-flowing traffic only (i.e. no following vehicles)

