Exhibit E

EXHIBIT G – PRELIMINARY STORMWATER REPORT

SITE HYDRAULICS REPORT

"THE PAD" DRAINAGE REPORT

FOR "THE PAD" DEVELOPMENT

SANDY, OREGON

JULY 6, 2020

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INTRODUCTION

1.1 Project Overview

This report contains the hydrologic and hydraulic design parameters for the "THE PAD" Sandy Development Project at tax lot 1500; Assessor Map 2S-24E-13DB-01500, with the total area is approximately 0.478 acres. The property is situated at 17650 Meinig Avenue in Sandy, Oregon. This report reviews and confirms the information necessary to design on-site conveyance systems as well as water quality treatment facilities for "THE PAD" Sandy Development Project and the retention system on the site which will be located in the south driveway of the development.

Please note that the methodology used to analyze the storm water conveyance system uses a computer program (Hydraflow 2002 by inteliSOLV) that uses SCS unit hydrograph as the method for calculating the Storm Flow. The land for the development required the use of a Contech storm filter system for treatment. The plan includes 1 Contech manhole storm filter that is shown on the C3 Utility Plan attached in the appendix.

1.2 Existing Conditions

The site originally had a home, shed and yard that encompassed the central portion of the property. The structures are no longer present.

1.3 Proposed Improvements

The proposed development will include a 10 unit 2 story townhouse apartments. 6 units with be on the south end while 4 will be on the north end of the development. 1 handicap parking space and 20 regular parking spaces will be provided. Six 9'x18'parking spaces will be on the north end while seven 9'x19' parking spaces will be on the east side and seven 9'x18' parking spaces the south side along with the 9'x18' handicap space and 9'x18' handicap loading zone. The southwest corner of the development will have mail boxes, picnic tables and a grassy recreation area. The East side of the lot will a trash/recycling enclosure at the southern end. The site will have a grassy recreation area with trees and a gazebo bordered by the south, east and north portions of the development as well as the west property line. The building and parking rain water collection system will be directed to the SE area of the parking lot in front of the trash/recycling enclosure. The storm water after detention and treatment will accommodate the 1yr, 2yr, 5yr, 10yr and 25yr storms using City of Sandy 24 hour rainfall. It will be metered out to retain the flow to reduce the storms to be stored and discharged at the same rate that the project discharged at existing conditions. The discharges will no longer be overland to City and Park District property but directed to the ditch along Meinig Ave. Storm drainage will be detained in a system of two 40' pipes 5' in diameter pipes. The project is in a location that does not allow for significant infiltration and this could be dangerous to downstream areas.

Existing Stormwater System

The existing system discharged storm drainage was discharge from the original house roof to daylight on to the ground and then be discharged overland to the city property and to the Park southeasterly from the property this water has no direct discharge to a channel. Continuing the discharge in pipes or overland would require approval of the Park district and require DSL and Corps approval to discharge with pipes to the street. By directing the flow to the existing storm drainage system of pipes we would not require approval because it enters a City pipes system after discharging to a ditch along Meinig Ave.

Storm Water Analysis

4.1 Design Solution:

The proposed storm water design on property includes: One catch basin, 2 5' diameter 40' long detention pipes, one detention manhole, and a water quality manhole.

4.2 Design Assumptions and Parameters of Detention

City of Sandy Rainfall in Inches per 24 hour period: 3.5 (2 year), 4.5 (5 year), 4.8 (10 year), 5.5 (25 year), 6.5 (100 year)

Impervious Area of Roof, Driveway Sidewalks and Patio Prior to Development.: 0.0 Acres CN# used for Impervious areas: 98 Length N/A Time interval of analysis: N/A Unit Hydrograph: N/A Storm Distribution: Type 1A

Area of Site Prior to Development.: 0.65 Acres (Including Large Right of Way) CN# used for Pervious areas: 77 Slope: 15% Length: 125 Feet Time interval of analysis: 1 minute Unit Hydrograph: Lag Storm Distribution: Type 1A

Impervious Area of Roof, Driveway, Sidewalks and Deck after Development: 0.478 Acres
CN# used for Impervious areas: 98
Slope: 2%
Length: 100 Feet
Time interval of analysis: 1 minute
Unit Hydrograph: Lag
Storm Distribution: Type 1A

Area of Landscaping after Development: 0.21 Acres CN# used for Pervious areas: 77 Slope: 15% Length: 125 Feet Time interval of analysis: 1 minute Unit Hydrograph: Lag Storm Distribution: Type 1A

4.3 Reservoir Analysis:

Please note the proposed Detention utilizes no percolation.

The storage was developed using detention pipes to modify the discharge to predevelopment levels.

The pipe system uses 80 lineal feet of 5 foot diameter N12 PVC conduits.

Most of the storm water collection system backwaters into the detention pipes.

Attached in the Appendix is the Reservoir Stage Storage Discharge Table (Reservoir Report)

The report analyzes a 2.4 inch orifice at the bottom of the pipe storage a 2.8 inch orifice at 2.5 feet and a 2 inch orifice at 4.15 feet which was never reached. The Final Analysis will refine the preliminary design and may change to Storm Tech Chambers.

This utilizes 1,288 cubic feet of storage of the 1571 cubic feet of pipe storage available.

4.4 Design Flow Analysis:

The values of discharge for each storm are tabulated. On the tables provided for each return interval in the Appendix. Below are the comparisons of peak discharge or each return interval.

Return Interval	Existing (CFS)	Proposed (CFS)
2 Year	0.19	0.19
5 Year	0.32	0.32
10 Year	0.36	0.36
25 Year	0.43	0.43

24 hour Statistical Storm Det

		tical Storm Da Peak Flow (c				
Year	in 24					
	Hours	Impervious	Pervious	Combined	Existing	Detention
2	3.5"	0.37	0.06	0.43	0.19	0.19
5	4.5"	0.48	0.10	0.58	0.32	0.32
10	4.8"	0.52	0.12	0.63	0.36	0.36
25	5.5"	0.59	0.15	0.74	0.46	0.43
100	6.5"					

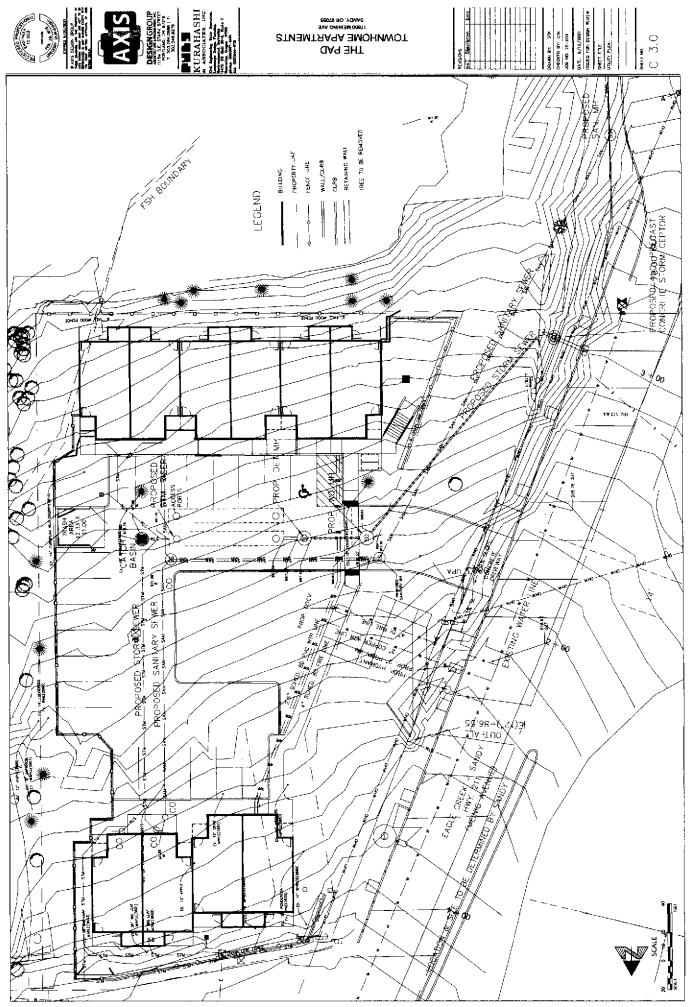
The allowable discharge that was the limit for Developed Discharge.

4.5 CONCLUSION:

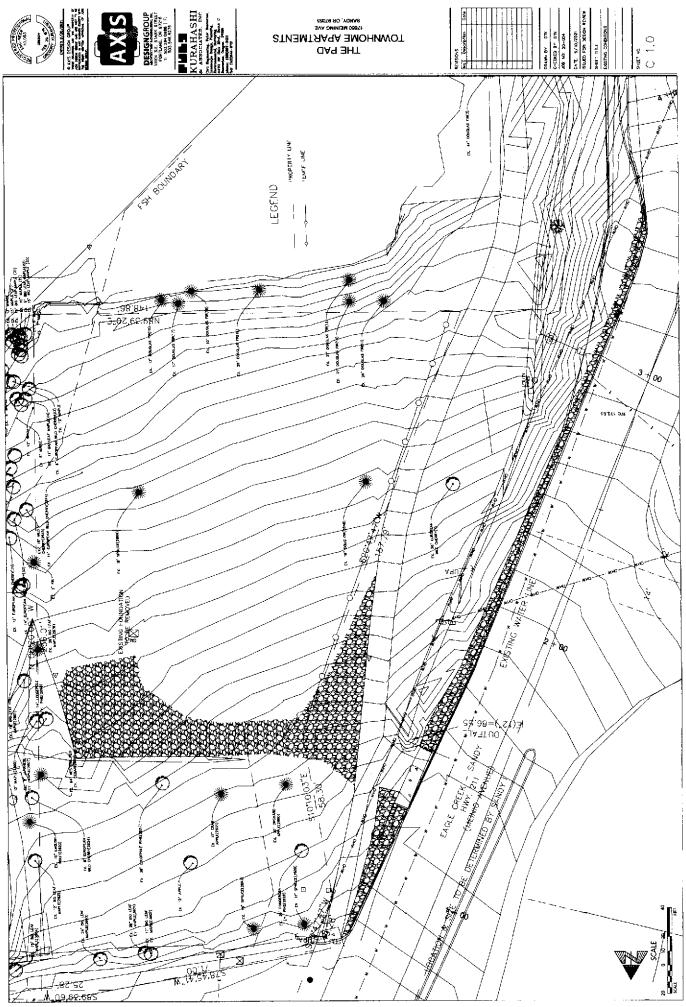
Based on the analysis and findings above, the proposed stormwater drainage system complies with the requirements of the City of Sandy.

Appendix

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THE PAD Development UTILITY PLAN	1
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FLOW SUMMARY REPORTS (.5 YEAR HYDO MOD. WQ), 2,5,10,25 YR. RET. PER.	5-8



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Runoff Curve Numbers f	Table 2.2	al Cuburban	الساللي			Ť
(Sources: TR 55, 1986, and Stor	muster Monogement Manual	1002 See Seeting		an Area	<u>as</u>	·
	inwater Management Manual,					
Cover type and hydrologic condition.	·	<u>C</u>			soil gro	ар
			A	B	<u> </u>	D
	Numbers for Pre-Developm	ent Conditions				
Pasture, grassland, or range-continuous for	rage for grazing:					
Fair condition (ground cover 50% to 75% and	not heavily grazed).		49	69	79	84
Good condition (ground cover >75% and light	tly or only occasionally graze	<u>d)</u>	39	61	74	80
Woods:						
Fair (Woods are grazed but not burned, and so	ome forest litter covers the soi	l).	36	60	73	79
Good (Woods are protected from grazing, and			30	55	70	77
	Numbers for Post-Developm	ent Conditions				
Open space (lawns, parks, golf courses, cem	eteries, landscaping, etc.)'					
Fair condition (grass cover on 50% - 75% of the			77	85	90	92
Good condition (grass cover on >75% of the a	rea)		68	80	86	90
Impervious areas:						
Open water bodies: lakes, wetlands, ponds etc	<u>_</u>		100	100	100	100
Paved parking lots, roofs2, driveways, etc. (ex	cluding right-of-way)		98	98	98	98
Permeable Pavement (See Appendix C to de	ecide which condition below	to use)	<u>-</u>			
Landscaped area			77	85	90	92
50% landscaped area/50% impervious			87	91	94	96
100% impervious area			98	98	98	98
Paved	<u> </u>		98	98	98	98
Gravel (including right-of-way)			76	85	89	91
Dirt (including right-of-way)			72	82	87	89
Pasture, grassland, or range-continuous forage fo	n grazine:		, 2	02		
Poor condition (ground cover <50% or heavily graze	ed with no mulch).		68	79	86	89
Fair condition (ground cover 50% to 75% and not he	eavily grazed).		49	69	79	84
Good condition (ground cover >75% and lightly or e	only occasionally grazed)		39	61	74	80
Woods:						
Poor (Forest litter, small trees, and brush are d			45	66	77	83
Fair (Woods are grazed but not burned, and so			36	60	73	79
Good (Woods are protected from grazing, and			30	55	70	77
	uld only be used for	Average Percent				
	divisions > 50 acres	impervious area ^{3,4}				
1.0 DU/GA	· · · · · · · · · · · · · · · · · · ·	15			e number/	
1.5 DU/GA		20		ll be selec		
2.0 DU/GA		25			npervious	
2.5 DU/GA		30		tions of th	e site or	
3.0 DU/GA		34	bas	מי		
3.5 DU/GA	····					
40 DU/GA 4.5 DU/GA		42 46		- ······	 .	
5.0 DU/GA		40 48				· · · · · ·
5.5 DU/GA		50				
6,0 DU/GA		52				
6.5 DU/GA		54				
7.0 DU/GA	· · · ·	56				
7.5 DU/GA		58				
PUD's, condos, apartments, commercial	%impervious	Separate curve m	imhers s	hall '	1	
businesses, industrial areas &	must be	be selected for pe				
& subdivisions < 50 acres χ	computed	impervious portio				
For a more detailed and complete description of land			بلله دب مسم	~ 1110		

Release No. 55, (210-V1-1R-55, Second Ed., sume 1200). ¹ Composite CN's may be computed for other combinations of open space cover type. ²Where roof runoff and driveway runoff are infiltrated or dispersed according to the requirements in Chapter 3, the average percent impervious area may be adjusted in accordance with the procedure described under "Flow Credit for Roof Downspout Infiltration" (Section 3.1.1), and "Flow Credit for Roof Downspout Dispersion" (Section 3.1.2). ³Assumes roof and driveway runoff is directed into street/storm system. ⁴All the remaining pervious area (lawn) are considered to be in good condition for these curve numbers.

February 2005

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Volume III – Hydrologic Analysis and Flow Control BMPs

Reservoir Report

Reservoir No. 1 - Detention Pipe

Pond Data

F Olia Data					
Pipe diameter	= 5.00 ft	Pipe length = 160.0	ft Pipe slope	= 0.00 % Invert elev.	= 100.00 ft
Stage / Storag	e Table				
			L		
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)	
0.00	100.00	00	0	0	
0.25	100.25	00	29	29	
0.50	100.50	00	52	82	
0.75	100.75	00	66	148	
1.00	101.00	00	76	224	
1.25	101.25	00	84	307	
1.50	101.50	00	89	397	
1.75	101.75	00	94	490	
2.00	102.00	00	96	587	
2.25	102.25	00	99	686	
2.50	102.50	00	100	786	
2.75	102.75	00	100	885	
3.00	103.00	00	99	985	
3.25	103.25	00	97	1,081	
3.50	103.50	00	93	1,175	
3.75	103.75	00	89	1,264	
4.00	104.00	00	84	1,348	
4.25	104.25	00	76	1,423	
4.50	104.50	00	66	1,489	
4.75	104.75	00	52	1,542	
5.00	105.00	00	29	1,571	

Wei	r Stru	ictures
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	[A]	[B]	[C]	[D]		[A]	[8]	[C]	[D]
Rise in	= 2.4	2.8	2.0	0.0	Crest Len ft	= 0.00	0.00	0.00	0.00
Span in	= 2.4	2.8	2.0	0.0	Crest El. ft	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	1	1	0	Weir Coeff.	= 0.00	0.00	0.00	0.00
Invert El. ft	= 100.00	102.50	104.15	0.00	Weir Type	=			
Length ft	= 10.0	10.0	10.0	0.0	Multi-Stage	= No	No	No	No
Slope %	= 1.00	1.00	1.00	0.00					
N-Value	= .013	.013	.013	.000					
Orif. Coeff.	= 0.60	0.60	0.60	0.00					
Multi-Stage	= n/a	No	No	No	Exfiltration Rat	te = 0.00 in/hr/	sqft Tailw	ater Elev. =	= 0.00 ft

								Note: A	Il outflows hav	e been analyz	ed under inlet and	d outlet control.
Stage /	Storage / I	Discharge ⁻	Table									
Stage	Storage	Elevation	Civ A	Clv B	Clv C	Civ D	Wr A	Wr B	Wr C	Wr D	Exfil	Total
ft	cuft	ft	cfs	cfs	cfs	cfs	cfs	cfs	cfs	cfs	cfs	cfs
0.00	0	100.00	0.00	0.00	0.00							0.00
0.25	29	100.25	0.05	0.00	0.00							0.05
0.50	82	100.50	0.08	0.00	0.00							0.08
0.75	148	100.75	0.10	0.00	0.00			_		_		0.10
1.00	224	101.00	0.12	0.00	0.00							0.12
1.25	307	101.25	0.13	0.00	0.00				—		—	0.13
1.50	397	101.50	0.15	0.00	0.00							0.15
1.75	490	101.75	0.16	0.00	0.00					—		0.16
2.00	587	102.00	0.17	0.00	0.00							0.17
2.25	686	102.25	0.18	0.00	0.00							0.18
2.50	786	102.50	0.19	0.00	0.00							0.19
2.75	885	102.75	0.20	0.06	0.00						***	0.26
3.00	985	103.00	0.21	0.10	0.00							0.32
3.25	1,081	103.25	0.22	0.14	0.00							0.36
3.50	1,175	103.50	0.23	0.16	0.00							0.39
3.75	1,264	103.75	0.24	0.18	0.00							0.42
4.00	1,348	104.00	0.24	0.20	0.00						—	0.45
4.25	1,423	104.25	0.25	0.22	0.02							0.49
4.50	1,489	104.50	0.26	0.24	0.04						—	0.54
4.75	1,542	104.75	0.27	0.25	0.06							0.58
5.00	1,571	105.00	0.27	0.26	0.07							0.61

Hydraflow Hydrographs by Intelisolve

Hyd.	Hydrograph	Peak	Time	Time		Inflow	Maximum	Maximum	Hydrograph
No.	type	flow	interval	to peak	Volume		elevation	storage	description
	(origin)	(cfs)	(min)	(min)	(cuft)		(ft)	(cuft)	a good go an an ann an ann an Ann an An
1	SCS Runoff	0.37	1	469.00	5,309				Pad Impervious
2	SCS Runoff	0.06	1	477.00	1,021				The Pad Pervious
3	Combine	0.43	1	470.00	6,330	1, 2			Combined Site
4	SCS Runoff	0.19	1	477.00	3,160				Existing Conditions
5	Reservoir	0.19	1	500.00	6,309	3	102.33	718	Detention Pipe
6									
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. Hydro	ograph ype	Peak flow	Time interval	Time to peak	Volume	Inflow hyd(s)	Maximum elevation	Maximum storage	Hydrograph description
(or	rigin)	(cfs)	(min)	(min)	(cuft)		(ft)	(cuft)	
and the second s	Runoff	0.48	1	469.00	6,931				Pad Impervious
	Runoff	0.10	1	475.00	1,578				The Pad Pervious
4	nbine	0.58	1	470.00	8,509	1, 2			Combined Site
	Runoff	0.32	1	475.00	4,884	., –			Existing Condition
	ervoir	0.32	1	489.00	8,475	3	103.03	998	Detention Pipe
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Hyd. No.	Hydrograph type	Peak flow	Time interval	Time to peak	Volume	Inflow hyd(s)	Maximum elevation	Maximum storage	Hydrograph description
	(origin)	(cfs)	(min)	(min)	(cuft)		(ft)	(cuft)	
1	SCS Runoff	0.52	1	469.00	7,418				Pad Impervious
2	SCS Runoff	0.12	1	475.00	1,754				The Pad Pervious
3	Combine	0.63	1	470.00	9,171	1, 2			Combined Site
4	SCS Runoff	0.36	1	475.00	5,428				Existing Conditions
5	Reservoir	0.36	1	488.00	9,131	3	103.25	1,081	Detention Pipe
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1. ,	Hydrograph type	Peak flow			Volume	inflow hyd(s)	Maximum elevation	Maximum storage	Hydrograph description
	(origin)	(cfs)	(min)	(min)	(cuft)		(ft)	(cuft)	
	SCS Runoff	0.59	1	469.00	8,554				Pad Impervious
	SCS Runoff	0.15	1	474.00	2,175				The Pad Pervious
	Combine	0.74	1	470.00	10,729	1, 2			Combined Site
	SCS Runoff	0.46	1	474.00	6,731				Existing Conditions
	Reservoir	0.43	1	487.00	10,673	3	103.82	1,288	Detention Pipe
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